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A MODEL FOR
THE ANALYSIS OF STOCKPILE/PRODUCTION
BASE TRADEOFFS

Do Jeffrey H. Grotte
Do Paul F. McCoy

March 1979

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This paper presents a linear programming model that determines the least cost mix of stockpile and production base necessary to satisfy wartime consumption. The model includes a build-up period during which production base is acquired and the stockpile is built, a steady-state period during which assets are at maintained post-build-up levels until the start of the war, and a mobilization-and-war period during which demand for the consumable must be met, either through stockpile depletion or through wartime production from previously acquired base.

The model is fast running and allows the user great flexibility in specifying the planning scenario.

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I. INTRODUCTION

A. BACKGROUND

Two mechanisms are available to provide a consumable, such as ammunition, for a possible future war:

(1) A *stockpile* is generally established to meet the immediate (and usually heavy) demand in the early stages of the war. Stockpiles are generally very responsive; that is, they are quickly made available, but unless very large, they can be eventually exhausted if the war endures for any length of time.

(2) A *production base* for manufacturing the consumable can provide for the requirements of a protracted war. However, because of the length of time required to bring a production base into operation, production bases are inadequate to satisfy demand early in the war.

It is therefore generally accepted that both a stockpile and a production base are necessary to satisfy wartime requirements--the stockpile for the early stages of the war, the production base later on. During the intermediate stages of the war, trade-offs can be made to some extent--a larger stockpile can postpone the need for bringing the production base into play, thus permitting a less reactive and possibly less costly base, whereas a production base that can quickly be brought to wartime levels of production can reduce the size of the required stockpile. In this sense stockpile and production base are partially substitutable during wartime. *+ peacetime*

Too simplified

During peacetime, however, stockpile and production base are complementary. The larger the stockpile being established, the larger is the production base needed to produce it.

Because of these relationships, stockpile and production base are inextricably linked. One cannot determine the correct stockpile size without considering the production base nor can one specify the production base without accounting for the stockpile. It follows, therefore, that if one wishes to optimally fix, by some measure of effectiveness, the sizes of the stockpile and production base to satisfy the requirements of some projected war, one must consider them jointly and balance their respective features and costs. Among other things, one must attend to such attributes as responsiveness to demand, holding and production costs, deterioration rates, budget limitations, and so forth, in order to determine the best stockpile/production base mix.

To assist in this determination, this paper presents the IDA Stockpile/Production Base Model (hereafter the S/PB model), an optimizing computer model that determines the least costly combination of stockpile and production base required to meet a specified wartime consumption curve. The model explicitly considers such parameters as planning and warning periods, deterioration rates, cost discounting factors, and so forth. Using the methods of linear programming, the model determines a globally optimal schedule of production base purchases and consumable production. The model can also be used to find the best combination of two alternative production bases for the same consumable. The model examines a single type of consumable at a time, but can be applied to many different types.

B. MODEL OVERVIEW

The S/PB model is based on a simple time step model wherein the variables represent activities at certain times. However, in order to combine the peacetime planning period, wherein

stockpile and production base are acquired in an orderly fashion, with the wartime period, where they must be managed to deal with rapidly changing requirements, the basic, or core, time step model has been modified to account for those separate periods of time.

The first period--what we call the Build-up period--is characterized by the smooth acquisition of assets. Typically lasting many years, this period includes the purchase of production base to be used to build the stockpile, the purchase of the production base to be stored for later, wartime, use, and the creation of the stockpile from production base producing at peacetime rates. Pre-existing assets, of course, are considered in this period.

We do not assume that the war necessarily begins conveniently right after the Build-up period. Although supposing the war will occur is necessary to establish the consumption requirements, whether it actually occurs, and when, is not at all certain. In order to address these types of uncertainties, the model allows an interval of variable (user-specified) length called the Steady-state period which separates the onset of the war from the conclusion of the Build-up period. During the Steady-state period, resources acquired during the Build-up period are maintained at constant levels. The long-term peacetime costs of stockpile and production base may be accounted for during this period.

The Steady-state period terminates with the beginning of industrial mobilization, which marks the beginning of the Mobilization/War period. This period most closely resembles the core time-step model and during this period the production base previously acquired is typically brought to wartime production rates and the consumable is produced by the production base as well as drawn down by the wartime requirements. Additional production base may be acquired, if needed, and time

lags in changing production rates, as well as shipping the consumable from where it is produced to the theater, are carefully kept track of.

Throughout these three periods, the costs of all activities are accounted for and the objective of the model is to arrange these activities during the Build-up, Steady-state, and Mobilization/War periods so as to minimize the total costs.¹

There are various optional constraints, such as budget constraints, that can be imposed by the user who wishes to explore a range of policy options.

Chapter II supplies the mathematical formulation of the model. Chapter III is a User's Guide. Appendix A contains Glossaries of Input Parameters and Model Variables and Appendix B is a FORTRAN listing of the model as implemented at IDA.

¹At the user's discretion, wartime costs can be included or omitted in this total.

II. MATHEMATICAL FORMULATION

The S/PB model represents activities over time--from the beginning of an acquisition period, during which capital equipment for the production base is acquired and the stockpile is prepared, through a period from the end of the build-up to the beginning of the mobilization, during which the various components of the model are kept at constant levels, to a final period of mobilization and war. These are called, respectively, the Build-up, the Steady-state and the Mobilization/War periods. While each of these periods is an embodiment of essentially the same activities, the different emphasis placed on each period makes it convenient to model the three periods in quite different ways.

In order to assist the reader in comprehending not only the entire model, but also the differences and similarities among the three periods that partition the model, we adopt a two step approach. We first define what we shall call a "core model" which comprises the fairly simple equations that specify the interactions among model components without regard to initial and final conditions and ignoring the specific assumptions that distinguish the three periods. Once the core model has been described, it provides the background for the three periods of the S/PB model. We begin by discussing the components common to the core and S/PB models.

For simplicity of exposition, we will refer to the consumable as ammunition. Bear in mind, however, that this is only one form of consumable and that the model has applications to other wartime consumables.

A. COMPONENTS

The fundamental components shared by the core and S/PB models are these:

- (1) Capital equipment for producing ammunition
- (2) A domestic ammunition stockpile
- (3) An in-theater ammunition stockpile supplied from the domestic stockpile
- (4) Domestic and in-theater demands for ammunition.

*could
warm
hot*
The capital equipment may be in one of three states. It may be in storage and not producing ammunition, or it may be producing ammunition at a moderate rate (as during peacetime) or at a high rate (as during mobilization and war). These three states we will refer to as cold, warm, and hot, respectively. Each state entails different costs, both of maintaining the capital, and of producing ammunition in the case of warm and hot ammunition. Capital may be transferred among states, although this incurs additional costs as well as time delays.

*layaway?
stockpile*

In order for the model to distinguish between, for instance, expensive, highly automated equipment that may be very responsive to wartime demands, and less responsive, less costly equipment, or between other capital alternatives (e.g., capital equipment with differing productivities), the model accommodates two types of capital for producing a single ammunition type, which we will refer to as type 1 and type 2 capital. These types of capital are distinguishable only through the values of the inputs that pertain to them. Otherwise the model handles them in identical ways.

Ammunition produced by warm and hot type 1 and type 2 capital equipment enters the domestic stockpile, from which some of it may be shipped to the in-theater stockpile. The domestic stockpile is used to satisfy domestic demand while in-theater demand draws on the in-theater stockpile.

Capital equipment in all states and ammunition in both stockpiles are subject to deterioration; that is, over a period of time, a certain fraction of the resources becomes useless.

The relationships among these components are depicted in Figure 1. New capital of either type enters the model via purchases which feed directly into cold stock. From cold stocks, capital may be transferred to warm or hot stocks and capital in warm stocks may be transferred to hot or back to cold stocks. Hot capital may transfer to either cold or warm stocks. Note that there is no transfer between type 1 and type 2 capital. Over time, all six categories of capital suffer deterioration, as we have already said, although this is not depicted on the diagram.

Ammunition produced by warm and hot capital stocks enters the domestic stockpile from which some is removed to satisfy domestic demand, some is lost to deterioration, and some is transferred to the in-theater stockpile. The mechanism by which ammunition is transported from the domestic to the in-theater stockpile, be it airlift, sealift, or some other means, will be referred to as the "pipeline." Part of the in-theater stockpile goes to satisfy in-theater demand and another fraction deteriorates. The remainder is held against future requirements. The domestic and in-theater stockpiles are distinguished primarily to model the effect of time lag in the pipeline; that is, the delay between when ammunition is produced and when it is available in the theater, and also to account for pipeline quantity constraints and upper bounds on the in-theater stockpile. As in the case of capital equipment, the deterioration of the domestic and in-theater stockpiles is not depicted in Figure 1.

Each transfer of resource, whether capital equipment or ammunition, incurs a time delay. Equipment purchased may not appear in cold stocks until after a suitable period of time. Equipment transferred from cold to warm or hot stocks cannot produce until after a suitable period of time while equipment

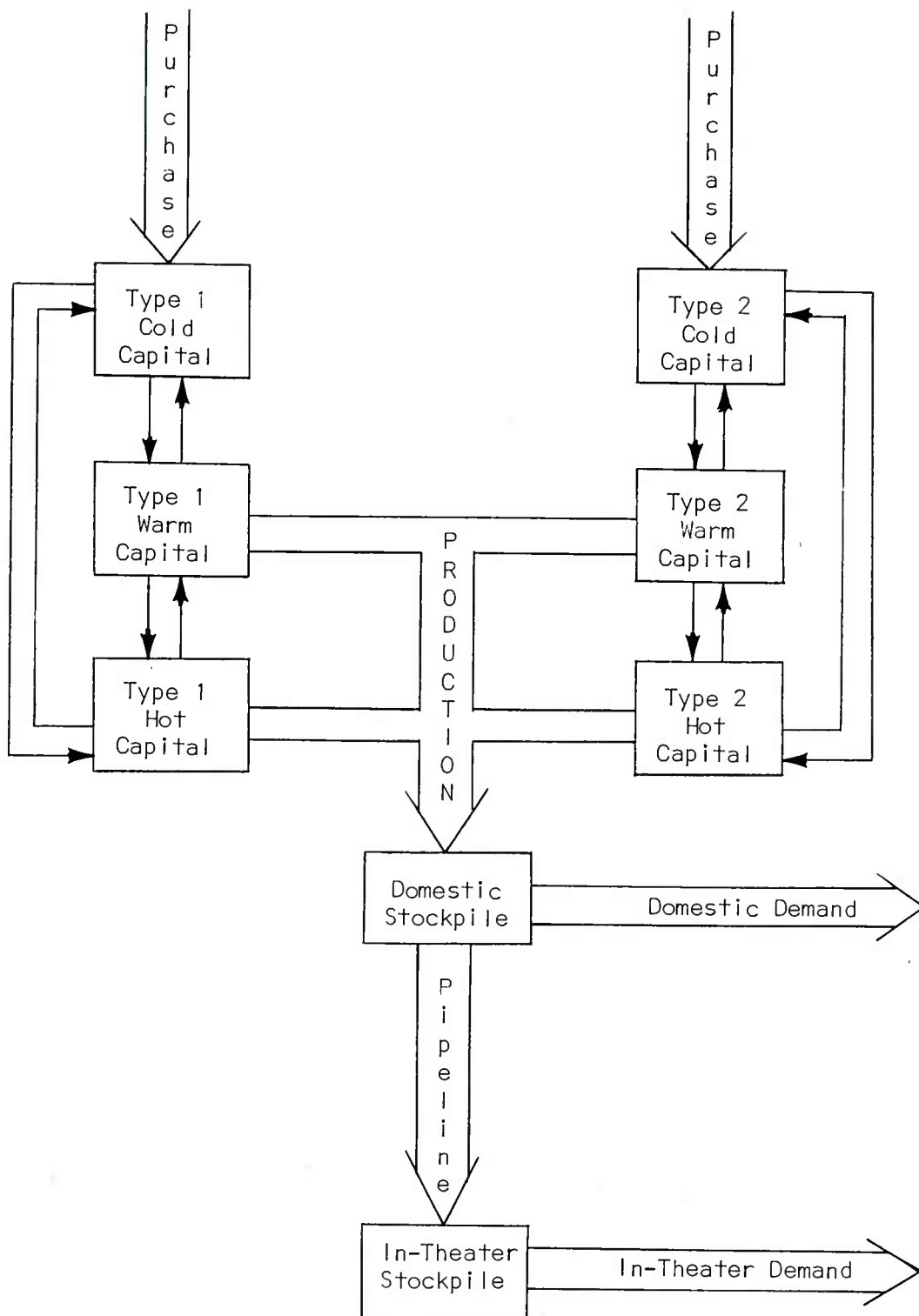


Figure 1. SCHEMATIC OF MODEL

going from warm to hot requires a certain time to reach the hot level, during which it continues to produce at the warm rate. In a like manner, ammunition going from the domestic to the in-theater stockpile may be thought of as being in the pipeline for a certain length of time.

Although not explicitly represented in Figure 1, each activity depicted has an associated cost. Costs apply to the holding and transfer of resources, as well as the purchase of capital and the production of ammunition.

B. TIME PERIODS

As discussed previously, the components are manipulated over a time span that comprises a Build-up period, a Steady-state period, and a Mobilization/War period. In order to model the dynamics of this manipulation over time, the three periods are divided into various numbers of equal length time steps. The time step is the fundamental unit of time--no action can take less than this time unit to execute. For instance, if the time step is one month, then all the time delays in the model must be multiples of one month, as must be the lengths of the three periods. A typical time span under investigation might have a Build-up period of five years (60 time steps), and a Steady-state period of 15 years (180 time steps) and a Mobilization/War period of two years (24 time steps). The time required for purchased capital to enter cold stocks may be 24 months (24 time steps); for capital to transfer from cold to warm stocks, six months (6 time steps); and so forth. The length of the time step, as well as the duration of the three periods, is flexible and determined by the user of the S/PB model.

C. THE CORE MODEL

The core model describes the interactions of the model components without regard to initial and terminal conditions. In addition, the differences among the Build-up, Steady-state

and Mobilization/War periods are suppressed. The core model describes how levels of resources at any given time step relate to the levels of resources at other time steps without the complicating distinctions among periods. The S/PB model is based entirely on the core model, although the assumptions implicit in each period alter the basic mathematical expressions considerably.

We will index the time steps using the integer t , which, one may assume, takes on values between $-\infty$ and ∞ (because we have ignored initial and terminal conditions). The variables of the core model are listed and defined below. Because of our assumptions, note that there are a countably infinite number of variables in the core model, which makes it impractical to employ, although this does not decrease its pedagogical usefulness. The units of measurement implicit in each variable are not important as long as a consistent standard is adopted. Finally, we employ FORTRAN-like variable names. Although this is somewhat cumbersome, these variable names parallel those in the computer implementation of the S/PB model and, therefore, once used to these variable names, the reader will find it easier to learn the S/PB model. All the variables are assumed nonnegative.

1. Variables

a. Capital Stocks

- $C1(t)$ = the amount of type 1 cold capital stocks held during time step t
- $C2(t)$ = the amount of type 2 cold capital stocks held during time step t
- $W1(t)$ = the amount to type 1 warm capital stocks held during time step t
- $W2(t)$ = the amount of type 2 warm capital stocks held during time step t
- $H1(t)$ = the amount of type 1 hot capital stocks held during time step t
- $H2(t)$ = the amount of type 2 hot capital stocks held during time step.

b. Ammunition Stockpile

$S(t)$ = the amount of ammunition held in the domestic stockpile during time step t

$SP(t)$ = the amount of ammunition held in the in-theater stockpile during time step t .

2. Transfer Variables

Note: In all cases, the transfers of assets described below are initiated during time step t and concluded during a future time step.

$TCW1(t)$ = the amount of type 1 capital transferred from cold to warm stocks beginning during time step t

$TCW2(t)$ = the amount of type 2 capital transferred from cold to warm stocks beginning during time step t

$TCH1(t)$ = the amount of type 1 capital transferred from cold to hot stocks beginning during time step t

$TCH2(t)$ = the amount of type 2 capital transferred from cold to hot stocks beginning during time step t

$TWH1(t)$ = the amount of type 1 capital transferred from warm to hot stocks beginning during time step t

$TWH2(t)$ = the amount of type 2 capital transferred from warm to hot stocks beginning during time step t

$THW1(t)$ = the amount of type 1 capital transferred from hot to warm stocks beginning during time step t

$THW2(t)$ = the amount of type 2 capital transferred from hot to warm stocks beginning during time step t

$THC1(t)$ = the amount of type 1 capital transferred from hot to cold stocks beginning during time step t

$THC2(t)$ = the amount of type 2 capital transferred from hot to cold stocks beginning during time step t

$TWC1(t)$ = the amount of type 1 capital transferred from warm to cold stocks beginning during time step t

$TWC2(t)$ = the amount of type 2 capital transferred from warm to cold stocks beginning during time step t

$PIPE(t)$ = the amount of ammunition transferred from the domestic to the in-theater stockpile beginning during time step t .

3. Capital Purchase Variables

$PC1(t)$ = the amount of type 1 capital purchased during time step t

$PC2(t)$ = the amount of type 2 capital purchased during time step t .

4. Structural Equations

The structural equations of the core model are given below. They describe the interactions over time of the stockpiles and capital stocks. Parameters required by the core model are described following the equations in which they are introduced.

a. Cold Equipment Stocks

$$(1) \quad C1(t) = C1(t-1) \cdot (1-DC1) + PC1(t-LP1) + TWC1(t-LWC1) \\ + THC1(t-LHC1) - TCH1(t) - TCW1(t)$$

$$(2) \quad C2(t) = C2(t-1) \cdot (1-DC2) + PC2(t-LP2) + TWC2(t-LWC2) \\ + THC2(t-LHC2) - TCH2(t) - TCW2(t)$$

where

$DC1$ = the fraction of type 1 cold stocks lost to deterioration during one time step

$DC2$ = the fraction of type 2 cold stocks lost to deterioration during one time step

$LP1$ = the number of time steps from the time type 1 capital is purchased until it is delivered to cold stocks

$LP2$ = the number of time steps from the time type 2 capital is purchased until it is delivered to cold stocks

$LWC1$ = the number of time steps required to transfer type 1 capital from warm to cold stocks

$LWC2$ = the number of time steps required to transfer type 2 capital from warm to cold stocks

$LHC1$ = the number of time steps required to transfer type 1 capital from hot to cold stocks

$LHC2$ = the number of time steps required to transfer type 2 capital from hot to cold stocks.

Equations (1) and (2) are easily interpreted. For instance, Equation (1) states that the amount of type 1 cold capital held during time step t is the total of (i) the amount held during time step $t-1$, corrected for deterioration, (ii) plus the amount of type 1 capital purchased LP1 time steps previously, (iii) plus the amount of type 1 capital transferred from warm to cold stocks beginning LWCl time steps previously, (iv) plus the amount of type 1 capital transferred from hot to cold stocks beginning LHCl time steps previously, (v) minus the amount of type 1 capital transferred from cold to warm stocks beginning during this time step, (vi) minus the amount of type 1 capital transferred from cold to hot stocks beginning during this time step. An analogous explanation applies to Equation (2).

Because the remaining structural equations closely resemble Equations (1) and (2), being accountings of the flows of resources, we leave it to the reader to supply most of the interpretations of the remaining equations.

b. Warm Equipment Stocks

$$\begin{aligned}
 (3) \quad W1(t) &= W1(t-1) \cdot (1-DW1) + TCW1(t-LCW1) + THW1(t-LHW1) \\
 &\quad - TCW1(t) - TWH1(t) \\
 W2(t) &= W2(t-1) \cdot (1-DW2) + TCW2(t-LCW2) + THW2(t-LHW2) \\
 &\quad - TWC2(t) - TWH2(t)
 \end{aligned}$$

where

- DW1 = the fraction of type 1 warm stocks lost to deterioration during one time step
- DW2 = the fraction of type 2 warm stocks lost to deterioration during one time step
- LCW1 = the number of time steps required to transfer type 1 capital from cold to warm stocks
- LCW2 = the number of time steps required to transfer type 2 capital from cold to warm stocks
- LHW1 = the number of time steps required to transfer type 1 capital from hot to warm stocks

LHW2 = the number of time steps required to transfer type 2 capital from hot to warm stocks.

c. Hot Equipment Stocks

$$\begin{aligned}
 (5) \quad H1(t) &= H1(t-1) \cdot (1-DH1) + TCH1(t-LCH1) + TWH1(t-LWH1) \\
 &\quad - THC1(t) - THW1(t) \\
 (6) \quad H2(t) &= H2(t-1) \cdot (1-DH2) + TCH2(t-LCH2) + TWH2(t-LWH2) \\
 &\quad - THC2(t) - THW2(t)
 \end{aligned}$$

where

DH1 = the fraction of type 1 hot stocks lost to deterioration during one time step
 DH2 = the fraction of type 2 hot stocks lost to deterioration during one time step
 LCH1 = the number of time steps required to transfer type 1 capital from cold to hot stocks
 LCH2 = the number of time steps required to transfer type 2 capital from cold to hot stocks
 LWH1 = the number of time steps required to transfer type 1 capital from warm to hot stocks
 LWH2 = the number of time steps required to transfer type 2 capital from warm to hot stocks.

d. Domestic Ammunition Stockpile

$$\begin{aligned}
 (7) \quad S(t) &= S(t-1) \cdot (1-DS) + \frac{W1(t)}{KW1} + \frac{W2(t)}{KW2} + \frac{H1(t)}{KH1} + \frac{H2(t)}{KH2} \\
 &\quad + \sum_{t-LWH1 < s \leq t} \frac{TWH1(s)}{KW1} + \sum_{t-LWH2 < s \leq t} \frac{TWH2(s)}{KW2} \\
 &\quad - PIPE(t) - DD(t)
 \end{aligned}$$

where

DS = the fraction of the domestic ammunition stockpile lost to deterioration during one time step
 KW1 = the capital to output ratio for type 1 warm capital (see discussion below)

²
KW2 = the capital to output ratio for type 2 warm capital
(see discussion below)

KH1 = the capital to output ratio for type 1 hot capital
(see discussion below)

KH2 = the capital to output ratio for type 2 hot capital
(see discussion below)

DD(t) = the domestic demand for ammunition during time
step t.

The core model represents the production of ammunition through the capital to output ratios KW1, KW2, KH1, and KH2. Each ratio represents the amount of capital of the specified category required to produce one unit of ammunition, so that the expression

$$\frac{W1(t)}{KW1} + \frac{W2(t)}{KW2} + \frac{H1(t)}{KH1} + \frac{H2(t)}{KH2} \\ + \sum_{t-LWH1 < s \leq t} \frac{TWH1(s)}{KW1} + \sum_{t-LWH2 < s \leq t} \frac{TWH2(s)}{KW2}$$

represents the total amount of ammunition produced during time step t. The final two terms represent production at warm rates by capital being transferred from warm to hot stocks. The summations account for the transfer time delay.

e. In-Theater Ammunition Stockpile

$$(8) \quad SP(t) = SP(t-1) \cdot (1-DSP) + PIPE(t-LPIPE) - FD(t)$$

where

DSP = the fraction of the in-theater ammunition stockpile lost to deterioration during one time step

LPIPE = the number of time steps required to transfer ammunition from the domestic to the in-theater stockpile

FD(t) = the in-theater demand for ammunition during time step t.

5. Costs

The user's goal in employing the S/PB model is to determine values for the variables that are consistent with the structural equations, that satisfy additional constraints of the user's choosing, and that minimize some objective function. The objective function we choose is that which represents the total cost of all activities represented by the model, discounted over time. To be consistent with our two step approach to the description of the S/PB model, we provide, in this section, an objection function for the core model.

We begin by listing, for each variable of the core model, the name of the parameter describing the cost associated with that variable and the definition of the cost. Note that some variables, specifically $W1(t)$, $W2(t)$, $H1(t)$, and $H2(t)$, are associated with more than one cost, and that some costs, namely, $VPW1$ and $VPW2$, are associated with more than one variable.

<u>Variable</u>	<u>Cost Parameter</u>	<u>Definition</u>
$PC1(t)$	$VPC1$	The cost of purchasing one unit of type 1 capital
$PC2(t)$	$VPC2$	The cost of purchasing one unit of type 2 capital
$C1(t)$	$VC1$	The cost of maintaining one unit of type 1 capital in cold stocks for one time step.
$C2(t)$	$VC2$	The cost of maintaining one unit of type 2 capital in cold stocks for one time step
$W1(t)$	$VW1$	The cost of maintaining one unit of type 1 capital in warm stocks for one time step
$W2(t)$	$VW2$	The cost of maintaining one unit of type 2 capital in warm stocks for one time step

<u>Variable</u>	<u>Cost Parameter</u>	<u>Definition</u>
$\left. \begin{array}{l} \frac{W1(t)}{KW1} \\ \frac{TWH1(t)}{KW1} \end{array} \right\}$	VPW1	The cost of producing one unit of ammunition from type 1 warm stocks.
$\left. \begin{array}{l} \frac{W2(t)}{KW2} \\ \frac{TWH2(t)}{KW2} \end{array} \right\}$	VPW2	The cost of producing one unit of ammunition from type 2 warm stocks.
H1(t)	VH1	The cost of maintaining one unit of type 1 capital in hot stocks for one time step
H2(t)	VH2	The cost of maintaining one unit of type 2 capital in hot stocks for one time step
$\frac{H1(t)}{KH1}$	VPH1	The cost of producing one unit of ammunition from type 1 hot stocks
$\frac{H2(t)}{KH2}$	VPH2	The cost of producing one unit of ammunition from type 2 hot stocks
S(t)	VS	The cost of maintaining one unit of ammunition in the domestic stockpile for one time step
SP(t)	VSP	The cost of maintaining one unit of ammunition in the in-theater stockpile for one time step
PIPE(t)	VPIPE	The cost of transferring one unit of ammunition from the domestic to the in-theater stockpile
TCW1(t)	VCW1	The cost of transferring one unit of type 1 capital from cold to warm stocks
TCW2(t)	VCW2	The cost of transferring one unit of type 2 capital from cold to warm stocks
TCH1(t)	VCH1	The cost of transferring one unit of type 1 capital from cold to hot stocks
TCH2(t)	VCH2	The cost of transferring one unit of type 2 capital from cold to hot stocks
TWH1(t)	VWH1	The cost of transferring one unit of type 1 capital from warm to hot stocks
TWH2(t)	VWH2	The cost of transferring one unit of type 2 capital from warm to hot stocks
TWC1(t)	VWC1	The cost of transferring one unit of type 1 capital from warm to cold stocks

<u>Variable</u>	<u>Cost Parameter</u>	<u>Definition</u>
TWC2(t)	VWC2	The cost of transferring one unit of type 2 capital from warm to cold stocks
THC1(t)	VHC1	The cost of transferring one unit of type 1 capital from hot to cold stocks
THC2(t)	VHC2	The cost of transferring one unit of type 2 capital from hot to cold stocks
THW1(t)	VHW1	The cost of transferring one unit of type 1 capital from hot to warm stocks
THW2(t)	VHW2	The cost of transferring one unit of type 2 capital from hot to warm stocks

Note that the above cost parameters are independent of time--they are the same for all time steps. To allow for inflation and also opportunity costs, the core model permits these costs to be discounted over time. Let the parameter R denote the discount factor that applies to a single time step. Then the cost of an activity for a single time step is $(1+R)^{-1}$ times the cost of that activity for the previous time step. For instance, if the cost of maintaining one unit of ammunition in the domestic stockpile during time step t is VS , then the cost of maintaining one unit of the domestic stockpile during time step $(t+1)$ is $VS/(1+R)$, and the cost during time step $(t+2)$ is $VS/(1+R)^2$.

For the core model, we will arbitrarily select time $t = 0$ for the base costs so that the cost of an activity during time step t is the cost parameter times $(1+R)^{-t}$.

We present below the objective function of the core model. Because of the core model's infinite time horizon, one should view this function as a formal expression only, since for actual variables and parameters it may well be infinite.

$$\begin{aligned}
(9) \quad \sum_{all \ t} \frac{1}{(1+R)^t} \cdot \left\{ PC1(t) \cdot VPC1 + PC2(t) \cdot VPC2 + C1(t) \cdot VC1 \right. \\
+ C2(t) \cdot VC2 + W1(t) \cdot \left(VW1 + \frac{VPW1}{KW1} \right) + W2(t) \cdot \left(VW2 + \frac{VPW2}{KW2} \right) \\
+ H1(t) \cdot \left(VH1 + \frac{VPH1}{KH1} \right) + H2(t) \cdot \left(VH2 + \frac{VPH2}{KH2} \right) + S(t) \cdot VS \\
+ SP(t) \cdot VSP + PIPE(t) \cdot VPIPE + TCW1(t) \cdot VCW1 \\
+ TCW2(t) \cdot VCW2 + TCH1(t) \cdot VCH1 \\
+ TCH2(t) \cdot VCH2 + TWH1(t) \cdot \left(VWH1 + \frac{VPW1}{KW1} \cdot \sum_{i=1}^{LWH1} \frac{1}{(1+R)^{i-1}} \right) \\
+ TWH2(t) \cdot \left(VWH2 + \frac{VPW2}{KW2} \cdot \sum_{i=1}^{LWH2} \frac{1}{(1+R)^{i-1}} \right) \\
+ TWC1(t) \cdot VWC1 + TWC2(t) \cdot VWC2 \\
+ THC1(t) \cdot VHC1 + THC2(t) \cdot VHC2 + THW1(t) \cdot VHW1 \\
+ THW2(t) \cdot VHW2 \left. \right\} .
\end{aligned}$$

This concludes our discussion of the core model. Although not implementable, it is easily comprehensible. Note that all the structural equations as well as the objective function are linear in all the variables. By imposing additional assumptions on the interactions defined by the core model, we will create the S/PB model, to which we will append some additional constraints.

D. THE STOCKPILE/PRODUCTION BASE MODEL

Although it is feasible to structure the S/PB model as a completely time-stepped model, similar to the core model, the result of long Build-up, Steady-state and Mobilization/War periods combined with reasonably short time steps would be a model much too unwieldy for analytical purposes. Indeed, such a model probably could be handled by only the largest computers.

We therefore have built the S/PB model as a hybrid, wherein the Build-up and Steady-state periods have been simplified by aggregation so that all the activities during those periods, no matter how long they are, can be described by comparatively few variables. This allows us to expand the detail of the model during the Mobilization/War period where a true time-stepped approach is used.

1. The Build-Up Period

The Build-up period is distinguished by the acquisition of resources: capital equipment and ammunition. These are added to resources already owned. We denote by NPURCH the number of time steps in the Build-up period. The assumptions behind the Build-up period include:

- (1) The demand for ammunition during this period is constant over time.
- (2) The domestic and in-theater ammunition stockpiles are essentially indistinguishable; that is, they may be considered as a single ammunition reservoir.
- (3) Because the Build-up period occurs during peacetime, we assume that ammunition is produced at a single production rate (presumably the most economical rate). Therefore only cold stocks (for storage) and warm stocks (for production) are active during the Build-up period. Hot stocks do not actively appear.
- (4) The longer time delays involved in the acquisition of new capital are taken into account while the smaller time delays involved in transferring capital between producing and nonproducing states are disregarded, except for the purpose of discounting costs.

In order to make the description and equations simpler, we will first describe the Build-up period as if there were no time delay in acquiring new capital and then in the final part of this section we will describe the effects of considering that time delay.

We divide the purchases of capital into two categories. The first category is that capital purchased for eventual use,

but which, for the Build-up period, will be maintained in cold stocks. The second category is that capital purchased for the purpose of creating the ammunition stockpile and for satisfying demand during this period. This latter category of capital will therefore be maintained in warm stocks. The distinct purposes of these categories of capital suggest that there should be no transfer of capital between them during the Build-up period, and we will, in fact, assume this. With this idea in mind, we will refer to the "purchase of cold capital" as the purchase of that capital intended for cold stocks, and to the "purchase of warm capital" as the purchase of that capital intended for warm stocks. Recalling the core model, it is evident that the "purchase of warm capital" involves two steps: the purchase of capital and its transfer from cold to warm stocks.

a. Purchase of Cold Capital

In order to succeed in our effort to limit the number of variables required to describe the Build-up period, we must select, *a priori*, a family of purchase trends over time. For the purchase of cold capital, we allow only linear purchase patterns. Examples of linear purchase patterns for type 1 capital are depicted in Figure 2.

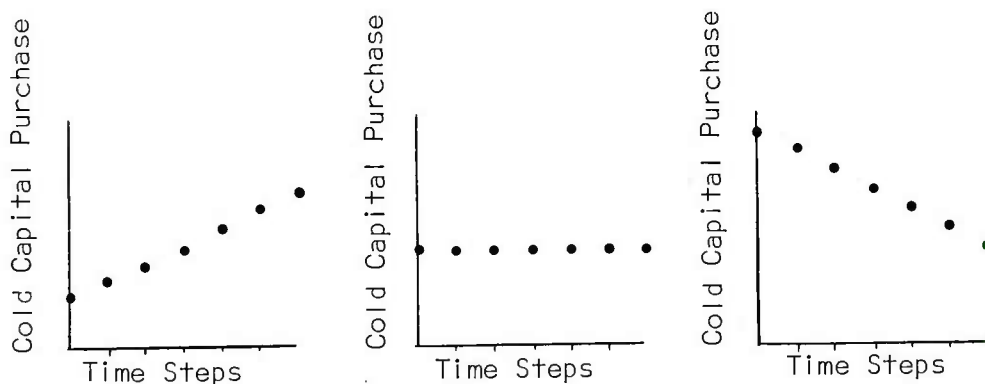


Figure 2. LINEAR PURCHASE PATTERNS

The horizontal axes in Figure 2 show the time steps of the Build-up period. The vertical axes all measure the amount of type 1 capital purchased. It is clear why these are called linear purchase patterns. Figure 3 illustrates a purchase pattern not permitted.

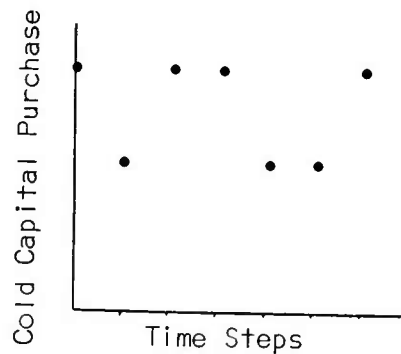


Figure 3. DISALLOWED PURCHASE PATTERN

For the purpose of this discussion, let us assume that the first time step of this period is denoted by $t = 1$. The last is therefore $t = \text{NPURCH}$. The S/PB model variables that describe the family of cold capital purchase patterns are:

- BC1 = the amount of type 1 cold capital purchased at time step $t = 1$
- BC2 = the amount of type 2 cold capital purchased at time step $t = 1$
- SLPPC1 = the positive component of the slope of the type 1 cold capital purchase pattern
- SLPNC1 = the negative component of the slope of the type 1 cold capital purchase pattern
- SLPPC2 = the positive component of the slope of the type 2 cold capital purchase pattern
- SLPNC2 = the negative component of the slope of the type 2 cold capital purchase pattern.

The type 1 cold capital purchase at any time step t of

the Build-up period is therefore

$$BC1 + (t-1) \cdot (SLPPC1-SLPNC1)$$

and, similarly, the type 2 cold capital purchased at any time step t is

$$BC2 + (t-1) \cdot (SLPPC2-SLPNC2) .$$

The reason we require the slopes be divided into positive and negative components is to maintain the nonnegativity of all model variables.

The total amount of cold capital at the end of the Build-up period is the sum of all the purchases plus any original cold capital existing before time step $t = 1$. Note that capital purchased during different time steps suffers varying deterioration by the end of the Build-up period. Capital purchased during time step $t = 1$ as well as original capital has deteriorated for $(NPURCH-1)$ time steps while capital purchased during time step $t = NPURCH$ has not deteriorated at all by the end of the Build-up period.

Table 1 illustrates how the total cold capital at the end of the Build-up period is determined. In this table B stands for $BC1$, S for $(SLPPC1-SLPNC1)$ and O for the original type 1 cold capital.

The term $DC1$, or course, is the type 1 cold capital deterioration factor we have already encountered in the core model.

A similar progression applies to type 2 cold capital purchases.

Let

$OCOLD1$ = the amount of original type 1 cold capital and

$OCOLD2$ = the amount of original type 2 cold capital.

Table 1. COLD CAPITAL ACCRUAL

Time Step	Capital Purchased	Capital on Hand
1	B	0+B
2	B+S	B+S + (1-DC1)(0+B)
3	B+2S	B+2S + (1-DC1)(B+S) + (1-DC1) ² (0+B)
4	B+3S	B+3S + (1-DC1)(B+2S) + (1-DC1) ² (B+S) + (1-DC1) ³ (0+B)
⋮	⋮	
⋮	⋮	
NPURCH	B+(NPURCH-1)·S	$B \left[\sum_{i=1}^{NPURCH} (1-DC1)^{i-1} \right] + S \left[\sum_{i=1}^{NPURCH-1} i(1-DC1)^{NPURCH-1-i} \right]$

Then the amounts of type 1 and type 2 cold capital at the end of the Build-up period are given by

$$(10) \quad BC1 \cdot \left[\sum_{i=1}^{NPURCH} (1-DC1)^{i-1} \right] + (SLPPC1-SLPNC1) \cdot \left[\sum_{i=1}^{NPURCH-1} i(1-DC1)^{NPURCH-1-i} \right] \\ + OCOLD1 \cdot (1-DC1)^{NPURCH-1}$$

$$(11) \quad BC2 \cdot \left[\sum_{i=1}^{NPURCH} (1-DC1)^{i-1} \right] + (SLPPC2-SLPNC2) \cdot \left[\sum_{i=1}^{NPURCH-1} i(1-DC2)^{NPURCH-1-i} \right] \\ + OCOLD2 \cdot (1-DC2)^{NPURCH-1}$$

b. Purchase of Warm Capital

Because the purchase of warm capital is tied to the production of ammunition, the S/PB model allows not only the linear purchase patterns already discussed, but also additional purchases for the first time step only. The motivation behind this additional degree of freedom is that warm capital purchased during the latter stages of the Build-up period can produce

ammunition for only a relatively short time. Therefore, the model allows one to look at scenarios in which the maximum use can be obtained from warm capital; that is, when all the warm capital is purchased at the beginning of the Build-up period. Figure 4 illustrates permissible warm capital purchase patterns.

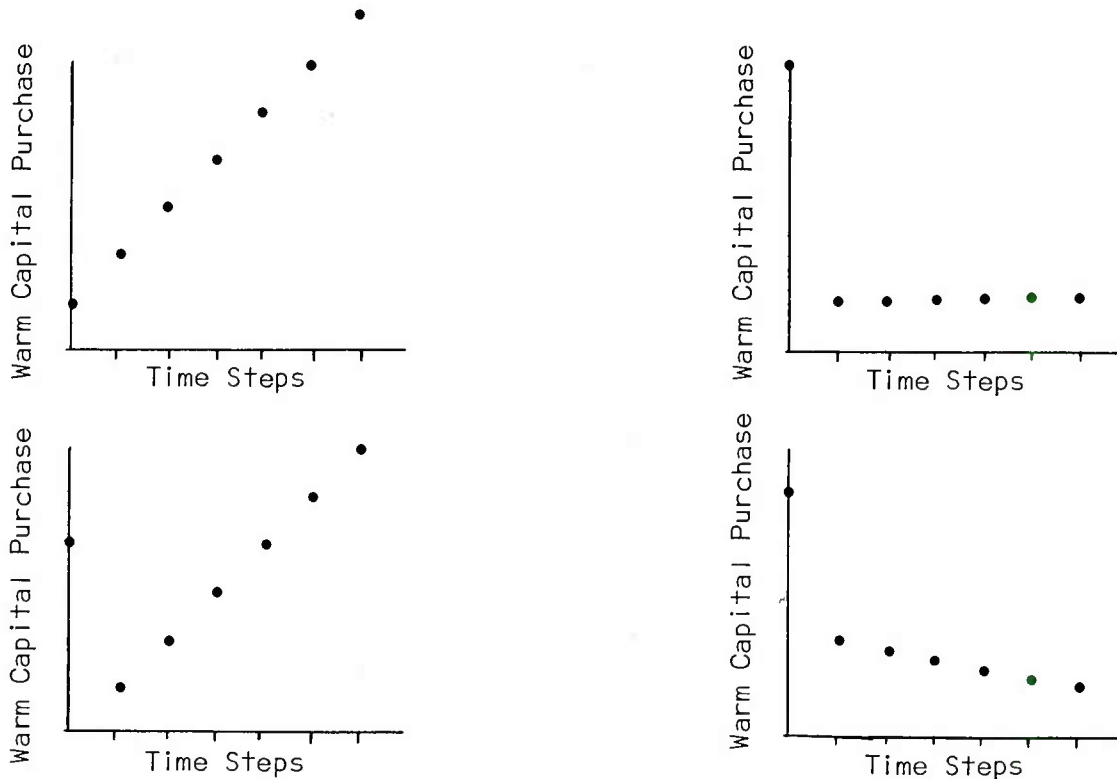


Figure 4. ALLOWABLE WARM CAPITAL PURCHASES

The model variables that determine this family of purchase patterns are:

- BW1 = the amount of type 1 warm capital purchased during time step 1 as part of the linear portion of the purchase pattern
- BW2 = the amount of type 2 warm capital purchased during time step 1 as part of the linear portion of the purchase pattern

$IBW1$ = the amount of type 1 warm capital purchased during time step 1 in addition to $BW1$
 $IBW2$ = the amount of type 2 warm capital purchased during time step 1 in addition to $BW2$
 $SLPPW1$ = the positive component of the slope of the linear portion of the type 1 warm capital purchase pattern
 $SLPNW1$ = the negative component of the slope of the linear portion of the type 1 warm capital purchase pattern
 $SLPPW2$ = the positive component of the slope of the linear portion of the type 2 warm capital purchase pattern
 $SLPNW2$ = the negative component of the slope of the linear portion of the type 2 warm capital purchase pattern.

Therefore, at time step $t = 1$, the amounts of types 1 and 2 warm capital purchased are, respectively

$$BW1 + IBW1$$

and

$$BW2 + IBW2$$

while for time steps t between $t = 2$ and $t = NPURCH$, the amounts of warm capital purchased are

$$BW1 + (t-1) \cdot (SLPPW1 - SLPNW1)$$

and

$$BW2 + (t-1) \cdot (SLPPW2 - SLPNW2).$$

The amounts of warm capital at the end of the Build-up period are given by expressions similar to those for cold capital. The only differences are the $IBW1$ and $IBW2$ terms which can clearly be handled the same way as original warm capital. Let

$OWARM1$ = the amount of original type 1 warm capital, and
 $OWARM2$ = the amount of original type 2 warm capital.

Then the amounts of type 1 and type 2 warm capital at the end of the Build-up period are given by the following expressions:

$$(12) \quad BW1 \cdot \left[\sum_{i=1}^{NPURCH} (1-DW1)^{i-1} \right] + (SLPPW1-SLPNW1) \cdot \left[\sum_{i=1}^{NPURCH-1} i(1-DW1)^{NPURCH-1-i} \right] \\ + (IBW1 + OWAR1) \cdot (1-DW1)^{NPURCH-1}$$

$$(13) \quad BW2 \cdot \left[\sum_{i=1}^{NPURCH} (1-DW2)^{i-1} \right] + (SLPPW2-SLPNW2) \cdot \left[\sum_{i=1}^{NPURCH-1} i(1-DW2)^{NPURCH-1-i} \right] \\ + (IBW2 + OWAR2) \cdot (1-DW2)^{NPURCH-1}$$

As warm capital is purchased, ammunition is produced. Some of this ammunition goes to satisfy peacetime demand, another portion is lost to deterioration. The ammunition remaining at the end of the Build-up period can be determined using much the same approach illustrated by Table 1, with the inclusion of ammunition production and deterioration, and the satisfaction of ammunition demands. If

OMUN = the amount of original ammunition,

BPDEM = the demand for ammunition during each time step of the Build-up period,

then the size of the ammunition stockpile at the end of the Build-up period is

$$(14) \quad \frac{BW1}{KW1} \cdot \left[\sum_{j=1}^{NPURCH} (1-DS)^{NPURCH-j} \cdot \left\{ \sum_{i=1}^j (1-DW1)^{i-1} \right\} \right] \\ + \frac{BW2}{KW2} \cdot \left[\sum_{j=1}^{NPURCH} (1-DS)^{NPURCH-j} \cdot \left\{ \sum_{i=1}^j (1-DW2)^{i-1} \right\} \right] \\ + \frac{(SLPPW1-SLPNW1)}{KW1} \cdot \left[\sum_{j=1}^{NPURCH} (1-DS)^{NPURCH-j} \cdot \left\{ \sum_{i=1}^{j-1} i(1-DW1)^{j-1-i} \right\} \right] \\ + \frac{(SLPPW2-SLPNW2)}{KW1} \cdot \left[\sum_{j=1}^{NPURCH} (1-DS)^{NPURCH-j} \cdot \left\{ \sum_{i=1}^{j-1} i(1-DW2)^{j-1-i} \right\} \right]$$

(continued on next page)

$$\begin{aligned}
& + \frac{(IBW1+OWARM1)}{KW1} \cdot \left[\sum_{i=1}^{NPURCH-1} (1-DW1)^{NPURCH-1-i} \cdot (1-DS)^i \right] \\
& + \frac{(IBW2+OWARM2)}{KW2} \cdot \left[\sum_{i=1}^{NPURCH-1} (1-DW2)^{NPURCH-1-i} \cdot (1-DS)^i \right] \\
& - BPDEM \cdot \left[\sum_{j=1}^{NPURCH-1} (1-DS)^{j-1} \right] + OMUN \cdot (1-DS)^{NPURCH-1} .
\end{aligned}$$

Note: In the above expression, and throughout this paper, we will adopt the convention that in summation of the form

$\sum_{i=a}^b f(i)$, where $b < a$, is equal to zero.

c. Feasibility Consideration

Certain constraints are imposed on these variables to ensure that the purchase patterns are feasible. In particular, we demand that the amounts of capital purchased during any time step of the Build-up period are nonnegative. This can be ensured by the nonnegativity of the model variables and by the following constraints:

$$(15) \quad BC1 + (NPURCH-1) \cdot (SLPPC1-SLPNC1) \geq 0$$

$$(16) \quad BC2 + (NPURCH-1) \cdot (SLPPC2-SLPNC2) \geq 0$$

$$(17) \quad BW1 + (NPURCH-1) \cdot (SLPPW1-SLPNW1) \geq 0$$

$$(18) \quad BW2 + (NPURCH-1) \cdot (SLPPW2-SLPNW2) \geq 0 .$$

We also require that the warm capital purchased also be able to satisfy Build-up period demand for ammunition. This will generally be ensured by requiring that production be sufficient to satisfy this demand at both the beginning and end of the Build-up period. These constraints take the form

$$(19) \quad \frac{1}{KW1}(IBW1+BW1+OWARM1) + \frac{1}{KW2} (IBW2+BW2+OWARM2) \geq BPDEM$$

$$(20) \quad \frac{1}{KW1} \cdot \langle 12 \rangle + \frac{1}{KW2} \cdot \langle 13 \rangle \geq BPDEM$$

where $\langle 12 \rangle$ stands for expression (12) above and $\langle 13 \rangle$ stands for expression (13).

d. Costs

In this section we list the costs associated with each variable of the Build-up period. Because we have compressed the core model variables into the fewer Build-up period variables of the S/PB model, each variable will have associated with it two or more costs from the core model.

BC1

Two costs are associated with BC1. The first accounts for the actual purchase of type 1 capital and the second specifies the costs of maintaining that capital, taking into account the fact that some of that capital is deteriorating.

The unit purchase costs over the Build-up period are simply

$$(21) \quad VPC1 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^{i-LP1}} \cdot$$

This is because, during each time step t , the costs of purchasing capital through this variable are just

$$BC1 \cdot VPC1/(1+R)^{t-LP1} \cdot$$

This expression implies that we discount costs beginning with time step $t = 1$, a convention we will maintain throughout this

paper. Note that we have corrected the costs for the time lag LPl connected with the purchase of type 1 capital.

The second cost is that associated with maintaining the cold capital stocks contributed by BC1. Table 2 lists the cold stock level, over time, contributed by the BC1, taking deterioration into account.

Table 2. COLD STOCKS CONTRIBUTED BY BC1

Time Step	Stock Level
1	BC1
2	BC1 + (1-DC1)BC1
3	BC1 + (1-DC1)BC1 + (1-DC1) ² · BC1
·	·
·	·
·	·
NPURCH	BC1 $\left[\sum_{i=1}^{NPURCH} (1-DC1)^{i-1} \right]$

Therefore the unit cost of maintaining the portion of the type 1 cold stock contributed by BC1 is

$$(22) \quad VC1 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \left[\sum_{j=1}^i (1-DC1)^{j-1} \right]$$

so that the total unit cost associated with BC1 is just

$$(23) \quad \langle 21 \rangle + \langle 22 \rangle ;$$

that is, the total cost attributable to BC1 is

$$BC1 \cdot \langle 23 \rangle .$$

BC2

The unit cost of BC2 can be calculated in precisely the same manner as those of BC1. The result is

$$(24) \quad VPC2 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1-R)^{i-LP2}} + VC2 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \left[\sum_{j=1}^i (1-DC2)^{j-1} \right].$$

SLPPC1-SLPNC1

The costs associated with the quantity (SLPPC1-SLPNC1) also comprise purchase and stockpile maintenance costs. It is not difficult to see that the unit purchase costs are

$$(25) \quad VPC1 \cdot \sum_{i=1}^{NPURCH} \frac{i-1}{(1+R)^{i-LP1}}.$$

To determine the stockpile maintenance cost contributed by (SLPPC1-SLPNC1), consider Table 3. Note that if the difference (SLPPC1-SLPNC1) is negative, the stock levels contributed are negative, which is perfectly reasonable, since these are only part of the total stocks.

Table 3. COLD STOCKS CONTRIBUTED BY (SLPPC1-SLPNC1)

Time Step	Stock Level
1	0
2	SLPPC1 - SLPNC1
3	2(SLPPC1-SLPNC1) + (1-DC1)(SLPPC1-SLPNC1)
⋮	⋮
⋮	⋮
NPURCH	(SLPPC1-SLPNC1) $\left[\sum_{i=1}^{NPURCH-1} i(1-DC1)^{NPURCH-1-i} \right]$

Therefore, the unit stockpile maintenance costs are

$$(26) \quad VC1 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \left[\sum_{j=1}^{i-1} j(1-DC1)^{i-1-j} \right]$$

so that the total unit cost associated with (SLPPC1-SLPNC1) is

$$(27) \quad \langle 25 \rangle + \langle 26 \rangle .$$

SLPPC2-SLPNC2

An analysis similar to the one above shows the unit cost associated with (SLPPC2-SLPNC2) to be

$$(28) \quad VPC2 \cdot \sum_{i=1}^{NPURCH} \frac{i-1}{(1+R)^{i-LP2}} +$$

$$VC2 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \left[\sum_{j=1}^{i-1} j(1-DC2)^{i-1-j} \right] .$$

IBW1

The variables describing warm capital purchases are associated with the following costs.

- (1) The cost of purchasing the capital
- (2) The cost of transferring capital from cold to warm stocks
- (3) The cost of maintaining the warm stocks
- (4) The costs of ammunition production
- (5) The costs of maintaining the ammunition stockpile.

To determine the costs contributed by IBW1, first consider Table 4. The unit purchase cost associated with IBW1 is clearly

Table 4. RESOURCES CONTRIBUTED BY IBW1

Time Step	Warm Stocks Contributed by IBW1	Ammunition Production Contributed by IBW1	Ammunition Stockpile Contributed by IBW1
1	$IBW1$	$\frac{IBW1}{KWT}$	$\frac{IBW1}{KWT}$
2	$IBW1 \cdot (1-DW1)$	$\frac{IBW1}{KWT} \cdot (1-DW1)$	$\frac{IBW1}{KWT} \cdot (1-DW1) + \frac{IBW1}{KWT} \cdot (1-DS)$
3	$IBW1 \cdot (1-DW1)^2$	$\frac{IBW1}{KWT} \cdot (1-DW1)^2$	$\frac{IBW1}{KWT} \cdot (1-DW1)^2 + \frac{IBW1}{KWT} \cdot (1-DW1)(1-DS) + \frac{IBW1}{KWT}(1-DS)^2$
.	.	.	.
.	.	.	.
.	.	.	.
NPURCH	$IBW1 \cdot (1-DW1)^{NPURCH-1}$	$\frac{IBW1}{KWT} \cdot (1-DW1)^{NPURCH-1}$	$\frac{IBW1}{KWT} \sum_{i=1}^{NPURCH-1} (1-DS)^i (1-DW1)^{NPURCH-1-i}$

$$(29) \quad VPC1 \cdot \frac{1}{(1+R)^{1-LCW1-LP1}} \cdot$$

Note that the time required to transfer the capital to warm stocks has been factored into the discount coefficient.

The unit cost of the cold to warm transfer is

$$(30) \quad VCW1 \cdot \frac{1}{(1+R)^{1-LCW1}} \cdot$$

The warm stockpile maintenance unit cost can be determined from Table 4 to be

$$(31) \quad VW1 \cdot \sum_{i=1}^{NPURCH} \frac{(1-DW1)^{i-1}}{(1+R)^i} \cdot$$

The cost per unit of ammunition production contributed by IBW1 is given by

$$(32) \quad \frac{VPW1}{KW1} \cdot \sum_{i=1}^{NPURCH} \frac{(1-DW1)^{i-1}}{(1+R)^i} \cdot$$

Finally, the unit cost of maintaining the component of warm stocks contributed by IBW1 is

$$(33) \quad \frac{VS}{KW1} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \left[\sum_{j=1}^{i-1} (1-DW1)^j (1-DS)^{i-1-j} \right] \cdot$$

The sum of these

$$(34) \quad \langle 29 \rangle + \langle 30 \rangle + \langle 31 \rangle + \langle 32 \rangle + \langle 33 \rangle$$

constitutes the total unit cost associated with IBW1.

IBW2

The same logic yields the unit cost associated with IBW2:

$$(35) \quad \frac{VPC2}{(1+R)^{1-LCW2-LP2}} + \frac{VCW2}{(1+R)^{1-LCW2}} + VW2 \cdot \sum_{i=1}^{NPURCH} \frac{(1-DW2)^{i-1}}{(1+R)^i} \\ + \frac{VPW2}{KW2} \cdot \sum_{i=1}^{NPURCH} \frac{(1-DW2)^{i-1}}{(1+R)^i} \\ + \frac{VS}{KW2} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \left[\sum_{j=1}^{i-1} (1-DW2)^j (1-DS)^{i-1-j} \right] .$$

BW1

Consider the contributions by BW1 listed in Table 5. Certainly, the unit purchase cost is

$$(36) \quad VPC1 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^{i-LCW1-LP1}}$$

and the unit transfer cost is

$$(37) \quad VCW1 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^{i-LCW1}} .$$

From Table 5, one can determine the unit stock maintenance to be

$$(38) \quad VW1 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \left[\sum_{j=1}^i (1-DW1)^{j-1} \right]$$

and the unit ammunition production cost is

Table 5. RESOURCES CONTRIBUTED BY BW1

Time Step	Warm Stocks Contributed by BW1	Ammunition Production Contributed by BW1	Ammunition Stockpile Contributed by BW1
1	BW1	$\frac{BW1}{KWT}$	$\frac{BW1}{KWT}$
2	$BW1 + (1-DW1) \cdot BW1$	$\frac{BW1}{KWT} \cdot [1 + (1-DW1)]$	$\frac{BW1}{KWT} \cdot [1 + (1-DW1)] + \frac{BW1}{KWT} \cdot (1-DS)$
3	$BW1 + (1-DW1) \cdot BW1 + (1-DW1)^2 \cdot BW1$	$\frac{BW1}{KWT} \cdot [1 + (1-DW1) + (1-DW1)^2]$	$\frac{BW1}{KWT} [1 + (1-DW1) + (1-DW1)^2] + \frac{BW1}{KWT} [1 + (1-DW1)]$
.	.	.	$\leftarrow (1-DS) + \frac{BW1}{KWT} (1-DS)^2$
.	.	.	.
NPURCH	$BW1 \cdot \left[\sum_{i=1}^{NPURCH} (1-DW1)^{i-1} \right]$	$\frac{BW1}{KWT} \cdot \left[\sum_{i=1}^{NPURCH} (1-DW1)^{i-1} \right]$	$\frac{BW1}{KWT} \sum_{i=1}^{NPURCH} (1-DS)^{NPURCH-i} \left[\sum_{j=1}^i (1-DW1)^{j-1} \right]$

$$(39) \quad \frac{VPW1}{KW1} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \left[\sum_{j=1}^i (1-DW1)^{j-1} \right] .$$

Finally, the unit stockpile maintenance cost associated with BW1 is

$$(40) \quad \frac{VS}{KW1} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \sum_{j=1}^i (1-DS)^{i-j} \cdot \left[\sum_{k=1}^j (1-DW1)^{k-1} \right] .$$

Thus the total unit cost of BW1 is

$$(41) \quad \langle 36 \rangle + \langle 37 \rangle + \langle 38 \rangle + \langle 39 \rangle + \langle 40 \rangle .$$

BW2

The unit cost associated with BW2 is

$$(42) \quad VPC2 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^{i-LCW2-LP2}} + VCW2 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^{i-LCW2}} \\ + VW2 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \left[\sum_{j=1}^i (1-DW2)^{j-1} \right] \\ + \frac{VPW2}{KW2} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \left[\sum_{j=1}^i (1-DW2)^{j-1} \right] \\ + \frac{VS}{KW2} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \sum_{j=1}^i (1-DS)^{i-j} \left[\sum_{k=1}^j (1-DW2)^{k-1} \right] .$$

SLPPW1-SLPNW1

Table 6 gives the progression of resources contributed over time by the difference (SLPPW1-SLPNW1).

The unit purchase cost is simply

Table 6. RESOURCES CONTRIBUTED BY (SLPPWT-SLPNWT)

$$(43) \quad VPC1 \cdot \sum_{i=1}^{NPURCH} \frac{i-1}{(1+R)^{i-LCW1-LP1}}$$

and the unit transfer cost is similarly

$$(44) \quad VCW1 \cdot \sum_{i=1}^{NPURCH} \frac{i-1}{(1+R)^{i-LCW1}} .$$

From Table 6, one can determine the unit stockpile maintenance cost to be

$$(45) \quad VW1 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \sum_{j=1}^{i-1} j(1-DW1)^{i-1-j}$$

while the unit ammunition production cost is

$$(46) \quad \frac{VPW1}{KW1} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \sum_{j=1}^{i-1} j(1-DW1)^{i-1-j} .$$

Lastly, the unit ammunition stockpile maintenance cost contributed by (SLPPW1-SLPNW1) is

$$(47) \quad \frac{VS}{KW1} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \sum_{j=1}^i (1-DS)^{i-j} \cdot \sum_{k=1}^{j-1} k(1-DW1)^{j-1-k}$$

The total unit cost associated with (SLPPW1-SLPNW1) is therefore

$$(48) \quad \langle 43 \rangle + \langle 44 \rangle + \langle 45 \rangle + \langle 46 \rangle + \langle 47 \rangle .$$

SLPPW2 - SLPNW2

Finally, the total unit cost associated with (SLPPW2-SLPNW2) is

$$\begin{aligned}
 (49) \quad & VPC2 \cdot \sum_{i=1}^{NPURCH} \frac{i-1}{(1+R)^{i-LCW2-LP2}} + VCW2 \cdot \sum_{i=1}^{NPURCH} \frac{i-1}{(1+R)^{i-LCW2}} \\
 & + VW2 \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \sum_{j=1}^{i-1} j(1-DW2)^{i-1-j} \\
 & + \frac{VPW2}{KW2} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \sum_{j=1}^{i-1} j(1-DW2)^{i-1-j} \\
 & + \frac{VS}{KW2} \cdot \sum_{i=1}^{NPURCH} \frac{1}{(1+R)^i} \cdot \sum_{j=1}^i (1-DS)^{i-j} \cdot \sum_{k=1}^{j-1} k(1-DW2)^{j-1-k} .
 \end{aligned}$$

It should be noted that there are additional costs associated with the Build-up period that do not depend on the variable values. These are the costs of maintaining the original cold and warm capital stocks, the costs of ammunition production by the original warm stocks, and the cost of maintaining the original ammunition stockpile as well as that produced by original warm capital. There are also savings to be considered because ammunition that goes to satisfy demand during this period need not be maintained. These costs and savings, however, are fixed. They depend only on original resource levels and on the demand for ammunition during the Build-up period; therefore, they are explicitly excluded from the objective function of the S/PB model.

e. Time Delay in Capital Acquisition

So far we have described the Build-up period as if there were no time delay in acquiring capital. For most problems

there will be some time delay which we denote by NLAG and explicitly define as the initial time delay from the decision to buy new capital to the time it can first produce. This delay may be different from the time delay for acquiring capital during the Mobilization/War period which will be discussed later. The general effect of the NLAG delay on the model is that during the first NLAG periods of the Build-up period new capital is not yet available, stocks are being produced by the initial warm capital and consumed, and costs are accruing due to production and maintenance. The important thing to realize is that these factors are not affected by anything over which we have a choice and thus are not part of the mathematical programming model itself. The results of the decision to buy new capital are not felt until time period $NLAG+1$, when new capital first arrives. The NLAG period does affect the mathematical programming model indirectly by determining the amount of capital and stocks at time $NLAG+1$. The amount of stocks at the end of NLAG periods is given by Equation (14) with all variables relating to capital buys set to zero.

2. The Steady-State Period

At the end of the Build-up period, we enter the Steady-state period, in which the chief actions taken are those required to maintain the capital and ammunition determined during the Build-up period. The basic unit of time is the time step, and the Steady-state period is assumed to be NSS time steps long. NSS is allowed to be zero, by which the user indicates that the scenario moves directly from the Build-up period to the Mobilization/War period.

a. Steady-State Variables and Equations

As before, we assume that the demand for ammunition during this period is constant over time, that no hot capital appears,

that time lags appear only in the costs, and that the domestic and in-theater ammunition stockpiles are essentially indistinguishable.

Among the variables of this period are

ES = the total amount of ammunition held in stockpiles during this period

EC1 = the amount of type 1 cold capital held during this period

EC2 = the amount of type 2 cold capital held during this period

EW1 = the amount of type 1 warm capital held during this period

EW2 = the amount of type 2 warm capital held during this period.

An equation that must obviously hold is

$$(50) \quad ES = \langle 14 \rangle ;$$

that is, the ammunition held during this period is equal to that acquired during the Build-up period. In order for this to be constant over the period, it must be true that

$$(51) \quad \frac{EW1}{KW1} + \frac{EW2}{KW2} = SSDEM + ES \cdot DS$$

where

SSDEM = the demand for ammunition per time step during the Steady-state period.

Equation (51) is a statement that the total production, per time step, is precisely that necessary to meet demand and to replace the ammunition that has deteriorated during each previous time step. In case NSS = 0, there will be no demand or deterioration and this equation will not appear in the model.

Because this period is a peacetime period, we must ensure that the amount of warm capital acquired during the Build-up period is sufficient to maintain the stockpile level. Therefore, when NSS > 0, we require that

$$(52) \quad EW1 \leq \langle 12 \rangle$$

and

$$(53) \quad EW2 \leq \langle 13 \rangle .$$

Note that this implies that cold capital acquired during the Build-up period is acquired solely for the needs of the Mobilization/War period. In other words, the preparation during the Build-up period must take the Steady-state period into account.

When $NSS = 0$, we replace (52) and (53) by

$$(54) \quad EW1 = \langle 12 \rangle$$

$$(55) \quad EW2 = \langle 13 \rangle$$

in order to tie together the Build-up and the Mobilization/War periods.

In general, more capital will be in warm stocks at the end of the Build-up period than will be required during the Steady-state period. The excess warm stocks are put into cold stocks for future use:

$$(56) \quad EC1 + EW1 = \langle 10 \rangle + \langle 12 \rangle$$

$$(57) \quad EC2 + EW2 = \langle 11 \rangle + \langle 13 \rangle .$$

To permit the model to enter the Mobilization/War period with distinct domestic and in-theater ammunition stockpiles, we perform, during this period, what we shall call the prepositioning of ammunition through the use of the following variable.

EPREP = the amount of ammunition explicitly prepositioned into the in-theater stockpile during the Steady-state period.

The only structural constraint on this prepositioning is

$$(58) \quad EPREP \leq ES ;$$

that is, one cannot preposition more ammunition than one has.

The amount of ammunition remaining in the domestic stockpile is then

$$(59) \quad ES - EPREP.$$

b. Costs

The costs of this period include those of explicit activities, such as ammunition production, as well as those of implicit activities, such as the purchase of capital to replace that which deteriorates. The unit costs associated with each variable of the Steady-state period are as follows.

EC1

The maintenance cost of one unit of EC1 throughout the Steady-state period is clearly

$$(60) \quad VC1 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i+NPURCH}} \cdot$$

The NPURCH term in the exponent of the denominator represents the fact that the first time step of the Steady-state period is time step $t = NPURCH + 1$.

Because type 1 cold capital deteriorates by an amount $EC1 \cdot DC1$ during each time step, we must include the cost of purchasing capital to maintain the type 1 cold capital stocks at an even level. This cost, per unit of EC1, is

$$(61) \quad VPC1 \cdot DC1 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i-LP1+NPURCH}},$$

so that the total unit cost associated with EC1 is

$$(62) \quad \langle 60 \rangle + \langle 61 \rangle.$$

EC2

In a like manner, the unit cost of EC2 is

$$(63) \left(VC2 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i+NPURCH}} \right) + \left(VPC2 \cdot DC2 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i-LP2+NPURCH}} \right).$$

EW1

The cost associated with Steady-state warm capital comprises

- (1) the purchase of replacement capital to correct deterioration
- (2) the cost of transferring that capital to warm stocks
- (3) the cost of maintaining the warm stocks, and
- (4) the cost of producing ammunition.

In order, these unit costs are, for type 1 capital

$$(63) \quad VPC1 \cdot DW1 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i-LCW1-LP1+NPURCH}}$$

$$(64) \quad VCW1 \cdot DW1 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i-LCW1+NPURCH}}$$

$$(65) \quad VW1 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i+NPURCH}}$$

$$(66) \quad \frac{VPW1}{KW1} \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i+NPURCH}}.$$

The total unit cost of EW1 is then

$$(67) \quad \langle 63 \rangle + \langle 64 \rangle + \langle 65 \rangle + \langle 66 \rangle.$$

EW2

The total unit cost for type 2 warm capital during the Steady-state period is

$$\begin{aligned} (68) \quad & VPC2 \cdot DW2 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i-LCW2-LP2+NPURCH}} \\ & + VCW2 \cdot DW2 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i-LCW2+NPURCH}} \\ & + VW2 \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i+NPURCH}} \\ & + \frac{VPW2}{KW2} \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i+NPURCH}} . \end{aligned}$$

ES

The cost of maintaining the Steady-state stockpile, per unit, is

$$(69) \quad VS \cdot \sum_{i=1}^{NSS} \frac{1}{(1+R)^{i+NPURCH}} .$$

EPREP

We assume, for costing purposes, that the prepositioned stocks are separated from the ammunition stockpile during the last time step of the Steady-state period. The user must assess this one-time cost and supply it as the parameter VPREP which is then discounted. The unit cost associated with the variable EPREP is therefore

$$(70) \quad VPREP \cdot \frac{1}{(1+R)^{NSS+NPURCH}} .$$

3. Mobilization/War Period

The Mobilization/War period, which is assumed to last ISTEP time steps, follows the Steady-state period, except when $NSS = 0$, which places the Mobilization/War period directly after the Build-up period (although the Steady-state variables still appear in the model).

The structural equations of this period closely resemble the core model--this period is explicitly time stepped--except that those pertaining to the earlier time steps of this period are modified to provide the interface with the previous two periods. In particular, stock and stockpile levels at the start of this period must reflect the levels at the end of the Steady-state period and also the transfer variables in the initial stages of this period must be set to appropriate values. As with the core model, each of the following equations represents a sequence of equations as t ranges from 1 to ISTEP.

a. Cold Capital Stocks

$$(71) \quad C1(t) = \langle a \rangle \cdot (1-DC1) + \langle b \rangle + \langle c \rangle + \langle d \rangle - TCH1(t) - TCW1(t)$$

where

$$\langle a \rangle = \begin{cases} EC1 & \text{if } t = 1 \\ C1(t-1) & \text{if } t \geq 2 \end{cases}$$

$$\langle b \rangle = \begin{cases} EC1 \cdot DC1 + EW1 \cdot DW1 & \text{if } 1 - NSS \leq t - LP1 \leq 0 \\ PC1(t-LP1) & \text{if } t - LP1 \geq 1 \\ 0 & \text{if } t - LP1 < 1 - NSS \end{cases}$$

$$\langle c \rangle = \begin{cases} TWCl(t-LWCl) & \text{if } t - LWCl \geq 1 \\ 0 & \text{if } t - LWCl \leq 0 \end{cases}$$

$$\langle d \rangle = \begin{cases} \text{THC1}(t - \text{LHC1}) & \text{if } t - \text{LHC1} \geq 1 \\ 0 & \text{if } t - \text{LHC1} \leq 0 \end{cases}$$

The expressions $\langle a \rangle$, $\langle b \rangle$, $\langle c \rangle$, and $\langle d \rangle$ constitute the interface between the type 1 cold capital equations of the Mobilization/War period and the previous periods. These terms reflect both the explicit activities of these periods as well as implicit ones.

Expression $\langle a \rangle$ brings the type 1 cold capital accrued during the first two periods into the Mobilization/War period. For time steps $t \geq 2$, this term reflects the cold capital of the previous time step, which is then adjusted for deterioration. However, when $t=1$, the previous type 1 cold capital is that in the Steady-state period and hence $\langle a \rangle$ is set to EC1 .

Expression $\langle b \rangle$ reflects purchases of type 1 capital. When $t - \text{LP1} \geq 1$, these purchases are those that have been generated earlier in the Mobilization/War period which are only presently entering cold stocks. If $t - \text{LP1} < 1 - \text{NSS}$, then the time lag combined with the time step is such that the purchases entering cold stocks at this time step t would have had to have been purchased during the Build-up period. We have assumed, however, that purchases during that period entered cold stocks immediately and hence have already been accounted for. Therefore, we set $\langle b \rangle = 0$. For $1 - \text{NSS} \leq t - \text{LP1} \leq 0$, the purchases are those that would have had to be purchased during the Steady-state period. Recall that Steady-state purchases are implicit activities; that is, their costs are accounted for but there is no Steady-state variable corresponding to purchases of capital. Rather, we have assumed that the purchases during the Steady-state period are precisely what is needed to maintain capital stock levels. This is clearly $\text{EC1} \cdot \text{DC1} + \text{EW1} \cdot \text{DW1}$ units of capital per time step, which we allow to be brought forward into the Mobilization/War period. In this way continuity

is provided between the Steady-state and Mobilization/War periods.

Expression $\langle c \rangle$ represents warm to cold transfer of type 1 capital. Because we have assumed that the only such transfer prior to the Mobilization/War period is that at the end of the Build-up period, which has already been explicitly included in the values of the Steady-state variables, for all time steps t for which $t - LCW1 \leq 0$, we set $\langle c \rangle = 0$. For those values of t for which $t - LCW1 \geq 1$, this transfer occurs entirely within the Mobilization/War period and so $\langle c \rangle = TWC1(t-LWC1)$.

Expression $\langle d \rangle$ stands for hot to cold transfer of type 1 capital. Because we have assumed that there is no hot capital prior to the Mobilization/War period, $\langle d \rangle$ must clearly equal 0 if $t - LHC1 \leq 0$. For all other time steps t , $\langle d \rangle = THC1(t-LHC1)$.

For type 2 cold stocks, the representative equation is

$$(72) \quad C2(t) = \langle a \rangle \cdot (1-DC2) + \langle b \rangle + \langle c \rangle + \langle d \rangle - TCH2(t) - TCW2(t)$$

where

$$\langle a \rangle = \begin{cases} EC2 & \text{if } t = 1 \\ C2(t-1) & \text{if } t \geq 2 \end{cases}$$

$$\langle b \rangle = \begin{cases} EC2 \cdot DC2 + EW2 \cdot DW2 & \text{if } 1 - NSS \leq t - LP2 \leq 0 \\ PC2(t-LP2) & \text{if } t - LP2 \geq 1 \\ 0 & \text{if } t - LP2 < 1 - NSS \end{cases}$$

$$\langle c \rangle = \begin{cases} TWC2(t-LWC2) & \text{if } t - LWC2 \geq 1 \\ 0 & \text{if } t - LWC2 \leq 0 \end{cases}$$

$$\langle d \rangle = \begin{cases} THC2(t-LHC2) & \text{if } t - LHC2 \geq 1 \\ 0 & \text{if } t - LHC2 \leq 0 \end{cases}$$

b. Warm Capital Stocks

For type 1 warm capital stocks, the appropriate equation is

$$(73) \quad W1(t) = \langle a \rangle \cdot (1-DW1) + \langle b \rangle + \langle c \rangle - TWC1(t) - TWH1(t)$$

where

$$\langle a \rangle = \begin{cases} EW1 & \text{if } t = 1 \\ W1(t-1) & \text{if } t \geq 2 \end{cases}$$

$$\langle b \rangle = \begin{cases} DW1 \cdot EW1 & \text{if } 1 - NSS \leq t - LCW1 \leq 0 \\ TCW1(t-LCW1) & \text{if } t - LCW1 \geq 1 \\ 0 & \text{if } t - LCW1 < 1 - NSS \end{cases}$$

$$\langle c \rangle = \begin{cases} THW1(t-LHW1) & \text{if } t - LHW1 \geq 1 \\ 0 & \text{if } t - LHW1 \leq 0 \end{cases}$$

The expression $\langle a \rangle$ brings the Steady-state type 1 warm capital into the Mobilization/War period during time step $t=1$. For later time steps, $\langle a \rangle$ represents the carry-over of the previous time step's warm capital.

Expression $\langle b \rangle$ stands for cold to warm capital transfer. If $t - LCW1 \geq 1$, then the entire transfer occurs during the Mobilization/War period and $\langle b \rangle = TCW1(t-LCW1)$. If $t - LCW1 < 1 - NSS$, the transfer would have had to originate in the Build-up period, during which, we have assumed, there are no such transfers. Therefore, in this case, $\langle b \rangle = 0$. If $1 - NSS \leq t - LCW1 \leq 0$, we set $\langle b \rangle$ equal to the implicit cold to warm transfer during the Steady-state period which is the $EW1 \cdot DW1$ units per time step that were needed to correct for deterioration.

Expression $\langle c \rangle$ represents hot to warm capital transfer. Prior to the Mobilization/War period, there are no hot capital stocks and so $\langle c \rangle = 0$ if $t - LHW1 \leq 0$. Otherwise, $\langle c \rangle = THW1(t-LHW1)$.

Type 2 warm capital stocks are described by Equation (74).

$$(74) \quad W2(t) = \langle a \rangle \cdot (1-DW2) + \langle b \rangle + \langle c \rangle - TWC2(t) - TWH2(t)$$

where

$$\langle a \rangle = \begin{cases} EW2 & \text{if } t = 1 \\ W2(t-1) & \text{if } t \geq 2 \end{cases}$$

$$\langle b \rangle = \begin{cases} DW2 \cdot EW2 & \text{if } 1 - NSS \leq t - LCW2 \leq 0 \\ TCW2(t-LCW2) & \text{if } t - LCW2 \geq 1 \\ 0 & \text{if } t - LCW2 < 1 - NSS \end{cases}$$

$$\langle c \rangle = \begin{cases} TWH2(t-LHW2) & \text{if } t - LHW2 \geq 1 \\ 0 & \text{if } t - LHW2 \leq 0 \end{cases}$$

c. Hot Capital Stocks

The type 1 hot capital stocks are modelled by the following equation:

$$(75) \quad H1(t) = \langle a \rangle \cdot (1-DH1) + \langle b \rangle + \langle c \rangle - THC1(t) - TWH1(t)$$

where

$$\langle a \rangle = \begin{cases} H1(t-1) & \text{if } t \geq 2 \\ 0 & \text{if } t = 1 \end{cases}$$

$$\langle b \rangle = \begin{cases} TCH1(t-LCH1) & \text{if } t - LCH1 \geq 1 \\ 0 & \text{if } t - LCH1 \leq 0 \end{cases}$$

$$\langle c \rangle = \begin{cases} TWH1(t-LWH1) & \text{if } t - LWH1 \geq 1 \\ 0 & \text{if } t - LWH1 \leq 0 \end{cases}$$

Expression $\langle a \rangle$, the hot capital carry-over, must clearly be zero when $t=1$. For $t \geq 2$, $\langle a \rangle$ is simply $H1(t-1)$. Expressions $\langle b \rangle$ and $\langle c \rangle$ represent, respectively, the type 1 cold-to-hot and warm-to-hot capital transfers. Because there is no hot

capital prior to the Mobilization/War period, we permit no transfers to hot capital to originate during previous periods. Therefore, these are zero when $t - LCH1$ and $t - LWH1$, respectively, are less than or equal to zero. Otherwise $\langle b \rangle = TCH1(t-LCH1)$ and $\langle c \rangle = TWH1(t-LWH1)$.

The corresponding equation for type 2 hot capital is:

$$(76) \quad H2(t) = \langle a \rangle \cdot (1-DH2) + \langle b \rangle + \langle c \rangle - THC2(t) - THW2(t)$$

where

$$\langle a \rangle = \begin{cases} H2(t-1) & \text{if } t \geq 2 \\ 0 & \text{if } t = 1 \end{cases}$$

$$\langle b \rangle = \begin{cases} TCH2(t-LCH2) & \text{if } t - LCH2 \geq 1 \\ 0 & \text{if } t - LCH2 \leq 0 \end{cases}$$

$$\langle c \rangle = \begin{cases} TWH2(t-LWH2) & \text{if } t - LWH2 \geq 1 \\ 0 & \text{if } t - LWH2 \leq 0 \end{cases}$$

d. Ammunition Stockpile

The interfaces for the domestic and in-theater stockpiles include the prepositioning of ammunition that occurred during the Steady-state interval. The ammunition stockpile equations are:

$$(77) \quad S(t) = \langle a \rangle \cdot (1-DS) + \frac{W1(t)}{KW1} + \frac{W2(t)}{KW2} + \frac{H1(t)}{KH1} + \frac{H2(t)}{KH2} \\ + \sum_{\substack{t-LWH1 < s \leq t \\ s \geq 1}} \frac{TWH1(s)}{KW1} + \sum_{\substack{t-LWH2 < s \leq t \\ s \geq 1}} \frac{TWH2(s)}{KW2} \\ - DD(t) - PIPE(t)$$

$$(78) \quad SP(t) = \langle b \rangle \cdot (1-DSP) + \langle c \rangle - FD(t)$$

where

$$\begin{aligned}\langle a \rangle &= \begin{cases} ES - EPREP & \text{if } t = 1 \\ S(t-1) & \text{if } t \geq 2 \end{cases} \\ \langle b \rangle &= \begin{cases} EPREP & \text{if } t = 1 \\ SP(t-1) & \text{if } t \geq 2 \end{cases} \\ \langle c \rangle &= \begin{cases} PIPE(t-LPIPE) & \text{if } t - LPIPE \geq 1 \\ 0 & \text{if } t - LPIPE \leq 0 \end{cases}\end{aligned}$$

Expressions $\langle a \rangle$ and $\langle b \rangle$ demonstrate how prepositioned ammunition is removed from the domestic stockpile and placed in the in-theater stockpile by the beginning of the Mobilization/War period.

Expression $\langle c \rangle$ is zero if $t - LPIPE \leq 0$ since we have assumed no distinction between the stockpiles, and hence no pipeline, prior to the Mobilization/War period.

e. Costs

The Mobilization/War period costs closely resemble the costs of the core model. They differ in that the discount factor must include the previous two periods and in that salvage values of ammunition held at the end of the war are permitted. This is accomplished by providing two additional cost parameters:

VSSALV = the cost of holding one unit of ammunition in the domestic stockpile during the final time step of the Mobilization/War period (if negative, this represents salvage value).

VSPALV = the cost of holding one unit of ammunition in the in-theater stockpile during the final time step of the Mobilization/War period (if negative, this represents salvage value).

The cost of each activity of the Mobilization/War period is listed in Table 7. Note that the S/PB model provides only ISTEP-1 variables to describe transfers of assets. To provide more would only permit the model to transfer assets beyond the end of the

Table 7. MOBILIZATION/WAR PERIOD COSTS

Variable	Unit Cost	Applicable Time Steps
PC1(t)	$VPC1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
PC2(t)	$VPC2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
C1(t)	$VC1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
C2(t)	$VC2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
W1(t)	$VW1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
W1(t)/KW1	$VPW1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
W2(t)	$VW2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
W2(t)/KW1	$VPW2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
H1(t)	$VH1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
H1(t)/KH1	$VPH1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
H2(t)	$VH2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
H2(t)/KH2	$VPH2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP$
S(t)	$VS/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
	$VSSALV/(1+R)^{ISTEP+NSS+NPURCH}$	$t=ISTEP$
SP(t)	$VSP/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
	$VSPALV/(1+R)^{ISTEP+NSS+NPURCH}$	$t=ISTEP$
PIPE(t)	$VPIPE/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
TCW1(t)	$VCW1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
TCW2(t)	$VCW2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
TWH1(t)	$VWH1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
	$\rightarrow + \frac{VPW1}{KW1} \cdot \frac{1}{(1+R)^{t+NSS+NPURCH}} \cdot \sum_{i=1}^{LWH1} \frac{1}{(1+R)^{i-1}}$	
TWH2(t)	$VWH2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
	$\rightarrow + \frac{VPW2}{KW2} \cdot \frac{1}{(1+R)^{t+NSS+NPURCH}} \cdot \sum_{i=1}^{LWH2} \frac{1}{(1+R)^{i-1}}$	

(continued)

Table 7. (concluded)

Variable	Unit Cost	Applicable Time Steps
TWC1(t)	$VWC1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
TWC2(t)	$VWC2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
THC1(t)	$VHC1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
THC2(t)	$VHC2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
THW1(t)	$VHW1/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$
THW2(t)	$VHW2/(1+R)^{t+NSS+NPURCH}$	$t=1, \dots, ISTEP-1$

final time step. As with the core model, warm and hot stocks have two associated costs--maintenance and ammunition production.

The total cost of the Mobilization/War period is, therefore,

$$\begin{aligned}
 (77) \quad & \sum_{t=1}^{ISTEP} \frac{1}{(1+R)^{t+NSS+NPURCH}} \left\{ PC1(t) \cdot VPC1 + PC2(t) \cdot VPC2 \right. \\
 & + C1(t) \cdot VC1 + C2(t) \cdot VC2 + W1(t) \cdot (VW1 + \frac{VPW1}{KW1}) \\
 & + W2(t) \cdot (VW2 + \frac{VPW2}{KW2}) + H1(t) \cdot (VH1 + \frac{VPH1}{KH1}) \\
 & \left. + H2(t) \cdot (VH2 + \frac{VPH2}{KH2}) \right\} \\
 & + \sum_{t=1}^{ISTEP-1} \frac{1}{(1+R)^{t+NSS+NPURCH}} \left\{ S(t) \cdot VS + SP(t) \cdot VSP \right. \\
 & + PIPE(t) \cdot VPIPE + TCW1(t) \cdot VCW1 + TCW2(t) \cdot VCW2 + TCH1(t) \cdot VCH1 \\
 & + TCH2(t) \cdot VCH2 + TWH1(t) \cdot \left\{ VWH1 + \frac{VPW1}{KW1} \cdot \sum_{i=1}^{LWH1} \frac{1}{(1+R)^{i-1}} \right\} \\
 & \left. + TWH2(t) \cdot \left\{ VWH2 + \frac{VPW2}{KW2} \cdot \sum_{i=1}^{LWH2} \frac{1}{(1+R)^{i-1}} \right\} \right\}
 \end{aligned}$$

$$\begin{aligned}
& + \text{TWC1}(t) \cdot \text{VWC1} + \text{TWC2}(t) \cdot \text{VWC2} \\
& + \text{THC1}(t) \cdot \text{VHC1} + \text{THC2}(t) \cdot \text{VHC2} + \text{THW1}(t) \cdot \text{VHW1} \\
& + \text{THW2}(t) \cdot \text{VHW2} \left\{ \right. \\
& + \text{S}(\text{ISTEP}) \cdot \frac{\text{VSSALV}}{(1+R)^{\text{ISTEP}+\text{NSS}+\text{NPURCH}}} \\
& + \text{SP}(\text{ISTEP}) \cdot \frac{\text{VSPALV}}{(1+R)^{\text{ISTEP}+\text{NSS}+\text{NPURCH}}} .
\end{aligned}$$

We will note at this juncture that the objective function of the S/PB model is the sum of the costs of the three periods, although, as we will see in Chapter III, the model provides the user the option of applying multipliers to wartime costs. In particular, these multipliers may equal zero, allowing one to include only peacetime costs in the objective function.

E. ADDITIONAL CONSTRAINTS

Although the equations described above are sufficient to specify the S/PB model, certain constraints have been added to allow the user increased flexibility when experimenting with the model. These additional constraints fall into three general classes. The first class imposes upper bounds on certain activities. The second class limits the strategies available to the model with which to acquire and dispose of resources. The final class comprises budget constraints.

1. Upper Bounds

The upper bounds are imposed on the activities relating to the in-theater stockpile, in particular on the variables EPREP, SP(t), $t = 1, \dots, \text{ISTEP}$, and PIPE(t), $t = 1, \dots, \text{ISTEP}$. These constraints take the forms:

$$(77) \quad \text{EPREP} \leq \text{UBPREP}$$

$$(79) \quad \text{SP}(t) \leq \text{UBSP}(t) \quad t = 1, \dots, \text{ISTEP}$$

$$(80) \quad \text{PIPE}(t) \leq \text{UBPIPE}(t) \quad t = 1, \dots, \text{ISTEP} - 1$$

where

UBPREP = the maximum amount of ammunition that can be prepositioned into the in-theater stockpile

UBSP(t) = the maximum amount of ammunition that can be held in the in-theater stockpile during time step t

UBPIPE(t) = the maximum amount of ammunition that can be transferred from the domestic to the in-theater stockpile beginning at time step t.

The parameters are input by the user and might represent limits on in-theater storage capability or limits of the ability of airlift and/or sealift to transport ammunition.

2. Strategic Constraints

The strategic constraints are characterized by the user's ability to include or delete them from the model at will. Therefore, these constraints only appear if the user so desires.

The first such constraint is actually a set of three inequalities specifying the minimum levels of production and of the stockpiles that must be maintained during the final time step of the Mobilization/War period. Such constraints might be useful as a proxy for a protracted war that extended beyond the explicitly modelled period. These equations take the form:

$$(81) \quad S(ISTEP) \geq ENDS$$

$$(82) \quad SP(ISTEP) \geq ENDSP$$

$$(83) \quad \frac{W1(ISTEP)}{KW1} + \frac{W2(ISTEP)}{KW2} + \frac{H1(ISTEP)}{KH1} + \frac{H2(ISTEP)}{KH2} \geq ENDPRD$$

where

ENDS = the amount of ammunition that must be held in the domestic stockpile during the final time step

ENDSP = the amount of ammunition that must be held in the in-theater stockpile during the final time step

ENDPRD = the level of ammunition production to be achieved during the final time step. Note that production from capital transferring from warm to hot states is not included in this constraint.

In order to examine "rules of thumb" wherein the proper stockpile/production base mix is given by a simple ratio, the user may invoke constraint (84)

$$(84) \quad EC1 + EC2 + EW1 + EW2 = ES \cdot \text{RATIO}$$

where

RATIO = the user-specified ratio of total capital to total stockpile to be achieved by the end of the Build-up period.

A final set of constraints allows the user to restrict the families of purchase patterns, particularly those of warm capital, during the Build-up period. These are as follows:.

$$(85) \quad IBW1 + IBW2 = 0$$

$$(86) \quad BW1 + BW2 = 0$$

$$(87) \quad SLPPC1 - SLPNC1 = SLOPC1$$

$$(88) \quad SLPPC2 - SLPNC2 = SLOPC2$$

$$(89) \quad SLPPW1 - SLPNW1 = SLOPW1$$

$$(90) \quad SLPPW2 - SLPNW2 = SLOPW2$$

where

SLOPC1 = the slope desired by the user for the type 1 cold capital purchase pattern

SLOPC2 = the slope desired by the user for the type 2 cold capital purchase pattern

SLOPW1 = the slope desired by the user for the linear component of the type 1 warm capital purchase pattern.

SLOPW2 = the slope desired by the user for the linear component of the type 2 warm capital purchase pattern.

Equations(87) through (90) must be invoked as a group. One should also note that the nonnegativity of the variables requires that if constraint (85) is invoked, both IBW1 and IBW2 must necessarily be zero. The same logic applies to constraint (86).

3. Budget Constraints

The budget constraints impose limits on the undiscounted costs that are incurred by the acquisition of capital and the production of ammunition. Costs associated with other activities are not included. Single constraints apply to the Build-up and Steady-state periods while each time step of the Mobilization/War period has its associated budget constraints.

a. Build-Up Period

By removing the discounting factors from those costs of the Build-up period that pertain to capital acquisition and ammunition production, we obtain the budget constraint for this period.

$$\begin{aligned}
 (91) \quad & BC1 \cdot (VPC1 \cdot NPUCH) + BC2 \cdot (VPC2 \cdot NPUCH) \\
 & + [SLPPC1 - SLPNC1] \cdot \left(VPC1 \sum_{i=1}^{NPUCH} (i-1) \right) \\
 & + [SLPPC2 - SLPNC2] \cdot \left(VPC2 \sum_{i=1}^{NPUCH} (i-1) \right) \\
 & + IBW1 \cdot \left(VPC1 + \frac{VPW1}{KW1} \cdot \sum_{i=1}^{NPUCH} (1-DW1)^{i-1} \right) \\
 & + IBW2 \cdot \left(VPC2 + \frac{VPW2}{KW2} \cdot \sum_{i=1}^{NPUCH} (1-DW2)^{i-1} \right) \\
 & + BW1 \cdot \left(VPC1 \cdot NPUCH + \frac{VPW1}{KW1} \cdot \sum_{i=1}^{NPUCH} \sum_{j=1}^i (1-DW1)^{j-1} \right) \\
 & + BW2 \cdot \left(VPC2 \cdot NPUCH + \frac{VPW2}{KW2} \cdot \sum_{i=1}^{NPUCH} \sum_{j=1}^i (1-DW2)^{j-1} \right) \\
 & + [SLPPW1 - SLPNW1] \cdot \left(VPC1 \cdot \sum_{i=1}^{NPUCH} (i-1) + \frac{VPW1}{KW1} \cdot \sum_{i=1}^{NPUCH} \sum_{j=1}^{i-1} j (1-DW1)^{i-1-j} \right) \\
 & + [SLPPW2 - SLPNW2] \cdot \left(VPC2 \cdot \sum_{i=1}^{NPUCH} (i-1) + \frac{VPW2}{KW2} \cdot \sum_{i=1}^{NPUCH} \sum_{j=1}^{i-1} j (1-DW2)^{i-1-j} \right) \\
 & \leq BPBUDG
 \end{aligned}$$

where

BPBUDG = the user-supplied limit on the Build-up period capital purchase and ammunition production costs (undiscounted).

b. Steady-State Period

In like manner, we determine the Steady-state period budget constraint to be

$$\begin{aligned}
 (92) \quad & EC1 \cdot (VPC1 \cdot DC1 \cdot NSS) + EC2 \cdot (VPC2 \cdot DC2 \cdot NSS) \\
 & + EW1 \cdot (VPC1 \cdot DW1 \cdot NSS + \frac{VPW1}{KW1} \cdot NSS) \\
 & + EW2 \cdot (VPC2 \cdot DW2 \cdot NSS + \frac{VPW2}{KW2} \cdot NSS) \\
 & \leq EBUDG
 \end{aligned}$$

where

EBUDG = the user-supplied limit on the Steady-state period capital purchase and ammunition production costs (undiscounted).

c. Mobilization/War Period

For each time step t of the Mobilization/War period, there is a budget constraint of the following form:

$$\begin{aligned}
 (93) \quad & PC1(t) \cdot VPC1 + PC2(t) \cdot VPC2 \\
 & + W1(t) \cdot \frac{VPW1}{KW1} + W2(t) \cdot \frac{VPW2}{KW2} \\
 & + H1(t) \cdot \frac{VPH1}{KW1} + H2(t) \cdot \frac{VPH2}{KW2} \\
 & + \frac{VPW1}{KW1} \cdot \sum_{\substack{t-LWH1 < s \leq t \\ s \geq 1}} TWH1(s) + \frac{VPW2}{KW2} \cdot \sum_{\substack{t-LWH2 < s \leq t \\ s \geq 1}} TWH2(s) \\
 & \leq BUDG(t)
 \end{aligned}$$

where

BUDG(t) = the user-supplied limit on the undiscounted costs of capital purchase and ammunition production applying to time step t.

F. MODEL SUMMARY

For completeness, we restate in this section the variables, the objective function, and constraints of the S/PB model. Although, as before, we use numbers in bent brackets ($\langle \cdot \rangle$) to represent constraints and expressions, the reader may, if he so chooses, substitute the terms so represented by the numbers and write down the model explicitly. We adopt this approach to save space.

The constraints are given in the order in which they have been programmed into the computer implementation of this model. This order is arbitrary. Recall that ISTEP is the number of time steps in the Mobilization/War period.

Variables

The variables of the S/PB model are:

BC1	SLPPW1
BC2	SLPNW1
SLPPC1	SLPPW2
SLPNC1	SLPNW2
SLPPC2	EC1
SLPNC2	EC2
IBW1	EW1
IBW2	EW2
BW1	ES
BW2	EPREP

(continued on next page)

C1(t)	t = 1, ..., ISTEP
C2(t)	t = 1, ..., ISTEP
W1(t)	t = 1, ..., ISTEP
W2(t)	t = 1, ..., ISTEP
H1(t)	t = 1, ..., ISTEP
H2(t)	t = 1, ..., ISTEP
S(t)	t = 1, ..., ISTEP
SP(t)	t = 1, ..., ISTEP
TCW1(t)	t = 1, ..., ISTEP - 1
TCW2(t)	t = 1, ..., ISTEP - 1
TCH1(t)	t = 1, ..., ISTEP - 1
TCH2(t)	t = 1, ..., ISTEP - 1
TWH1(t)	t = 1, ..., ISTEP - 1
TWH2(t)	t = 1, ..., ISTEP - 1
TWC1(t)	t = 1, ..., ISTEP - 1
TWC2(t)	t = 1, ..., ISTEP - 1
THC1(t)	t = 1, ..., ISTEP - 1
THC2(t)	t = 1, ..., ISTEP - 1
THW1(t)	t = 1, ..., ISTEP - 1
THW2(t)	t = 1, ..., ISTEP - 1
PIPE(t)	t = 1, ..., ISTEP - 1

Objective Function

(94) Minimize
 (over all variables)

$$\begin{aligned}
 & \{BC1 \cdot \langle 23 \rangle + BC2 \cdot \langle 24 \rangle + (SLPPC1-SLPNC1) \cdot \langle 27 \rangle \\
 & + (SLPPC2-SLPNC2) \cdot \langle 28 \rangle + IBW1 \cdot \langle 34 \rangle + IBW2 \cdot \langle 35 \rangle \\
 & + BW1 \cdot \langle 41 \rangle + BW2 \cdot \langle 42 \rangle + (SLPPW1-SLPNW1) \cdot \langle 48 \rangle \\
 & + (SLPPW2-SLPNW2) \cdot \langle 49 \rangle + EC1 \cdot \langle 62 \rangle + EC2 \cdot \langle 63 \rangle \\
 & + EW1 \cdot \langle 67 \rangle + EW2 \cdot \langle 68 \rangle + ES \cdot \langle 69 \rangle + EPREP \cdot \langle 70 \rangle + \langle 77 \rangle\}
 \end{aligned}$$

subject to:

Warm Capital Acquisition

(95) <52>

(96) <53>

Capital Conservation from Build-up through Steady-state

(97) <56>

(98) <57>

Ammunition Acquisition

(99) <50>

Satisfaction of Build-up Period Demand

(100) <19>

(101) <20>

Prepositioning Limitation

(102) <58>

Prepositioning Upper Bound

(103) <78>

Mobilization/War Cold Stocks

(104) <71> (ISTEP equations)

(105) <72> (ISTEP equations)

Mobilization/War Warm Stocks

(106) <73> (ISTEP equations)

(107) <74> (ISTEP equations)

Mobilization/War Hot Stocks

(108) <75> (ISTEP equations)

(109) <76> (ISTEP equations)

Mobilization/War Domestic Stockpile

(110) <77> (ISTEP equations)

Mobilization/War In-Theater Stockpile

(111) <78> (ISTEP equations)

Foreign Stockpile Upper Bounds

(112) <79> (ISTEP inequalities)

Pipeline Upper Bounds

(113) <80> (ISTEP-1 inequalities)

Mobilization/War Budget Constraints

(114) <89> (ISTEP inequalities)

Build-up Budget Constraint

(115) <87>

Steady-State Budget Constraint

(116) <88>

Nonnegative Purchase Requirements

(117) <15>

(118) <16>

(119) <17>

(120) <18>

Final Value Constraints (optional)

- (121) <81>
- (122) <82>
- (123) <83>

Purchase Pattern Slope Constraints (optional)

- (124) <87>
- (125) <88>
- (126) <89>
- (127) <90>

Capital-to-Stockpile Ratio Constraint

- (128) <84>

Satisfaction of Steady-State Demands

- (129) <51>

No Level Warm Capital Buy Constraint (optional)

- (130) <86>

No Initial Warm Capital Buy Constraint (optional)

- (131) <85>

In addition to these constraints, we require that all variables be nonnegative.

III. IMPLEMENTATION AND USER'S GUIDE

The S/PB model, as formulated in the preceding chapter, presents a linear programming problem to which the well-known techniques of linear programming can be applied to obtain a set of variable values minimizing the objective function. We solve this linear programming problem using the linear programming subroutines of a code that solves, by branch-and-bound, separable piecewise-linear programming problems. This program, named MOGG, is documented in Reference [1]. There are two reasons for adopting this approach:

1. It is a simple matter to employ MOGG as a linear programming routine.
2. Minor modifications allow one to replace some linear terms with piecewise-linear functions of the variables, thereby enabling one to investigate certain nonlinear formulations of the model. This is a possible future effort.

The model has been implemented by reprogramming the initial section of MOGG in such a way as to replace MOGG's input code with code that constructs MOGG input from S/PB input.

We will not discuss programming considerations in detail here; however, it may be useful to the user of the model to know that the linear programming tableau is filled by columns. First is a section of columns corresponding to artificial variables followed by columns corresponding to model variables in the following order:

<u>Column number(s)</u> <u>(after artificial variable(s))</u>		<u>Variable(s)</u>
1		BC1
2		BC2
3		BW1
4		BW2
5		SLPPC1
6		SLPNC1
7		SLPPC2
8		SLPNC2
9		SLPPW1
10		SLPNW1
11		SLPPW2
12		SLPNW2
13		EC1
14		EC2
15		EW1
16		EW2
17		ES
18		EPREP
19	to 18 + ISTEP	C1(t) (t=1,...,ISTEP)
19 + ISTEP	to 18 + 2ISTEP	C2(t) (t=1,...,ISTEP)
19 + 2ISTEP	to 18 + 3ISTEP	W1(t) (t=1,...,ISTEP)
19 + 3ISTEP	to 18 + 4ISTEP	W2(t) (t=1,...,ISTEP)
19 + 4ISTEP	to 18 + 5ISTEP	H1(t) (t=1,...,ISTEP)
19 + 5ISTEP	to 18 + 6ISTEP	H2(t) (t=1,...,ISTEP)
19 + 6ISTEP	to 18 + 7ISTEP	PC1(t) (t=1,...,ISTEP)
19 + 7ISTEP	to 18 + 8ISTEP	PC2(t) (t=1,...,ISTEP)
19 + 8ISTEP	to 18 + 9ISTEP	S(t) (t=1,...,ISTEP)
19 + 9ISTEP	to 18 + 10ISTEP	SP(t) (t=1,...,ISTEP)
19 + 10ISTEP	to 17 + 11ISTEP	PIPE(t) (t=1,...,ISTEP-1)
18 + 11ISTEP	to 16 + 12ISTEP	TCW1(t) (t=1,...,ISTEP-1)
17 + 12ISTEP	to 15 + 13ISTEP	TCW2(t) (t=1,...,ISTEP-1)

<u>Column number(s)</u> <u>(after artificial variable(s))</u>	<u>Variable(s)</u>
16 + 13ISTEP to 14 + 14ISTEP	TCH1(t) (t=1,...,ISTEP-1)
15 + 14ISTEP to 13 + 15ISTEP	TCH2(t) (t=1,...,ISTEP-1)
14 + 15ISTEP to 12 + 16ISTEP	TWH1(t) (t=1,...,ISTEP-1)
13 + 16ISTEP to 11 + 17ISTEP	TWH2(t) (t=1,...,ISTEP-1)
12 + 17ISTEP to 10 + 18ISTEP	TWC1(t) (t=1,...,ISTEP-1)
11 + 18ISTEP to 9 + 19ISTEP	TWC2(t) (t=1,...,ISTEP-1)
10 + 19ISTEP to 8 + 20ISTEP	THC1(t) (t=1,...,ISTEP-1)
9 + 20ISTEP to 7 + 21ISTEP	THC2(t) (t=1,...,ISTEP-1)
8 + 21ISTEP to 6 + 22ISTEP	THW1(t) (t=1,...,ISTEP-1)
7 + 22ISTEP to 5 + 23ISTEP	THW2(t) (t=1,...,ISTEP-1)
6 + 23ISTEP	IBW1
7 + 23ISTEP	IBW2

A. USING THE MODEL

The first card of the input deck is a title card. Any fifty character title is acceptable. Following the title card are the inputs required to run the S/PB model, which are listed below in the order in which they are read. After each bullet (•) is a list of parameter values that must appear on the card or cards as well as the applicable FORTRAN format statement. Only those parameters that are not defined in Chapter II are defined here.

- IXPRIIN, K1, K2, K3, K4, K5, KC1, KC2, KC3, KC4
FORMAT (10I5)

IXPRIIN = K1 = K2 = K3 = K4 = K5 = 0

The first six entries are MOGG options, which are explained in Reference [1]. Except for debugging purposes, they should all be set to zero. The next four entries are the means with which the user imposes the optional constants.

$$KC1 = \begin{cases} 1 & \text{if the user wishes to include the final value} \\ & \text{constraints (equations (121)-(123))} \\ 0 & \text{otherwise.} \end{cases}$$

$$KC2 = \begin{cases} 1 & \text{if the user wishes to include the purchase pattern} \\ & \text{shape constraints (Equations (124)-(127)).} \\ 0 & \text{otherwise.} \end{cases}$$

$$KC3 = \begin{cases} 1 & \text{if the user wishes to include the capital to} \\ & \text{stockpile ratio constraint (Equation (128)).} \\ 0 & \text{otherwise.} \end{cases}$$

$$KC4 = \begin{cases} 2 & \text{if the user wishes to include the no-level-warm-} \\ & \text{capital purchase constraint (Equation (130)).} \\ 1 & \text{if the user wishes to include the no-initial-warm-} \\ & \text{capital purchase constraint (Equation (131)).} \\ 0 & \text{otherwise.} \end{cases}$$

- NLAG, NPURCH, NSS, ISTEP
FORMAT (4I5)

NPURCH may assume any positive integer value. NSS and NLAG may be any nonnegative integer value. ISTEP is limited to integer values between 1 and 36 (because of core storage limitations).

- VC1, VC2, VW1, VW2, VPW1, VPW2, VH1, VH2
FORMAT (8F10.4)
- VPH1, VPH2, VPC1, VPC2, VCW1, VCW2, VCH1, VCH2
FORMAT (8F10.4)
- VWH1, VWH2, VWC1, VWC2, VHC1, VHC2, VHW1, VHW2
FORMAT (8F10.4)
- VPIPE, VS, VSSALV, VSP, VSPALV, VPREP, R
FORMAT (7F10.4)
- MA, MB, AMULT, BMULT
FORMAT (2I5, 2F10.3).

These last four entries are included to offer the user the opportunity to investigate the effect of weighting certain costs of the Mobilization/War period. For instance, one might wish to determine the optimal stockpile/production base mix where wartime costs are excluded from the objective function.

Let $t = 1, \dots, \text{ISTEP}$ denote the time steps of the Mobilization/War period. The unit costs corresponding to time steps t such that $\text{MA} \leq t < \text{MB}$ are multiplied by AMULT . Those costs corresponding to time steps t for which $\text{MB} \leq t \leq \text{ISTEP}$ are multiplied by BMULT .

- KW1, KW2, KH1, KH2
FORMAT (4F10.4)
- DC1, DC2, DW1, DW2, DH1, DH2, DS, DSP
FORMAT (15I5)
- LP1, LP2, LCW1, LCW2, LCH1, LCH2, LWH1, LWH2, LHC1, LHC2, LHW1, LHW2, LWC1, LWC2, LPIPE
FORMAT (16I5)

In order to prevent a resource from appearing in two places during any one time step, all these time lags should be at least 1.

- OMUN, OCOLD1, OCOLD2, OWARM1, OWARM2
FORMAT (5F10.4)
- BPBUG, EBUDG
- BUDG(1), ..., BUDG(ISTEP)
FORMAT (8F10.4)

More than two cards will be necessary if ISTEP is greater than 8.

- BPDEM, SSDEM
- DD(1), ..., DD(ISTEP)
- FD(1), ..., FD(ISTEP)
FORMAT (8F10.4)

More than three cards will be necessary if ISTEP is greater than 8.

- UBPREP
- UBSP(1),...,UBSP(ISTEP)
- UBPIPE(1),...,UBPIPE(ISTEP-1)

More than three cards will be necessary if ISTEP is greater than 8.

Optional Cards

If KC1 = 1, include

- ENDS, ENDSP, ENDP
FORMAT (3F10.4)

If KC2 = 1, include

- SLOPC1, SLOPC2, SLOPW1, SLOPW2
FORMAT (4F10.4)

If KC3 = 1, include

- RATIO
FORMAT (1F10.4)

Run times of the model on the CDC 6400 computer are on the order of 100 CPU seconds.

Output consists of three sections. The first restates the inputs and also contains a statement of production costs attributable to original warm capital stocks. The second section is MOGG output and, for those unfamiliar with Reference [1], may be ignored. The final section gives the value of the objective function at optimum and the optimal variable values.

B. SAMPLE RUN

Figure 5 shows a sample input deck. Note that, for this run, the Build-up period lasts a total of 60 time steps, with 30 of those required before new capital can produce. The Steady-state period is 180 time steps and the Mobilization/War period is 24. Also, the user has set the final value constraints such that the domestic stockpile must have in it at least 277.31302 units in the final time period. Notice also the negative entries for VSSALV and VSPALV, indicating that at the end of the Mobilization/War period, the salvage value of ammunition remaining in the stockpile is subtracted from the total costs.

The output of the S/PB model for this sample run is displayed in Figure 6. The output has been annotated to highlight certain features.

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Figure 5. SAMPLE INPUT DECK

IDA STOCKPILE/PRODUCTION BASE MODEL -- ILLIE
SAMPLE PROBLEM

FINAL PERIOD STOCKPILES AND PRODUCTION HAVE BEEN SET -- Listing of optional constraints that have been requested

NLAGE= 30 ADUPCUM= 30 NSS= 180 TSTEP= 24

CONSTs *****

VC1	.0000	VC2	.0000	VW1	0.0000	VW2	0.0000	VPW1	1.1190	VPW2	1000.0000	VM1	0.0000	VM2	0.0000
VPH1	1.1190	VPL2	1000.0000	VPC1	1.0000	VPC2	1000.0000	VCW1	0.0000	VCW2	0.0000	VCH1	0.0000	VCH2	0.0000
VWH1	0.0000	VWL2	0.0000	VWC1	0.0000	VWC2	0.0000	VHC1	0.0000	VHC2	0.0000	VHW1	0.0000	VHW2	0.0000
VPIPF	0.0000	VS	.0002	VSP	.0002	VSSA1 V	-.5000	VSPA1 V	0.0000	VBSALV	-.5000	VPREP	0.0000	R	.0083
MA	1	MR	1	AMULT	.0001	BMULT	.0001								

CAPITAL/EQUIPMENT RATIOS *****

KW1	2.893	KW2	2.893	KH1	1.223	KH2	1.223
-----	-------	-----	-------	-----	-------	-----	-------

DETERIORATION RATES *****

DC1	0.000	DC2	0.000	DW1	.004	DW2	.004	DH1	.004	DH2	.004	DS	.002	DSP	.002
-----	-------	-----	-------	-----	------	-----	------	-----	------	-----	------	----	------	-----	------

TIME LAGS *****

LP1	24	LP2	24	LC1	6	LC2	9	LCW1	3	LCH1	1	LWC1	1	LHW1	1	LHC1	1	LW2	1	LH2	1	LPC1	1	LPC2	2
-----	----	-----	----	-----	---	-----	---	------	---	------	---	------	---	------	---	------	---	-----	---	-----	---	------	---	------	---

ORIGINALS *****

OMUN	451.7452	OCALD1	0.0000	OCALD2	0.0000	OWAPM1	43.2601	OWAPM2	0.0000
------	----------	--------	--------	--------	--------	--------	---------	--------	--------

PRODUCTION LIFING NLAGE = 448.4151

INVENTORY AFTER NLAGE = 900.3403

BUDGETS *****

BPRUNG= 0000000.000

ERUDG= 100000.000

RIUG=	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000
-------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------

RIUG=	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000	100000.000
-------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------	------------

Figure 6. SAMPLE PROBLEM OUTPUT

```

BUDG= 100000.000 100000.000 100000.000 100000.000 100000.000 100000.000
DEMANDS *****
RPDEM= 0.0000
SSDEM= 0.0000
DD= 0.000 0.000 0.000 0.000 0.000 0.000
DD= 0.000 0.000 0.000 0.000 0.000 0.000
DD= 0.000 0.000 0.000 0.000 0.000 0.000
FD= 900.000 800.000 700.000 600.000 500.000 400.000
FD= 281.000 313.000 344.000 375.000 406.000 438.000
FD= 541.000 563.000 594.000 625.000 656.000 688.000
Upper Bounds *****
UAPRFP= 100000.0000
URSP= 100000.000 100000.000 100000.000 100000.000 100000.000 100000.000
URSP= 100000.000 100000.000 100000.000 100000.000 100000.000 100000.000
URSP= 100000.000 100000.000 100000.000 100000.000 100000.000 100000.000
URPIPF= 100000.000 100000.000 100000.000 100000.000 100000.000 100000.000
URPIPE= 100000.000 100000.000 100000.000 100000.000 100000.000 100000.000
URPIPE= 100000.000 100000.000 100000.000 100000.000 100000.000 100000.000
OPTIONAL INFORMATION *****
ENDS= 277.3130 ENDSP= 0.0000 ENDPMU= 0.0000
PRODUCTION COSTS FROM ORIGINAL WARM1= 708.344 PRODUCTION COSTS FROM ORIGINAL WARM2= 0.000 --Fixed costs independent
of variable values

```

REITERATION OF INPUT

Figure 6. (contd)

283ROWS
559VARIABLES
5 LP PROBLEMS WILL BE SOLVED

CONFIDENTIAL FLAG--

[illegible]

VARIABLE CARDS REPRODUCED--

RHS CARD(S) REPRODUCED--

[illegible]

Figure 6. (contd)

[illegible]

Figure 6. (contd)

STARTING TO ITERATE

STAGE PROBLEM LOWER BOUND UPPER BOUND BRANCHING VARIABLE

STABILITY COUNT = 0

0

OBJECTIVE FUNCTION AT OPTIMUM 4697

TOTAL DISCOUNTED COSTS= 5425.017 -- Cost at optimal variable values

VARIABLE VALUES AT OPTIMUM--

BUILD-UP PERIOD *****

LR1= 0.000 LR2= 0.000

RC1= 0.000 RC2= 0.000 RW1= 3.212 RW2= 0.000

SLOPEC1= 0.000 SLOPEC2= 0.000 SLOPEW1= 1.766 SLOPEW2= 0.000

Build-up period variable values

STEADY-STATE PERIOD *****

EC1= 841.511 EC2= 0.000 TW1= 24.542 EW2= 0.000 TOTAL CAPITAL= 868.053

Steady-state period variable values

ES= 4364.036 FPHFP= 1721.684

BACK/STOCKPILE RATIO= .100

WARTIME PERIOD *****

C1(1)= 0.000 C2(1)= 0.000 W1(1)= 0.000 W2(1)= 0.000 H1(1)= 0.000
C1(2)= 0.000 C2(2)= 0.000 W1(2)= 0.000 W2(2)= 0.000 H1(2)= 0.000
C1(3)= 0.000 C2(3)= 0.000 W1(3)= 0.000 W2(3)= 0.000 H1(3)= 0.000
C1(4)= 0.000 C2(4)= 0.000 W1(4)= 0.000 W2(4)= 0.000 H1(4)= 24.542
C1(5)= 0.000 C2(5)= 0.000 W1(5)= 0.000 W2(5)= 0.000 H1(5)= 24.542
C1(6)= 0.000 C2(6)= -0.000 W1(6)= 0.000 W2(6)= 0.000 H1(6)= 24.542
C1(7)= 0.000 C2(7)= 0.000 W1(7)= 0.000 W2(7)= 0.000 H1(7)= 24.542
C1(8)= 0.000 C2(8)= 0.000 W1(8)= 0.000 W2(8)= 0.000 H1(8)= 24.542
C1(9)= 0.000 C2(9)= 0.000 W1(9)= 0.000 W2(9)= 0.000 H1(9)= 24.542
C1(10)= 0.000 C2(10)= 0.000 W1(10)= 0.000 W2(10)= 0.000 H1(10)= 611.752
C1(11)= 0.000 C2(11)= 0.000 W1(11)= 0.000 W2(11)= 0.000 H1(11)= 609.294
C1(12)= 0.000 C2(12)= 0.000 W1(12)= 0.000 W2(12)= 0.000 H1(12)= 604.735
C1(13)= 0.000 C2(13)= 0.000 W1(13)= 0.000 W2(13)= 0.000 H1(13)= 604.298
C1(14)= 0.000 C2(14)= 0.000 W1(14)= 0.000 W2(14)= 0.000 H1(14)= 719.791
C1(15)= 0.000 C2(15)= 0.000 W1(15)= 0.000 W2(15)= 0.000 H1(15)= 716.879
C1(16)= 0.000 C2(16)= 0.000 W1(16)= 0.000 W2(16)= 0.000 H1(16)= 717.980
C1(17)= 0.000 C2(17)= 0.000 W1(17)= 0.000 W2(17)= 0.000 H1(17)= 711.093
C1(18)= 0.000 C2(18)= 0.000 W1(18)= 0.000 W2(18)= 0.000 H1(18)= 708.217
C1(19)= 0.000 C2(19)= 0.000 W1(19)= 0.000 W2(19)= 0.000 H1(19)= 705.243
C1(20)= 0.000 C2(20)= 0.000 W1(20)= 0.000 W2(20)= 0.000 H1(20)= 702.281
C1(21)= 0.000 C2(21)= 0.000 W1(21)= 0.000 W2(21)= 0.000 H1(21)= 699.331

MOBILIZATION/WAR PERIOD VARIABLE VALUES

Figure 6. (contd)

C1(22)=	.446	C2(22)=	0.000	W1(22)=	.000	W2(22)=	0.000	H1(22)=	694.394
C1(23)=	.557	C2(23)=	0.000	W1(23)=	.000	W2(23)=	0.000	H1(23)=	0.000
C1(24)=	.649	C2(24)=	0.000	W1(24)=	694.804	W2(24)=	0.000	H1(24)=	139.161
H2(1)=	0.000	PC1(1)=	0.000	PC2(1)=	0.000	S(1)=	1976.527	SP(1)=	801.684
H2(2)=	0.000	PC1(2)=	0.000	PC2(2)=	0.000	S(2)=	1341.590	SP(2)=	0.000
H2(3)=	0.000	PC1(3)=	0.000	PC2(3)=	0.000	S(3)=	487.941	SP(3)=	0.000
H2(4)=	0.000	PC1(4)=	0.000	PC2(4)=	0.000	S(4)=	507.900	SP(4)=	0.000
H2(5)=	0.000	PC1(5)=	0.000	PC2(5)=	0.000	S(5)=	228.657	SP(5)=	0.000
H2(6)=	0.000	PC1(6)=	0.000	PC2(6)=	0.000	S(6)=	0.000	SP(6)=	0.000
H2(7)=	0.000	PC1(7)=	0.000	PC2(7)=	0.000	S(7)=	31.711	SP(7)=	0.000
H2(8)=	0.000	PC1(8)=	0.000	PC2(8)=	0.000	S(8)=	11.355	SP(8)=	0.000
H2(9)=	0.000	PC1(9)=	0.000	PC2(9)=	0.000	S(9)=	0.000	SP(9)=	0.000
H2(10)=	0.000	PC1(10)=	0.000	PC2(10)=	0.000	S(10)=	0.000	SP(10)=	0.000
H2(11)=	0.000	PC1(11)=	0.000	PC2(11)=	0.000	S(11)=	258.222	SP(11)=	0.000
H2(12)=	0.000	PC1(12)=	0.000	PC2(12)=	0.000	S(12)=	326.667	SP(12)=	125.406
H2(13)=	0.000	PC1(13)=	0.000	PC2(13)=	0.000	S(13)=	421.951	SP(13)=	0.000
H2(14)=	0.000	PC1(14)=	0.000	PC2(14)=	0.000	S(14)=	509.832	SP(14)=	0.000
H2(15)=	0.000	PC1(15)=	0.000	PC2(15)=	0.000	S(15)=	0.000	SP(15)=	0.000
H2(16)=	0.000	PC1(16)=	0.000	PC2(16)=	0.000	S(16)=	544.014	SP(16)=	0.000
H2(17)=	0.000	PC1(17)=	0.000	PC2(17)=	0.000	S(17)=	570.402	SP(17)=	564.185
H2(18)=	0.000	PC1(18)=	0.000	PC2(18)=	0.000	S(18)=	523.428	SP(18)=	0.000
H2(19)=	0.000	PC1(19)=	0.000	PC2(19)=	0.000	S(19)=	443.120	SP(19)=	0.000
H2(20)=	0.000	PC1(20)=	0.000	PC2(20)=	0.000	S(20)=	328.559	SP(20)=	0.000
H2(21)=	0.000	PC1(21)=	0.000	PC2(21)=	0.000	S(21)=	140.825	SP(21)=	0.000
H2(22)=	0.000	PC1(22)=	0.000	PC2(22)=	0.000	S(22)=	0.000	SP(22)=	0.000
H2(23)=	0.000	PC1(23)=	0.000	PC2(23)=	0.000	S(23)=	0.000	SP(23)=	0.000
H2(24)=	0.000	PC1(24)=	0.000	PC2(24)=	0.000	S(24)=	353.644	SP(24)=	0.000
PIPE(1)=	700.000	TC1(1)=	841.622	TC2(1)=	0.000	TC1(1)=	0.000	TC2(1)=	0.000
PIPE(2)=	600.000	TC1(2)=	.111	TC2(2)=	0.000	TC1(2)=	0.000	TC2(2)=	0.000
PIPE(3)=	500.000	TC1(3)=	.111	TC2(3)=	0.000	TC1(3)=	0.000	TC2(3)=	0.000
PIPE(4)=	400.000	TC1(4)=	0.000	TC2(4)=	0.000	TC1(4)=	.111	TC2(4)=	0.000
PIPE(5)=	300.000	TC1(5)=	0.000	TC2(5)=	0.000	TC1(5)=	.111	TC2(5)=	0.000
PIPE(6)=	250.000	TC1(6)=	0.000	TC2(6)=	0.000	TC1(6)=	.111	TC2(6)=	0.000
PIPE(7)=	200.000	TC1(7)=	.111	TC2(7)=	0.000	TC1(7)=	0.000	TC2(7)=	0.000
PIPE(8)=	313.000	TC1(8)=	.111	TC2(8)=	0.000	TC1(8)=	0.000	TC2(8)=	0.000
PIPE(9)=	344.000	TC1(9)=	.111	TC2(9)=	0.000	TC1(9)=	0.000	TC2(9)=	0.000
PIPE(10)=	500.400	TC1(10)=	0.000	TC2(10)=	0.000	TC1(10)=	0.000	TC2(10)=	0.000
PIPE(11)=	280.854	TC1(11)=	0.000	TC2(11)=	0.000	TC1(11)=	0.000	TC2(11)=	0.000
PIPE(12)=	430.000	TC1(12)=	0.000	TC2(12)=	0.000	TC1(12)=	0.000	TC2(12)=	0.000
PIPE(13)=	460.000	TC1(13)=	0.000	TC2(13)=	0.000	TC1(13)=	0.000	TC2(13)=	0.000
PIPE(14)=	500.000	TC1(14)=	0.000	TC2(14)=	0.000	TC1(14)=	0.000	TC2(14)=	0.000
PIPE(15)=	1095.185	TC1(15)=	0.000	TC2(15)=	0.000	TC1(15)=	139.141	TC2(15)=	0.000
PIPE(16)=	0.000	TC1(16)=	0.000	TC2(16)=	0.000	TC1(16)=	0.000	TC2(16)=	0.000
PIPE(17)=	594.000	TC1(17)=	0.000	TC2(17)=	0.000	TC1(17)=	0.000	TC2(17)=	0.000
PIPE(18)=	625.000	TC1(18)=	.334	TC2(18)=	0.000	TC1(18)=	0.000	TC2(18)=	0.000
PIPE(19)=	656.000	TC1(19)=	0.000	TC2(19)=	0.000	TC1(19)=	0.000	TC2(19)=	0.000
PIPE(20)=	688.000	TC1(20)=	0.000	TC2(20)=	0.000	TC1(20)=	0.000	TC2(20)=	0.000
PIPE(21)=	710.000	TC1(21)=	0.000	TC2(21)=	0.000	TC1(21)=	0.000	TC2(21)=	0.000
PIPE(22)=	750.000	TC1(22)=	0.000	TC2(22)=	0.000	TC1(22)=	0.000	TC2(22)=	0.000
PIPE(23)=	0.000	TC1(23)=	0.000	TC2(23)=	0.000	TC1(23)=	0.000	TC2(23)=	0.000
TH1(1)=	26.542	TH1(1)=	0.000	TH2(1)=	0.000	TH2(1)=	0.000	TH1(1)=	0.000
TH1(2)=	.111	TH1(2)=	0.000	TH2(2)=	0.000	TH2(2)=	0.000	TH1(2)=	0.000
TH1(3)=	.111	TH1(3)=	0.000	TH2(3)=	0.000	TH2(3)=	0.000	TH1(3)=	0.000
TH1(4)=	.111	TH1(4)=	0.000	TH2(4)=	0.000	TH2(4)=	0.000	TH1(4)=	0.000
TH1(5)=	.111	TH1(5)=	0.000	TH2(5)=	0.000	TH2(5)=	0.000	TH1(5)=	0.000
TH1(6)=	.111	TH1(6)=	0.000	TH2(6)=	0.000	TH2(6)=	0.000	TH1(6)=	0.000
TH1(7)=	841.622	TH1(7)=	0.000	TH2(7)=	0.000	TH2(7)=	0.000	TH1(7)=	0.000
TH1(8)=	.111	TH1(8)=	0.000	TH2(8)=	0.000	TH2(8)=	0.000	TH1(8)=	0.000
TH1(9)=	.111	TH1(9)=	0.000	TH2(9)=	0.000	TH2(9)=	0.000	TH1(9)=	0.000
TH1(10)=	0.000	TH1(10)=	0.000	TH2(10)=	0.000	TH2(10)=	0.000	TH1(10)=	0.000
TH1(11)=	117.919	TH1(11)=	0.000	TH2(11)=	0.000	TH2(11)=	0.000	TH1(11)=	138.492
									0.000

Figure 6. (contd)

THW1(12)=	0.000	THW2(12)=	0.000	THW1(12)=	0.000	THW2(12)=	0.000
THW1(13)=	0.111	THW2(13)=	0.000	THW1(13)=	0.000	THW2(13)=	0.000
THW1(14)=	0.111	THW2(14)=	0.000	THW1(14)=	0.000	THW2(14)=	0.000
THW1(15)=	0.111	THW2(15)=	0.000	THW1(15)=	0.000	THW2(15)=	0.000
THW1(16)=	0.000	THW2(16)=	0.000	THW1(16)=	0.000	THW2(16)=	0.000
THW1(17)=	0.000	THW2(17)=	0.000	THW1(17)=	0.000	THW2(17)=	0.000
THW1(18)=	0.000	THW2(18)=	0.000	THW1(18)=	0.000	THW2(18)=	0.000
THW1(19)=	0.000	THW2(19)=	0.000	THW1(19)=	0.000	THW2(19)=	0.000
THW1(20)=	0.000	THW2(20)=	0.000	THW1(20)=	0.000	THW2(20)=	0.000
THW1(21)=	0.000	THW2(21)=	0.000	THW1(21)=	0.000	THW2(21)=	0.000
THW1(22)=	0.000	THW2(22)=	0.000	THW1(22)=	0.000	THW2(22)=	0.000
THW1(23)=	0.000	THW2(23)=	0.000	THW1(23)=	0.000	THW2(23)=	0.000
THW2(1)=	0.000	THW2(1)=	0.000	THW2(1)=	0.000	THW2(1)=	0.000
THW2(2)=	0.000	THW2(2)=	0.000	THW2(2)=	0.000	THW2(2)=	0.000
THW2(3)=	0.000	THW2(3)=	0.000	THW2(3)=	0.000	THW2(3)=	0.000
THW2(4)=	0.000	THW2(4)=	0.000	THW2(4)=	0.000	THW2(4)=	0.000
THW2(5)=	0.000	THW2(5)=	0.000	THW2(5)=	0.000	THW2(5)=	0.000
THW2(6)=	0.000	THW2(6)=	0.000	THW2(6)=	0.000	THW2(6)=	0.000
THW2(7)=	0.000	THW2(7)=	0.000	THW2(7)=	0.000	THW2(7)=	0.000
THW2(8)=	0.000	THW2(8)=	0.000	THW2(8)=	0.000	THW2(8)=	0.000
THW2(9)=	0.000	THW2(9)=	0.000	THW2(9)=	0.000	THW2(9)=	0.000
THW2(10)=	0.000	THW2(10)=	0.000	THW2(10)=	0.000	THW2(10)=	0.000
THW2(11)=	0.000	THW2(11)=	0.000	THW2(11)=	0.000	THW2(11)=	0.000
THW2(12)=	0.000	THW2(12)=	0.000	THW2(12)=	0.000	THW2(12)=	0.000
THW2(13)=	0.000	THW2(13)=	0.000	THW2(13)=	0.000	THW2(13)=	0.000
THW2(14)=	0.000	THW2(14)=	0.000	THW2(14)=	0.000	THW2(14)=	0.000
THW2(15)=	0.000	THW2(15)=	0.000	THW2(15)=	0.000	THW2(15)=	0.000
THW2(16)=	0.000	THW2(16)=	0.000	THW2(16)=	0.000	THW2(16)=	0.000
THW2(17)=	0.000	THW2(17)=	0.000	THW2(17)=	0.000	THW2(17)=	0.000
THW2(18)=	0.000	THW2(18)=	0.000	THW2(18)=	0.000	THW2(18)=	0.000
THW2(19)=	0.000	THW2(19)=	0.000	THW2(19)=	0.000	THW2(19)=	0.000
THW2(20)=	0.000	THW2(20)=	0.000	THW2(20)=	0.000	THW2(20)=	0.000
THW2(21)=	0.000	THW2(21)=	0.000	THW2(21)=	0.000	THW2(21)=	0.000
THW2(22)=	0.000	THW2(22)=	0.000	THW2(22)=	0.000	THW2(22)=	0.000
THW2(23)=	0.000	THW2(23)=	0.000	THW2(23)=	0.000	THW2(23)=	0.000

WABTIME PRODUCTION CUEVE

PRODUCTION(1)=	9.175
PRODUCTION(2)=	9.214
PRODUCTION(3)=	9.252
PRODUCTION(4)=	21.824
PRODUCTION(5)=	21.824
PRODUCTION(6)=	21.824
PRODUCTION(7)=	312.711
PRODUCTION(8)=	312.711
PRODUCTION(9)=	312.711
PRODUCTION(10)=	506.406
PRODUCTION(11)=	530.680
PRODUCTION(12)=	574.987
PRODUCTION(13)=	535.033
PRODUCTION(14)=	568.767
PRODUCTION(15)=	564.424
PRODUCTION(16)=	564.014
PRODUCTION(17)=	547.614
PRODUCTION(18)=	578.224
PRODUCTION(19)=	574.791
PRODUCTION(20)=	574.369
PRODUCTION(21)=	571.957
PRODUCTION(22)=	560.554

Figure 6. (contd)

PRODUCTION(21)=	.000
PRODUCTION(24)=	352.644
TOTAL WARTIME PRODUCTION= 8709.187	

Figure 6. (concluded)

REFERENCE

- [1] Grotte, Jeffrey H., *Computer Program for Solving Separable Nonconvex Optimization Problems*, IDA P-1318, Institute for Defense Analyses, Arlington, Virginia, January 1978.

APPENDIX A

GLOSSARY OF INPUT PARAMETERS AND VARIABLES

GLOSSARY OF INPUT PARAMETERS

<u>Name</u>	<u>Definition</u>	<u>Location of First Use</u>
AMULT	The cost multiplier for Mobilization/War time steps in the interval [MA,MB]	71
BMULT	The cost multiplier for Mobilization/War time steps in the interval [MB,ISTEP]	71
BPBUDG	The user-supplied limit on the Build-up period capital purchase and ammunition production costs (undiscounted)	60
BPDEM	The demand for ammunition during each time step of the Build-up period	27
BUDG(t)	The user-supplied limit on the undiscounted costs of capital purchase and ammunition production applying to time step t	61
DC1	The fraction of type 1 cold stocks lost to deterioration during one time step	12
DC2	The fraction of type 2 cold stocks lost to deterioration during one time step	12
DD(t)	The domestic demand for ammunition during time step t	15
DH1	The fraction of type 1 hot stocks lost to deterioration during one time step	14
DH2	The fraction of type 2 hot stocks lost to deterioration during one time step	14
DS	The fraction of the domestic ammunition stockpile lost to deterioration during one time step	14
DSP	The fraction of the in-theater ammunition stockpile lost to deterioration during one time step	15
DW1	The fraction of type 1 warm stocks lost to deterioration during one time step	13
DW2	The fraction of type 2 warm stocks lost to deterioration during one time step	13

GLOSSARY OF INPUT PARAMETERS (contd)

EBUDG	The user-supplied limit on the Steady-state capital purchase and ammunition production costs (undiscounted)	60
ENDPRD	The level of ammunition production to be achieved during the final time step	57
ENDS	The amount of ammunition that must be held in the domestic stockpile during the final time step	57
ENDSP	The amount of ammunition that must be held in the in-theater stockpile during the final time step	57
FD(t)	The in-theater demand for ammunition during time step t	15
ISTEP	The number of time steps in the Mobilization/War period	47
KH1	The capital to output ratio for type 1 hot capital	15
KH2	The capital to output ratio for type 2 hot capital	15
KW1	The capital to output ratio for type 1 warm capital	14
KW2	The capital to output ratio for type 2 warm capital	15
LCH1	The number of time steps required to transfer type 1 capital from cold to hot stocks	14
LCH2	The number of time steps required to transfer type 2 capital from cold to hot stocks	14
LCW1	The number of time steps required to transfer type 1 capital from cold to warm stocks	14
LCW2	The number of time steps required to transfer type 2 capital from cold to warm stocks	14
LHC1	The number of time steps required to transfer type 1 capital from hot to cold stocks	13
LHC2	The number of time steps required to transfer type 2 capital from hot to cold stocks	13

GLOSSARY OF INPUT PARAMETERS (contd)

LHW1	The number of time steps required to transfer type 1 capital from hot to warm stocks	14
LHW2	The number of time steps required to transfer type 2 capital from hot to warm stocks	15
LP1	The number of time steps from the time type 1 capital is purchased until it is delivered to cold stocks	12
LP2	The number of time steps from the time type 2 capital is purchased until it is delivered to cold stocks	12
LPIPE	The number of time steps required to transfer ammunition from the domestic to the in-theater stockpile	15
LWC1	The number of time steps required to transfer type 1 capital from warm to cold stocks	12
LWC2	The number of time steps required to transfer type 2 capital from warm to cold stocks	12
LWH1	The number of time steps required to transfer type 1 capital from warm to hot stocks	14
LWH2	The number of time steps required to transfer type 2 capital from warm to hot stocks	14
MA	The first time step of the Mobilization/War period at which cost multiplier AMULT is applied	71
MB	The first time step of the Mobilization/War period at which cost multiplier BMULT is applied	71
NLAG	The time delay in acquiring capital during the Build-up period	41
NPURCH	The number of time steps in the Build-up period	20
NSS	The number of time steps in the Steady-state period	41
OCOLD1	The amount of original type 1 cold capital	23
OCOLD2	The amount of original type 2 cold capital	23

GLOSSARY OF INPUT PARAMETERS (contd)

OMUN	The amount of original ammunition	27
OWARM1	The amount of original type 1 warm capital	26
OWARM2	The amount of original type 2 warm capital	26
R	The single time step discount factor for costs	18
RATIO	The user-specified ratio of total capital to total stockpile to be achieved during the end of the Build-up period	58
SLOPC1	The slope desired by the user for the type 1 cold capital purchase pattern	58
SLOPC2	The slope desired by the user for the type 2 cold capital purchase pattern	58
SLOPW1	The slope desired by the user for the linear component of the type 1 warm capital purchase pattern	58
SLOPW2	The slope desired by the user for the linear component of the type 2 warm capital purchase pattern	58
SSDEM	The demand for ammunition per time step during the Steady-state period	42
UBPIPE(t)	The maximum amount of ammunition that can be transferred from the domestic to the in-theater stockpile during time step t	57
UBPREP	The maximum amount of ammunition that can be prepositioned into the in-theater stockpile	57
UBSP(t)	The maximum amount of ammunition that can be held in the in-theater stockpile during time step t	57
VC1	The cost of maintaining one unit of type 1 capital in cold stocks for one time step	16
VC2	The cost of maintaining one unit of type 2 capital in cold stocks for one time step	16
VCH1	The cost of transferring one unit of type 1 capital from cold to hot stocks	17
VCH2	The cost of transferring one unit of type 2 capital from cold to hot stocks	17
VCW1	The cost of transferring one unit of type 1 capital from cold to warm stocks	17
VCW2	The cost of transferring one unit of type 2 capital from cold to warm stocks	17

GLOSSARY OF INPUT PARAMETERS (contd)

VH1	The cost of maintaining one unit of type 1 capital in hot stocks for one time step	17
VH2	The cost of maintaining one unit of type 2 capital in hot stocks for one time step	17
VHC1	The cost of transferring one unit of type 1 capital from hot to cold stocks	18
VHC2	The cost of transferring one unit of type 2 capital from hot to cold stocks	18
VHW1	The cost of transferring one unit of type 1 capital from hot to warm stocks	18
VHW2	The cost of transferring one unit of type 2 capital from hot to warm stocks	18
VPC1	The cost of purchasing one unit of type 1 capital	16
VPC2	The cost of purchasing one unit of type 2 capital	16
VPH1	The cost of producing one unit of ammunition from type 1 hot stocks	17
VPH2	The cost of producing one unit of ammunition from type 2 hot stocks	17
VPIPE	The cost of transferring one unit of ammunition from the domestic to the in-theater stockpile	17
VPREP	The cost of prepositioning one unit of ammunition in the in-theater stockpile	46
VPW1	The cost of producing one unit of ammunition from type 1 warm stocks	17
VPW2	The cost of producing one unit of ammunition from type 2 warm stocks	17
VS	The cost of maintaining one unit of ammunition in the domestic stockpile for one time step	17
VSP	The cost of maintaining one unit of ammunition in the in-theater stockpile for one time step	17
VSPALV	The cost of holding one unit of ammunition in the in-theater stockpile during the final time step of the Mobilization/War period (if negative, this represents salvage value)	53

GLOSSARY OF INPUT PARAMETERS (concluded)

VSSALV	The cost of holding one unit of ammunition in the domestic stockpile during the final time step of the Mobilization/War period (if negative, this represents salvage value)	53
VW1	The cost of maintaining one unit of type 1 capital in warm stock for one time step	16
VW2	The cost of maintaining one unit of type 2 capital in warm stock for one time step	16
VWC1	The cost of transferring one unit of type 1 capital from warm to cold stocks	17
VWC2	The cost of transferring one unit of type 2 capital from warm to cold stocks	18
VWH1	The cost of transferring one unit of type 1 capital from warm to hot stocks	17
VWH2	The cost of transferring one unit of type 2 capital from warm to hot stocks	17

GLOSSARY OF MODEL VARIABLES

<u>Name</u>	<u>Definition</u>	<u>Location of First Use</u>
BC1	The amount of type 1 cold capital purchased at time step $t=1$	22
BC2	The amount of type 2 cold capital purchased at time step $t=1$	22
BW1	The amount of type 1 warm capital purchased during time step 1 as part of the linear portion of the purchase pattern	25
BW2	The amount of type 2 warm capital purchased during time step 1 as part of the linear portion of the purchase pattern	25
C1(t)	The amount of type 1 cold capital stocks held during time step t	10
C2(t)	The amount of type 2 cold capital stocks held during time step t	10
EC1	The amount of type 1 cold capital held during the Steady-state period	42
EC2	The amount of type 2 cold capital held during the Steady-state period	42
EPREP	The amount of ammunition explicitly prepositioned into the in-theater stockpile during the Steady-state period	43
ES	The total amount of ammunition held in stockpiles during the Steady-state period	42
EW1	The amount of type 1 warm capital held during the Steady-state period	42
EW2	The amount of type 2 warm capital held during the Steady-state period	42
H1(t)	The amount of type 1 hot capital stocks held during time step t	10
H2(t)	The amount of type 2 hot capital stocks held during time step t	10

GLOSSARY OF MODEL VARIABLES (contd)

IBW1	The amount of type 1 warm capital purchased during time step 1 in addition to BW1	26
IBW2	The amount of type 2 warm capital purchased during time step 1 in addition to BW2	26
PIPE(t)	The amount of ammunition transferred from the domestic to the in-theater stockpile beginning during time step t	11
S(t)	The amount of ammunition held in the domestic stockpile during time step t	11
SLPNC1	The negative component of the slope of the type 1 cold capital purchase pattern	22
SLPNC2	The negative component of the slope of the type 2 cold capital purchase pattern	22
SLPNW1	The negative component of the slope of the linear portion of the type 1 warm capital purchase pattern	26
SLPNW2	The negative component of the slope of the linear portion of the type 2 warm capital purchase pattern	26
SLPPC1	The positive component of the slope of the type 1 cold capital purchase pattern	22
SLPPC2	The positive component of the slope of the type 2 cold capital purchase pattern	22
SLPPW1	The positive component of the slope of the linear portion of the type 1 warm capital purchase pattern	26
SLPPW2	The positive component of the slope of the linear portion of the type 2 warm capital purchase pattern.	26
SP(t)	The amount of ammunition held in the in-theater stockpile during time step t	11
TCH1(t)	The amount of type 1 capital transferred from cold to hot stocks beginning during time step t	11
TCH2(t)	The amount of type 2 capital transferred from cold to hot stocks beginning during time step t	11
TCW1(t)	The amount of type 1 capital transferred from cold to warm stocks beginning during time step t	11

GLOSSARY OF MODEL VARIABLES (concluded)

TCW2(t)	The amount of type 2 capital transferred from cold to warm stocks beginning during time step t	11
THC1(t)	The amount of type 1 capital transferred from hot to cold stocks beginning during time step t	11
THC2(t)	The amount of type 2 capital transferred from hot to cold stocks beginning during time step t	11
THW1(t)	The amount of type 1 capital transferred from hot to warm stocks beginning during time step t	11
THW2(t)	The amount of type 2 capital transferred from hot to warm stocks beginning during time step t	11
TWC1(t)	The amount of type 1 capital transferred from warm to cold stocks beginning during time step t	11
TWC2(t)	The amount of type 2 capital transferred from warm to cold stocks beginning during time step t	11
TWH1(t)	The amount of type 1 capital transferred from warm to hot stocks beginning during time step t	11
TWH2(t)	The amount of type 2 capital transferred from warm to hot stocks beginning during time step t	11
W1(t)	The amount of type 1 warm capital stocks held during time step t	10
W2(t)	The amount of type 2 warm capital stocks held during time step t	10

APPENDIX B

STOCKPILE/PRODUCTION BASE MODEL
FORTRAN LISTING


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20030 FORMAT(1F0,*BUY PERIOD SLOPES HAVE BEEN SET*)
      IF(KC3.NF.0)PRINT 20040
20040 FORMAT(1F0,*CAPITAL STOCK TO STOCKPILE RATIO HAS BEEN SET*)
      IF(KC4.FG.1)PRINT 20042
      IF(KC4.FG.2)PRINT 20044
20042 FORMAT(1F0,*INITIAL WARM CAPITAL PURCHASES ELIMINATED*)
20044 FORMAT(1F0,*LEVEL WARM CAPITAL PURCHASES ELIMINATED*)
      PRINT 20015,NLAG,NPURCH,NSS,ISTEP
20015 FORMAT(1F0,*NLAG= *15,AX*NDURCH= *15,AX*NSS= *15,AX*ISTEP= *15)
      PRINT 20050
20050 FORMAT(1F0,*COSTS *,50(1H*))
      READ 20175,VC1,VC2,VW1,VW2,VPW1,VPW2,VH1,VH2
      READ 20175,VPH1,VPH2,VPC1,VPC2,VCW1,VCW2,VCH1,VCH2
      READ 20175,VWH1,VWH2,VWC1,VWC2,VHC1,VHC2,VHW1,VHW2
      READ 20065,VPIF,VS,VSP,VSSALV,VSPALV,VBSALV,VPREP,R
20065 FORMAT(1F10.3)
      READ 20060,MA,MR,AMULT,UMULT
20060 FORMAT(2I5,2F10.3)
      PRINT 20070
20070 FORMAT(1F0,*VC1*12X*VC2*12X*VW1*12X*VW2*12X*VPW1*11X*VPW2*11X*VH1*
112X*VH2*)
      PRINT 20080,VC1,VC2,VW1,VW2,VPW1,VPW2,VH1,VH2
20080 FORMAT(1F ,8(F12.4,3X))
      PRINT 20090
20090 FORMAT(1F0,*VPH1*11X*VPH2*11X*VPC1*11X*VPC2*11X*VCW1*11X*VCW2*11X*
1VCH1*11X*VCH2*)
      PRINT 20100,VPH1,VPH2,VPC1,VPC2,VCW1,VCW2,VCH1,VCH2
20100 FORMAT(1F ,8(F12.4,3X))
      PRINT 20110
20110 FORMAT(1F0,*VWH1*11X*VWH2*11X*VWC1*11X*VWC2*11X*VHC1*11X*VHC2*11X*
1VHW1*11X*VHW2*)
      PRINT 20120,VWH1,VWH2,VWC1,VWC2,VHC1,VHC2,VHW1,VHW2
20120 FORMAT(1F ,8(F12.4,3X))
      PRINT 20130
20130 FORMAT(1F0,*VPIF*10X*VS*12X*VSP*12X*VSSALV*9X*VSPALV*9X*VBSALV*9X
1VPREP*10X*R*)
      PRINT 20140,VPIF,VS,VSP,VSSALV,VSPALV,VBSALV,VPREP,R
20140 FORMAT(1F ,8(F12.4,3X))
      PRINT 20150
20150 FORMAT(1F0,*MA*13X*MR*13X*AMULT*10X*UMULT*)
      PRINT 20160,MA,MR,AMULT,UMULT
20160 FORMAT(1F ,15,10X,15,10X,2(F12.4,3X))
C
      PRINT 20170
20170 FORMAT(1F0,*CAPITAL/OUTPUT RATIOS *,33(1H*))
      READ 20175,KW1,KW2,KH1,KH2
20175 FORMAT(1F10.4)
      PRINT 20180
20180 FORMAT(1F0,*KW1*12X*KW2*12X*KH1*12X*KH2*)
      PRINT 20190,KW1,KW2,KH1,KH2
20190 FORMAT(1F ,4(F12.3,3X))
      PRINT 20200
20200 FORMAT(1F0,*DETERMINATION PATFS *,36(1H*))
      READ 20210,DC1,DC2,DW1,DW2,DH1,DH2,DS,DSH
20210 FORMAT(1F10.4)
      PRINT 20220
20220 FORMAT(1F0,*DC1*12X*DC2*12X*DW1*12X*DW2*12X*DH1*12X*DH2*12X*DS*
113X*DSH*)

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PRINT 22230,DC1,DC2,DW1,DW2,DH1,DH2,DS,USP
20230 FORMAT(1H ,A(F12.3,3X))
PRINT 22240
20240 FORMAT(1H-,*TIME LAGS *,46(1H*))
READ 20250,LP1,LP2,LWC1,LWC2,LCH1,LCH2,LWH1,LWH2,LHC1,LHC2,LHW1,
1LHW2,LWC1,LWC2,1PIPE
20250 FORMAT(16I5)
PRINT 22260
20260 FORMAT(1H0,*LP1*4Y*LP2*4X*1CW1*3X*1CW2*3X*LCH1*3X*LCH2*3X*LWH1*3X*
1LWH2*3X*LHC1*3X*LHC2*3Y*LHW1*3X*LHW2*3X*LWC1*3X*LWC2*3X*1PIPE*)
PRINT 22270,LP1,LP2,LWC1,LWC2,LCH1,LCH2,LWH1,LWH2,LHC1,LHC2,LHW1,
1LHW2,LWC1,LWC2,1PIPE
20270 FORMAT(1H ,15(I3,4X))
C
PRINT 22280
20280 FORMAT(1H-,*ORIGINALS *,46(1H*))
READ 20290,OMUN,OCOLD1,OCOLD2,OWARM1,OWARM2
20290 FORMAT(8F10.4)
PRINT 22300
20300 FORMAT(1H0,*CMUN*11Y*OCOLD1*9X*OCOLD2*9X*OWARM1*9X*OWARM2*)
PRINT 22310,CMUN,OCOLD1,OCOLD2,OWARM1,OWARM2
20310 FORMAT(1H ,A(F12.4,3X))
OMLNX=(OWARM1/KW1)*NLAG+(OWARM2/KW2)*NLAG
PRINT 22315,CMUNX
20315 FORMAT(1H0,10X,*PRODUCTION DURING NLAG = *,F10.4)
OMLN=OMLN+OMUNX
PRINT 22316,CMUN
20316 FORMAT(1H0,10X,*INVENTORY AFTER NLAG = *,F10.4)
PRINT 22320
20320 FORMAT(1H-,*BUDGETS *,48(1H*))
READ 20330,BPBUNG,FBUNG
READ 20330,(BUDG(I),I=1,ISTEP)
20330 FORMAT(8F10.4)
PRINT 22340,BPBUNG
20340 FORMAT(1H0,*BPBUNG= *,F12.3)
PRINT 22350,EBUNG
20350 FORMAT(1H0,*EBUNG= *,F12.3)
PRINT 22360,(BUNG(I),I=1,ISTEP)
20360 FORMAT(1H0,*BUDG= *,A(F12.3,3X))
PRINT 22370
20370 FORMAT(1H-,*DEMANDS *,48(1H*))
I=1STEP
READ 20380,BPDFM,SSDEM
READ 20380,(DD(J),J=1,I)
READ 20380,(FD(J),J=1,I)
20380 FORMAT(8F10.4)
PRINT 22390,BPDFM
20390 FORMAT(1H0,*BPDFM= *,F12.4)
PRINT 22400,SSDEM
20400 FORMAT(1H0,*SSDEM= *,F12.4)
PRINT 22410,(DD(J),J=1,I)
20410 FORMAT(1H0,*DD= *,A(F12.3,3X))
PRINT 22420,(FD(J),J=1,I)
20420 FORMAT(1H0,*FD= *,A(F12.3,3X))
PRINT 22430
20430 FORMAT(1H-,*UPPER BOUNDS *.43(1H*))
I=1
READ 20440,URPRF

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      READ 20440,(UBSP(J),J=1,ISTEP)
      READ 20440,(UBPIPF(J),J=1,1)
20440  FORMAT(8F10.4)
      PRINT 20450,UBPPFD
20450  FORMAT(I10,*LBPPFD=*,F12.4)
      PRINT 20460,(UBSP(J),J=1,1,ISTEP)
20460  FORMAT(I10,*UBSP=*(F12.3,3X))
      PRINT 20470,(UBPIPF(J),J=1,1)
20470  FORMAT(I10,*UBPIPF=*,(F12.3,3X))
      PRINT 20480
20480  FORMAT(I10,*OPTIONAL INFORMATION **5(1H*))
      IF(KC1.EQ.0)GO TO 21015
      READ 20490,ENDS,ENDSP,ENDPR,U
20490  FORMAT(8F10.4)
      PRINT 20500,ENDS,ENDSP,ENDPR,U
20500  FORMAT(I10,*ENDS=*F12.4,2X*ENDSP=*F12.4,2X*ENDPR(1=*F12.4)
21010  IF(KC2.EQ.0)GO TO 21025
      READ 20510,SLOPC1,SLOPC2,SLOPW1,SLOPW2
20510  FORMAT(8F10.4)
      PRINT 20520,SLOPC1,SLOPC2,SLOPW1,SLOPW2
20520  FORMAT(I10,*SLOPC1=*F12.4,2X*SLOPC2=*F12.4,2X*SLOPW1=*F12.4,2X
1*SLOPW2=*F12.4)
21020  IF(KC3.EQ.0)GO TO 21035
      READ 20530,RATIO
20530  FORMAT(8F10.4)
      PRINT 20540,RATIO
20540  FORMAT(I10,*RATIO=*F12.4)
21030  CONTINUE
      ZZ1=C.
      ZY1=C.
      LII=NLAG+NPURCH
      IF (LII.(1.1) GO TO 40005
      LL=1
      DO 40003 J=LL,LII
      ZZ1=ZZ1+((1.-DW1)**(J-1))/(1.+R)**J)
40003  ZY1=ZY1+((1.-DW2)**(J-1))/(1.+R)**J)
40005  CONTINUE
      Z72=C.
      ZY2=C.
      IF (LII.(1.1) GO TO 40010
      LL=1
      DO 40007 J=LL,LII
      Z72=Z72+FUNCT5(DW1,DS,II)/(1.+R)**II)
40007  ZY2=ZY2+FUNCT5(DW2,DS,II)/(1.+R)**II)
40010  CONTINUE
      Z73=1./((1.+R)**(1-CW1))
      ZY3=1./((1.+R)**(1-CW2))
      Z74=1./((1.+R)**(1-CW1-LP1))
      ZY4=1./((1.+R)**(1-CW2-LP2))
      Z75=FUNCT5(DW1,DS,NPURCH)
      ZY5=FUNCT5(DW2,DS,NPURCH)
      Z77=(VW1+VPW1/KW1)*Z71+VS*Z2/KW1
      Z77=Z77*CWARM1
      ZY7=(VW2+VPW2/KW2)*ZY1+VS*ZY2/KW2
      ZY7=ZY7*CWARM2
      TCOSTS=Z77+ZYZ
      PRINT 40015,ZZZ,Z7Y
40015  FORMAT(I10,*PRODUCTION COSTS FROM ORIGINAL WARM1=*F12.3* PRODUCT

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ION COSIS FROM OPTIMAL WAKU2= *F12.3)
Z1=FUNCT1(DW1,NPIURCH)
Z2=FUNCT2(DW1,NPIURCH)
Z3=FUNCT1(DW2,NPIURCH)
Z4=FUNCT2(DW2,NPIURCH)
Z5=FUNCT1(DC1,NPIURCH)
Z6=FUNCT2(DC1,NPIURCH)
Z7=FUNCT1(DC2,NPIURCH)
Z8=FUNCT2(DC2,NPIURCH)
Z0=0.
DO 21040 I=1,NPIURCH
21040 Z0=Z0+FUNCT1(DW1,I)*((1.-US)**(NPIURCH-I))
Z0=Z0/KW1
Z9=0.
DO 21050 I=1,NPIURCH
21050 Z9=Z9+FUNCT1(DW2,I)*((1.-US)**(NPIURCH-I))
Z9=Z9/KW2
Z10=0.
DO 21060 I=1,NPIURCH
21060 Z10=Z10+FUNCT2(DW1,I)*((1.-DS)**(NPIURCH-I))
Z10=Z10/KW1
Z11=0.
DO 21070 I=1,NPIURCH
21070 Z11=Z11+FUNCT2(DW2,I)*((1.-DS)**(NPIURCH-I))
Z11=Z11/KW2
Z12=FUNCT1(DS,NPIURCH)
Z13=0.
DO 21080 I=1,NPIURCH
21080 Z13=Z13+(1.+R)**(1-P1-I)
Z13=Z13*VPC1
DO 21090 I=1,NPIURCH

21090 Z13=Z13+VPC1*FUNCT1(DC1,I)/((1.+R)**I)
Z14=0.
DO 21100 I=1,NPIURCH
21100 Z14=Z14+(VPC1*(FLOAT(I)-1.)/((1.+R)**(I-LP1)))+(VPC1*FUNCT2(DC1,I)/
1((1.+R)**I))
Z15=0.
DO 21110 I=1,NPIURCH
21110 Z15=Z15+(VPC2/((1.+R)**(I-LP2)))+(VPC2*FUNCT1(DC2,I)/((1.+R)**I))
Z16=0.
DO 21120 I=1,NPIURCH
21120 Z16=Z16+(VPC2*(FLOAT(I)-1.)/((1.+R)**(I-LP2)))+(VPC2*FUNCT2(DC2,I)/
1((1.+R)**I))
Z17=0.
DO 21130 I=1,NPIURCH
21130 Z17=Z17+(VPW1*FUNCT1(DW1,I)/((1.+R)**I))+(VPW1/KW1)*FUNCT1(DW1,I)/
1((1.+R)**I))+(VPC1/KW1)*FUNCT3(US,DW1,I)/((1.+R)**I))+(VCW1/((1.+R)
2**((I-LCW1)))+(VPC1/((1.+R)**(1-LCW1-LP1)))
Z19=0.
DO 21140 I=1,NPIURCH
21140 Z19=Z19+(VPW2*FUNCT1(DW2,I)/((1.+R)**I))+(VPW2/KW2)*FUNCT1(DW2,I)/
1((1.+R)**I))+(VPC2/KW2)*FUNCT3(US,DW2,I)/((1.+R)**I))+(VCW2/((1.+R)
2**((I-LCW2)))+(VPC2/((1.+R)**(1-LCW2-LP2)))
Z18=0.
DO 21150 I=1,NPIURCH
21150 Z18=Z18+(VPW1*FUNCT2(DW1,I)/((1.+R)**I))+(VPW1/KW1)*FUNCT2(DW1,I)/
1((1.+R)**I))+(VPC1/KW1)*FUNCT4(US,DW1,I)/((1.+R)**I))+(VCW1*(FLOAT(

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211-1.)/(1.+R)**(1-LCW1)))+(VPC1*(FLOAT(I)-1.)/(1.+R)**(1-LCW1-
3LP1)))
Z20=0.
DO 2116 I=1,NPURCH
2116 Z20=Z20+(VW2*FUNCT2(DW2,I)/(1.+R)**I)+(VPW2/KW2)*FUNCT2(DW2,I)/
1(1.+R)**I)+(VC/KW2)*FUNCT4(US,DW2,I)/(1.+R)**I)+(VCW2*(FLOAT(
21)-1.)/(1.+R)**(1-LCW2)))+(VPC2*(FLOAT(I)-1.)/(1.+R)**(1-LCW2-
3LP2)))
Z21=0.
Z22=0.
Z23=0.
Z24=0.
Z25=0.
Z26=0.
Z27=0.
Z28=0.
Z29=0.
Z30=0.
Z31=0.
Z32=0.
Z33=0.
IF(NSS.EQ.0)GO TO 2200
DO 2117 I=1,NSS
Z21=Z21+(VPC1*DC1/(1.+R)**(1-LP1+NPURCH)))+(VC1/(1.+R)**(1+NPURCH
1H)))
Z22=Z22+(VPC2*DC2/(1.+R)**(1-LP2+NPURCH)))+(VC2/(1.+R)**(1+NPURCH
1H)))
Z23=Z23+(VPW1/KW1)/(1.+R)**(1+NPURCH)))+(VW1/(1.+R)**(1+NPURCH
1)))+(VCW1*DW1/(1.+R)**(1-LCW1+NPURCH)))+(VPC1*DW1/(1.+R)**(1-LCW1
2-LP1+NPURCH)))
Z24=Z24+((VW2+VPW2/KW2)/(1.+R)**(1+NPURCH)))+(VCW2*DW2/(1.+R)**(
1-LCW2+NPURCH)))+(VPC2*DW2/(1.+R)**(1-LCW2-LP2+NPURCH)))
2117 Z25=Z25+VS/(1.+R)**(1+NPURCH))
Z26=VPC1*DC1*FLOAT(NSS)
Z27=VPC2*DC2*FLOAT(NSS)
Z28=(VPC1*DW1+VPW1/KW1)*FLOAT(NSS)
Z29=(VPC2*DW2+VPW2/KW2)*FLOAT(NSS)
2200 CONTINUE
Z26=0.
Z27=0.
Z28=0.
Z29=0.
Z30=0.
Z31=0.
Z32=0.
Z33=0.
DO 2201 I=1,NPURCH
Z30=Z30+VPC1*(FLOAT(I)-1.)
Z31=Z31+VPC2*(FLOAT(I)-1.)
Z28=Z28+(VPW1/KW1)*FUNCT1(DW1,I)
Z29=Z29+(VPW2/KW2)*FUNCT1(DW2,I)
Z32=Z32+(VPW1/KW1)*FUNCT2(DW1,I)+VPC1*(FLOAT(I)-1.)
2201 Z33=Z33+(VPW2/KW2)*FUNCT2(DW2,I)+VPC2*(FLOAT(I)-1.)
Z26=VPC1*FLOAT(NPURCH)
Z27=VPC2*FLOAT(NPURCH)
Z28=Z28+VPC1*FLOAT(NPURCH)
Z29=Z29+VPC2*FLOAT(NPURCH)
KRU8=0
12 FORMAT(F10.6)
PRINT 15
15 FORMAT(1F1,*PROBLEM INFORMATION*,/
NMPCWS=I*+11*ISTEP

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      IF (KC1.EQ.1) NMR0WS=NMR0WS+3
      IF (KC2.EQ.1) NMR0WS=NMR0WS+4
      IF (KC3.EQ.1) NMR0WS=NMR0WS+1
      IF (NSS.GT.0) NMR0WS=NMR0WS+1
      IF (KC4.EQ.1) NMR0WS=NMR0WS+1
      NUMVAR=K+23*ISTEP
      NUMVAR=NUMVAR+2
      MAXLP=5

      PRINT 20,NMR0WS
      FORMAT(1F,20X,110,4HROWS)
      PRINT 20,NUMVAR
      FORMAT(1F,20X,110,9HVARIALES)
      PRINT 30,MAXLP
      FORMAT(1F,20X,110,5X,26H10 PROBLEMS WILL BE SOLVED)
      IF (KR0H.NE.0) PRINT 35,RUB
      FORMAT(1F,20X,22HUSER SUPPLIED RUB IS--F10.6)
      IF (IXPR0H.NE.0) PRINT 40
      FORMAT(1F,20X,59HTHE USER REQUESTS THAT ALL FEASIBLE POINTS FOUND
1 RE PRINTED)
      IF (K1.NE.0) PRINT 45
      FORMAT(1F,20X,50HTHE USER REQUESTS THAT ALL LP SOLUTIONS BE PRINT
45 IED)
      IF (K2.NE.0) PRINT 50
      FORMAT(1F,20X,44HTHE USER REQUESTS THAT THE MATRIX BE PRINTED)
      IF (K3.NE.0) PRINT 51
      FORMAT(1F,20X,43HTHE USER REQUESTS LP INFORMATION BE PRINTED)
      IF (K4.NE.0) PRINT 52
      FORMAT(1F,20X,66HTHE USER REQUESTS THAT THE ENTIRE LIST BE PRINTE
52 ID AFTER EACH STAGE)
      IF (K5.NE.0) PRINT 53
      FORMAT(1F,20X,43HTHE USER REQUESTS THAT THE MATRIX BE SCALED)
      ISTEP(1)=0
      ISTEP(2)=1
      ISTEP(3)=1
      IF (NSS.EQ.0) ISTEP(2)=-1
      IF (NSS.EQ.0) ISTEP(3)=-1
      ISTEP(4)=-1
      ISTEP(5)=-1
      ISTEP(6)=-1
      ISTEP(7)=1
      ISTEP(8)=1
      ISTEP(9)=1
      ISTEP(10)=1
      LL=11
      LU=10+8*ISTEP
      DO 10010 I=LL,LU
10010 ISTEP(I)=-1
      LL=11+8*ISTEP
      LU=15+11*ISTEP
      DO 10020 I=LL,LU
10020 ISTEP(I)=1
      IF (KC1.EQ.0) GO TO 10030
      LU=LU+1
      ISTEP(LU)=1
      LU=LU+1
      ISTEP(LU)=1
      LU=LU+1

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        ISTYPE(I)=1
10030 IF(KC2.EQ.0)GO TO 10040
        DO 10035 I=1,4
        LII=LII+1
10035 ISTYPE(I)=-1
10040 IF(KC3.EQ.0)GO TO 10050
        LII=LII+1
        ISTYPE(I)=-1
10050 IF(KC5.EQ.0)GO TO 10060
        LII=LII+1
        ISTYPE(I)=-1
C      FNC OF SETTING ROW TYPE
10060 IF(KC4.EQ.0)GO TO 10065
        LII=LII+1
        ISTYPE(I)=-1
10065 CONTINUE
        PRINT40
        60 FORMAT(1H0,10HROW TYPE=)
        PRINT 60,(ISTYPE(I),I=1,NMROWS)
        65 FORMAT(1H , 40I2)
        DO 10070 I=1,NMROWS
C      VARIABLE CARDS
10070 ICHK(I)=0
        PRINT 70
        75 FORMAT(1H0,17HCONVEYITY FLAGS=,/)
        PRINT 75,(ICHK(I),I=1,NMROWS)
        80 FORMAT(1H ,80I1)
C      *****NOW SET UP CUTS VECTOR, KLO, AND KRO**
        PRINT 90
        90 FORMAT(1H0,27HVariable CARDS REPRODUCED=,/)
        DO 100 I=1,NMVAR
        NOVAP=1
        NOINC=0
        WORD=5HALT0.
        PHS CARDS
C      IF(NOVAP.NE.1)CALL FRR(1)
        IF(NOINC.EQ.0)115,160
115      IF(I.EQ.1)116,117
116      KLO(I)=1
        KRO(I)=1
        GO TO 100
117      IX=KRO(I-1)+1
        IF(IX.GT.MAXCUT)CALL EPR(2)
        KLO(I)=KRO(I-1)+1
        KRO(I)=KLO(I)
        GO TO 100
120      IF(I.EQ.1)122,124
122      KLO(I)=1
        GO TO 126
124      IX=KRO(I-1)+1
        IF(IX.GT.MAXCUT)CALL EPR(2)
        KLO(I)=KRO(I-1)+1
126 IF((KLO(I)+NOINC).GT.MAXCUT)CALL FRR(2)
        KRO(I)=KLO(I)+NOINC
        IF(WORD.EQ.WMM)GO TO 145
        I1=KLO(I)
        I2=KRO(I)
        READ 130,CUTS(I1),CUTS(I2)

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130      FORMAT(2F10.4)
      PRINT 135,CUTS(I1),CUTS(I2)
135      FORMAT(1H,2G10.4)
      IF ((I2-I1).EQ.1) GO TO 100
      IX=I2-I1-1
      DO 140 J=1,IX
140      CUTS(I1+J)=CUTS(I1)+J*(CUTS(I2)-CUTS(I1))/NOINC
      GO TO 100
145      CONTINUE
C      *****HERE IF WE ARE TO READ IN CUTS MANUALLY
      IW=KLO(I)
      IZ=KRO(I)
      READ 150,(CUTS(J),J=1W,IZ)
150      FORMAT(8F10.4)
      PRINT 155,(CUTS(J),J=1W,IZ)
155      FORMAT(7F,8G12.4)
100      CONTINUE
C      *****WE HAVE COMPLETED READING BOUNDS AND CUTS
      PRINT 160
160      FORMAT(1H,24HRHS CARD(S) REPRODUCED=,/)
      R(1)=0.
      R(2)=OWARM1*((1.-OW1)**(NPIHCH-1))
      R(3)=OWARM2*((1.-OW2)**(NPIHCH-1))
      R(4)=OCOLD1*((1.-OC1)**(NPIHCH-1))
      R(4)=R(4)+R(2)
      R(5)=OCOLD2*((1.-OC2)**(NPIHCH-1))
      R(5)=R(5)+R(3)
      R(6)=HPCDEM*712-OMIUN*((1.-OC)**(NPIHCH-1))
      R(6)=R(6)-(ZZ5*OWARM1/KW1)-(ZY5*OWARM2/KW2)
      R(7)=-HPCDEM
      R(7)=R(7)+OWARM1/KW1+OWARM2/KW2
      R(8)=-HPCDEM
      R(8)=R(8)+R(2)/KW1+R(3)/KW2
      R(9)=0
      R(10)=URPREP
      LL=11
      LU=10+6*ISTEP
      DO 10080 I=LL,LU
10080  R(I)=0.
      LL=11+6*ISTEP
      LU=10+7*ISTEP
      DO 10090 I=LL,LU
      IT=I-LL+1
10090  R(I)=UD(II)
      LL=LU+1
      LU=10+6*ISTEP
      DO 10100 I=LL,LU
      IT=I-LL+1
10100  R(I)=FD(II)
      LL=LU+1
      LU=10+9*ISTEP
      DO 10110 I=LL,LU
      IT=I-LL+1
10110  R(I)=UMCP(II)
      LL=LU+1
      LU=9+10*ISTEP
      DO 10120 I=LL,LU
      IT=I-LL+1

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10120 R(I)=IISTYPE(II)
      LI=LI+1
      LU=LI+ISTEP
      DO 10140 I=LL,LU
      IT=I-LL+1
10140 R(I)=RUNC(II)
      LI=LI+1
      R(LI)=HPRUDG
      LU=LI+1
      R(LU)=FPR(DG)
      LI=LI+1
      R(LI)=0.
      LU=LI+1
      R(LU)=0.
      LI=LI+1
      R(LI)=0.
      LU=LI+1
      R(LU)=0.
      IF(KC1.FG.0)GO TO 10150
      LU=LI+1
      R(LU)=-FANDS
      LI=LI+1
      R(LU)=-FANDSP
      LI=LI+1
      R(LU)=-FANDPRC
10150 IF(KC2.FG.0) GO TO 10160
      LU=LI+1
      R(LU)=S1(CPC1)
      LI=LI+1
      R(LU)=S1(CPC2)
      LI=LI+1
      R(LU)=S1(CPW1)
      LI=LI+1
      R(LU)=S1(CPW2)
10160 IF(KC3.FG.0)GO TO 10170
      LU=LI+1
      R(LU)=0.
10170 IF(KC4.FG.0)GO TO 10180
      LU=LI+1
      R(LU)=SCFEM
10180 IF(KC4.FG.0)GO TO 10185
      LU=LI+1
      R(LU)=0.
10185 CONTINUE
C      END OF PHS
C      FILL IN COLUMNS
PRINT 170,(R(I),I=1,NMROWS)
170 FORMAT(1F,8G12.4)
C
C      SFT NROW,R(.),ISTYPE(.)
C
      NROW=NMROWS
      DO 9000 JJ=1,NUMVAR
      J1=KLO(JJ)
      J2=KPO(JJ)
      IF (J1.FG.J2) GO TO 9000
      NROW=NROW+1
9000 CONTINUE

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C      I1=NMROWS+1
      DO 9010 I=1,NROW
      H(I)=1.
      ISTEP(I)=-1
9010 CONTINUE
C
C      ADD SLACKS TO COEFFICIENT MATRIX
C
      NFLEM=0
      NCOL=0
      DO 9100 I=1,NROW
      NELEM=NELEM+1
      NCOL=NCOL+1
      IA(NFLEM)=I
      A(NFLEM)=1.
      LA(NCOL)=NELEM
9100 CONTINUE
      LA(NCOL+1)=NELEM+1
C
C
C      FILL IN COEFFICIENT MATRIX
C
      NCCGUR=1
      DO 9400 JJ=1,NUMVAR
      J1=KLO(JJ)
      J2=KRO(JJ)
      IF (J1.IT.J2) GO TO 9300
C
      LJ=JJ
      IF(JJ.GF.19,A.JJ,1,F.(19+ISTEP))LJ=19
      IF(JJ.GF.(19+ISTEP),A.JJ,1,F.(19+2*ISTEP))LJ=20
      IF(JJ.GF.(19+2*ISTEP),A.JJ,1,F.(19+3*ISTEP))LJ=21
      IF(JJ.GF.(19+3*ISTEP),A.JJ,1,F.(19+4*ISTEP))LJ=22
      IF(JJ.GF.(19+4*ISTEP),A.JJ,1,F.(19+5*ISTEP))LJ=23
      IF(JJ.GF.(19+5*ISTEP),A.JJ,1,F.(19+6*ISTEP))LJ=24
      IF(JJ.GF.(19+6*ISTEP),A.JJ,1,F.(19+7*ISTEP))LJ=25
      IF(JJ.GF.(19+7*ISTEP),A.JJ,1,F.(19+8*ISTEP))LJ=26
      IF(JJ.GF.(19+8*ISTEP),A.JJ,1,F.(19+9*ISTEP))LJ=27
      IF(JJ.GF.(19+9*ISTEP),A.JJ,1,F.(19+10*ISTEP))LJ=28
      IF(JJ.GF.(19+10*ISTEP),A.JJ,1,F.(17+11*ISTEP))LJ=29
      IF(JJ.GF.(18+11*ISTEP),A.JJ,1,F.(16+12*ISTEP))LJ=30
      IF(JJ.GF.(17+12*ISTEP),A.JJ,1,F.(15+13*ISTEP))LJ=31
      IF(JJ.GF.(16+13*ISTEP),A.JJ,1,F.(14+14*ISTEP))LJ=32
      IF(JJ.GF.(15+14*ISTEP),A.JJ,1,F.(13+15*ISTEP))LJ=33
      IF(JJ.GF.(14+15*ISTEP),A.JJ,1,F.(12+16*ISTEP))LJ=34
      IF(JJ.GF.(13+16*ISTEP),A.JJ,1,F.(11+17*ISTEP))LJ=35
      IF(JJ.GF.(12+17*ISTEP),A.JJ,1,F.(10+18*ISTEP))LJ=36
      IF(JJ.GF.(11+18*ISTEP),A.JJ,1,F.(9+19*ISTEP))LJ=37
      IF(JJ.GF.(10+19*ISTEP),A.JJ,1,F.(8+20*ISTEP))LJ=38
      IF(JJ.GF.(9+20*ISTEP),A.JJ,1,F.(7+21*ISTEP))LJ=39
      IF(JJ.GF.(8+21*ISTEP),A.JJ,1,F.(6+22*ISTEP))LJ=40
      IF(JJ.GF.(7+22*ISTEP),A.JJ,1,F.(5+23*ISTEP))LJ=41
      IF(JJ.EQ.(6+23*ISTEP))LJ=42
      IF(JJ.EQ.(7+23*ISTEP))LJ=43
      ITVAR=0
      IF(LJ.FQ.19)ITVAR=JJ-19+1
      IF(LJ.FQ.20)ITVAR=JJ-19-ISTEP+1

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IF (LJ.EQ.21) ITVAR=JJ-19-2*ISTEP+1
IF (LJ.EQ.22) ITVAR=JJ-19-3*ISTEP+1
IF (LJ.EQ.23) ITVAR=JJ-19-4*ISTEP+1
IF (LJ.EQ.24) ITVAR=JJ-19-5*ISTEP+1
IF (LJ.EQ.25) ITVAR=JJ-19-6*ISTEP+1
IF (LJ.EQ.26) ITVAR=JJ-19-7*ISTEP+1
IF (LJ.EQ.27) ITVAR=JJ-19-8*ISTEP+1
IF (LJ.EQ.28) ITVAR=JJ-19-9*ISTEP+1
IF (LJ.EQ.29) ITVAR=JJ-19-10*ISTEP+1
IF (LJ.EQ.30) ITVAR=JJ-19-11*ISTEP+1
IF (LJ.EQ.31) ITVAR=JJ-17-12*ISTEP+1
IF (LJ.EQ.32) ITVAR=JJ-14-13*ISTEP+1
IF (LJ.EQ.33) ITVAR=JJ-15-14*ISTEP+1
IF (LJ.EQ.34) ITVAR=JJ-14-15*ISTEP+1
IF (LJ.EQ.35) ITVAR=JJ-13-16*ISTEP+1
IF (LJ.EQ.36) ITVAR=JJ-12-17*ISTEP+1
IF (LJ.EQ.37) ITVAR=JJ-11-18*ISTEP+1
IF (LJ.EQ.38) ITVAR=JJ-12-19*ISTEP+1
IF (LJ.EQ.39) ITVAR=JJ-9-20*ISTEP+1
IF (LJ.EQ.40) ITVAR=JJ-8-21*ISTEP+1
IF (LJ.EQ.41) ITVAR=JJ-7-22*ISTEP+1
DO 10190 I=1,NMPOWS
10190 YTEMP(1)=0.
DISC=(1.+R)**(NI*AG+NPUGH+NSS+ITVAR)
DISC=1./DISC
IF (ITVAR,GE,PA,AND,ITVAR,LT,MH) DISC=DISC*AMULT
IF (ITVAR,GE,MB) DISC=DISC*BMULT
GO TO (A0100,80200,80300,80400,80500,80600,80700,80800,80900,
181000,81100,81200,81300,81400,81500,81600,81700,81800,81900,82000,
282100,82200,82300,82400,82500,82600,82700,82800,82900,83000,83100,
383200,83300,83400,83500,83600,83700,83800,83900,84000,84100,84200,
484300),IJ
80100 CONTINUE
C HERE IF CB1
YTEMP(1)=Z13
YTEMP(4)=-Z5
I=10+1*ISTEP
YTEMP(1)=Z26
I=12+1*ISTEP
YTEMP(1)=-1.
GO TO 85000
80200 CONTINUE
C HERE IF CB2
YTEMP(1)=Z15
YTEMP(5)=-Z7
I=10+1*ISTEP
YTEMP(1)=Z27
I=13+1*ISTEP
YTEMP(1)=-1.
GO TO 85000
80300 CONTINUE
C HERE IF BW1
YTEMP(1)=Z17
YTEMP(2)=-Z1
YTEMP(4)=-Z1
YTEMP(6)=Z0
YTEMP(7)=-1./KW1
YTEMP(8)=-Z1/KW1

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I=10+11*ISTEP
YTEMP(1)=Z28
I=14+11*ISTEP
YTEMP(1)=-1.
I=15+11*ISTEP
IF(KC1.NF.0) I=I+3
IF(KC2.NF.0) I=I+4
IF(KC3.NF.0) I=I+1
IF(NSS.GT.0) I=I+1
IF(KC4.NF.2) GO TO R5000
I=I+1
YTEMP(1)=1.
GO TO R5000
R0400 CONTINUE
C HREF IF PW2
YTEMP(1)=Z19
YTEMP(3)=-Z3
YTEMP(5)=-Z3
YTEMP(6)=Z9
YTEMP(7)=-1./KW2
YTEMP(8)=-Z3/KW2
I=10+11*ISTEP
YTEMP(1)=Z29
I=15+11*ISTEP
YTEMP(1)=-1.
I=15+11*ISTEP
IF(KC1.NF.0) I=I+3
IF(KC2.NF.0) I=I+4
IF(KC3.NF.0) I=I+1
IF(NSS.GT.0) I=I+1
IF(KC4.NF.2) GO TO R5000
I=I+1
YTEMP(1)=1.
GO TO R5000
R0500 CONTINUE
C HREF IF SLPPC1
YTEMP(1)=Z14
YTEMP(4)=-Z6
I=10+11*ISTEP
YTEMP(1)=Z30
I=12+11*ISTEP
YTEMP(1)=1.-FLOAT(NPURCH)
I=15+11*ISTEP
IF(KC1.NF.0) I=I+3
I=I+1
IF(KC2.NF.0) YTEMP(1)=1.
GO TO R5000
R0600 CONTINUE
C HREF IF SLPNC1
YTEMP(1)=-Z14
YTEMP(4)=Z6
I=10+11*ISTEP
YTEMP(1)=-Z30
I=12+11*ISTEP
YTEMP(1)=FLOAT(NPURCH)-1.
I=15+11*ISTEP
IF(KC1.NF.0) I=I+3
I=I+1

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      IF (KC2.NF.0) YTEMP(I)=-1.
      GO TO 85000
80700 CONTINUE
C      HERE IF SLPPC2
      YTEMP(1)=Z16
      YTEMP(5)=-Z8
      I=10+11*ISTEP
      YTEMP(I)=Z31
      I=13+11*ISTEP
      YTEMP(I)=1.-FLOAT(NBURCH)
      I=15+11*ISTEP
      IF (KC1.NF.0) I=I+3
      I=I+2
      IF (KC2.NF.0) YTEMP(I)=1.
      GO TO 85000
80800 CONTINUE
C      HERE IF SLPNC2
      YTEMP(1)=-Z16
      YTEMP(5)=Z8
      I=10+11*ISTEP
      YTEMP(I)=-Z31
      I=13+11*ISTEP
      YTEMP(I)=FLOAT(NBURCH)-1.
      I=15+11*ISTEP
      IF (KC1.NF.0) I=I+3
      I=I+2
      IF (KC2.NF.0) YTEMP(I)=-1.
      GO TO 85000
80900 CONTINUE
C      HERE IF SLPPW1
      YTEMP(1)=Z18
      YTEMP(2)=-Z2
      YTEMP(4)=-Z2
      YTEMP(6)=Z10
      YTEMP(8)=-Z2/KW1
      I=10+11*ISTEP
      YTEMP(I)=Z32
      I=14+11*ISTEP
      YTEMP(I)=1.-FLOAT(NBURCH)
      I=15+11*ISTEP
      IF (KC1.NF.0) I=I+3
      I=I+3
      IF (KC2.NF.0) YTEMP(I)=1.
      GO TO 85000
81000 CONTINUE
C      HERE IF SLPNW1
      YTEMP(1)=-Z18
      YTEMP(2)=Z2
      YTEMP(4)=Z2
      YTEMP(6)=-Z10
      YTEMP(8)=Z2/KW1
      I=10+11*ISTEP
      YTEMP(I)=-Z32
      I=14+11*ISTEP
      YTEMP(I)=FLOAT(NBURCH)-1.
      I=15+11*ISTEP
      IF (KC1.NF.0) I=I+3
      I=I+3

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      IF (KC2.NE.0) YTEMP(I)=-1.
      GO TO H5000
81100 CONTINUE
C      HERE IF SLPPW2
      YTEMP(1)=Z20
      YTEMP(3)=-Z4
      YTEMP(5)=-Z4
      YTEMP(6)=Z11
      YTEMP(8)=-Z4/KW2
      I=10+11*ISTEP
      YTEMP(1)=Z33
      I=15+11*ISTEP
      YTEMP(1)=1.-FLOAT(NPURCH)
      I=15+11*ISTEP
      IF (KC1.NE.0) I=I+3
      I=I+4
      IF (KC2.NE.0) YTEMP(I)=1.
      GO TO H5000
81200 CONTINUE
C      HERE IF SLPNW2
      YTEMP(1)=-Z20
      YTEMP(3)=Z4
      YTEMP(5)=Z4
      YTEMP(6)=-Z11
      YTEMP(8)=Z4/KW2
      I=10+11*ISTEP
      YTEMP(1)=-Z33
      I=15+11*ISTEP
      YTEMP(1)=FLOAT(NPURCH)-1.
      I=15+11*ISTEP
      IF (KC1.NE.0) I=I+3
      I=I+4
      IF (KC2.NE.0) YTEMP(I)=-1.
      GO TO H5000
81300 CONTINUE
C      HERE IF FC1
      YTEMP(1)=Z21
      YTEMP(4)=1.
      LL=17
      LI=10+ISTEP
      DO 81305 I=LL,LI
      ITCONS=I-LL+1
      IF (ITCONS.EQ.1.AND.(ITCONS-LP1).GE.(1-NSS)) YTEMP(I)=1.
      IF (ITCONS.EQ.1.AND.(ITCONS-LP1).LT.(1-NSS)) YTEMP(I)=1.-DC1
      IF (ITCONS.GE.2.AND.(ITCONS-LP1).LE.0.AND.(ITCONS-LP1).GE.(1-NSS))
      ) YTEMP(I)=DC1
81305 CONTINUE
      I=11+11*ISTEP
      YTEMP(1)=Z34
      I=15+11*ISTEP
      IF (KC1.NE.0) I=I+3
      IF (KC2.NE.0) I=I+4
      I=I+1
      IF (KC3.NE.0) YTEMP(I)=1.
      GO TO H5000
81400 CONTINUE
C      HERE IF EC2
      YTEMP(1)=Z22

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      YTEMP(6)=1.
      LL=11+1*ISTEP
      LIJ=10+2*ISTEP
      DO A1405 I=LL,LIJ
        ITCONS=I-LL+1
        IF (ITCONS.EQ.1.AND.(ITCONS-LP2).GE.(1-NSS)) YTEMP(I)=1.
        IF (ITCONS.EQ.1.AND.(ITCONS-LP2).LT.(1-NSS)) YTEMP(I)=1.-DC2
        IF (ITCONS.GE.2.AND.(ITCONS-LP2).LE.0.AND.(ITCONS-LP2).GE.(1-NSS))
          YTEMP(I)=DC2
A1405 CONTINUE
      I=11+11*ISTEP
      YTEMP(1)=Z35
      I=15+11*ISTEP
      IF (KC1.NE.0) I=I+3
      IF (KC2.NE.0) I=I+4
      I=I+1
      IF (KC3.NE.0) YTEMP(I)=1.
      GO TO H5000
A1500 CONTINUE
C      HERE IF FW1
      YTEMP(1)=Z23
      YTEMP(2)=1.
      YTEMP(4)=1.
      LI=11
      LIJ=10+1*ISTEP
      DO A1505 I=LL,LIJ
        ITCONS=I-LL+1
        IF ((ITCONS-LP1).LE.0.AND.(ITCONS-LP1).GE.(1-NSS)) YTEMP(I)=DW1
A1505 CONTINUE
      LL=11+2*ISTEP
      LIJ=10+3*ISTEP
      DO A1510 I=LL,LIJ
        ITCONS=I-LL+1
        IF (ITCONS.EQ.1) YTEMP(I)=1.
        IF (ITCONS.GE.2.AND.(ITCONS-LCW1).LE.0.AND.(ITCONS-LCW1).GE.(1-NSS))
          YTEMP(I)=DW1
A1510 CONTINUE
      I=11+11*ISTEP
      YTEMP(1)=Z36
      I=15+11*ISTEP
      IF (KC1.NE.0) I=I+3
      IF (KC2.NE.0) I=I+4
      IF (KC3.NE.0) I=I+1
      IF (KC3.NE.0) YTEMP(I)=1.
      I=I+1
      IF (NSS.GT.0) YTEMP(I)=1./KW1
      GO TO H5000
A1600 CONTINUE
C      HERE IF FW2
      YTEMP(1)=Z24
      YTEMP(3)=1.
      YTEMP(5)=1.
      LL=11+1*ISTEP
      LIJ=10+2*ISTEP
      DO A1605 I=LL,LIJ
        ITCONS=I-LL+1
        IF ((ITCONS-LP2).LE.0.AND.(ITCONS-LP2).GE.(1-NSS)) YTEMP(I)=DW2
A1605 CONTINUE

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      LI=11+3*ISTEP
      LI=10+4*ISTEP
      DO 81615 I=LL,LI
      ITCONS=I-LL+1
      IF (ITCONS.EQ.1) YTEMP(I)=1.
      IF (ITCONS.GE.2.AND.(ITCONS-LCW2).LE.7.AND.(ITCONS-LCW2).GE.(1-NSS)
1) YTEMP(I)=DW2
81610 CONTINUE
      I=11+11*ISTEP
      YTEMP(1)=Z37
      I=15+11*ISTEP
      IF (KC1.NE.0) I=I+3
      IF (KC2.NE.0) I=I+4
      IF (KC3.NE.0) I=I+1
      IF (KC3.NE.0) YTEMP(I)=1.
      I=I+1
      IF (NSS.GT.0) YTEMP(I)=1./KW2
      GO TO 85000
81700 CONTINUE
C      HERE IF FS
      YTEMP(1)=Z25
      YTEMP(4)=-1.
      YTEMP(9)=-1.
      I=11+6*ISTEP
      YTEMP(1)=1.
      I=15+11*ISTEP
      IF (KC1.NE.0) I=I+3
      IF (KC2.NE.0) I=I+4
      IF (KC3.NE.0) I=I+1
      IF (KC3.NE.0) YTEMP(I)=-RATIO
      I=I+1
      IF (NSS.GE.1) YTEMP(I)=-NS
      GO TO 85000
81800 CONTINUE
C      HERE IF FPREP
      YTEMP(1)=VPREP/((1.+R)**(NSS+NMURCH))
      YTEMP(9)=1.
      YTEMP(15)=1.
      I=11+6*ISTEP
      YTEMP(1)=-1.
      I=11+7*ISTEP
      YTEMP(1)=1.
      GO TO 85000
81900 CONTINUE
C      HERE IF C1
      YTEMP(1)=VC1*DISC
      IF (ITVAR.EQ.1STEP) YTEMP(1)=VBSALV*DISC
      I=10
      I=I+ITVAR
      YTEMP(1)=-1.
      I=I+1
      IF (I.LE.(10+1STEP)) YTEMP(I)=1.-DC1
      GO TO 85000
82000 CONTINUE
C      HERE IF C2
      YTEMP(1)=VC2*DISC
      IF (ITVAR.EQ.1STEP) YTEMP(1)=VBSALV*DISC
      I=10+1STEP

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I=I+ITVAR
YTEMP(I)=-1.
I=I+1
IF (I.LE.(10+2*ISTEP)) YTEMP(I)=1.-DC2
GO TO 05000
R2100 CONTINUE
C
HERE IF W1
YTEMP(1)=DISC*(VW1+VPW1/KW1)
IF (ITVAR.EQ.ISTEP) YTEMP(1)=VBSALV*DISC
I=10+2*ISTEP
I=I+ITVAR
YTEMP(1)=-1.
I=I+1
IF (I.LE.(10+3*ISTEP)) YTEMP(I)=1.-DW1
I=10+6*ISTEP
I=I+ITVAR
YTEMP(1)=1./KW1
I=9+10*ISTEP
I=I+ITVAR
YTEMP(1)=VPW1/KW1
I=15+11*ISTEP
I=I+3
IF (KC1.NE.0.AND.ITVAR.EQ.ISTEP) YTEMP(1)=-1./KW1
GO TO 05000
R2200 CONTINUE
C
HERE IF W2
YTEMP(1)=DISC*(VW2+VPW2/KW2)
IF (ITVAR.EQ.ISTEP) YTEMP(1)=VBSALV*DISC
I=10+3*ISTEP
I=I+ITVAR
YTEMP(1)=-1.
I=I+1
IF (I.LE.(10+4*ISTEP)) YTEMP(I)=1.-DW2
I=10+6*ISTEP
I=I+ITVAR
YTEMP(1)=1./KW2
I=9+10*ISTEP
I=I+ITVAR
YTEMP(1)=VPW2/KW2
I=15+11*ISTEP
I=I+3
IF (KC1.NE.0.AND.ITVAR.EQ.ISTEP) YTEMP(1)=-1./KW2
GO TO 05000
R2300 CONTINUE
C
HERE IF H1
YTEMP(1)=DISC*(VH1+VPH1/KH1)
IF (ITVAR.EQ.ISTEP) YTEMP(1)=VBSALV*DISC
I=10+4*ISTEP
I=I+ITVAR
YTEMP(1)=-1.
I=I+1
IF (I.LE.(10+5*ISTEP)) YTEMP(I)=1.-DW3
I=10+6*ISTEP
I=I+ITVAR
YTEMP(1)=1./KH1
I=9+10*ISTEP
I=I+ITVAR
YTEMP(1)=VPH1/KH1

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I=15+11*ISTEP
I=I+3
IF (KCI,AE,0,AND,ITVAR,EQ,ISTEP) YTEMP(I)=-1./KH1
GO TO 05000
R2400 CONTINUE
C HERE IF 12
YTEMP(I)=DISC*(VH2+VPH2/KH2)
IF (ITVAR,EQ,ISTEP) YTEMP(I)=VBSALV*DISC
I=10+5*ISTEP
I=I+ITVAR
YTEMP(I)=-1.
I=I+1
IF (I.LE.,10+6*ISTEP) YTEMP(I)=1.-DH2
I=10+6*ISTEP
I=I+ITVAR
YTEMP(I)=1./KH2
I=9+10*ISTEP
I=I+ITVAR
YTEMP(I)=VPH2/KH2
I=15+11*ISTEP
I=I+3
IF (KCI,AE,0,AND,ITVAR,EQ,ISTEP) YTEMP(I)=-1./KH2
GO TO 05000
R2500 CONTINUE
C HERE IF FC1
YTEMP(I)=VPC1*DISC
I=10
I=I+ITVAR+LP1
IF (I.LE.,(10+ISTEP)) YTEMP(I)=1.
I=9+10*ISTEP
I=I+ITVAR
YTEMP(I)=VPC1
GO TO 05000
R2600 CONTINUE
C HERE IF FC2
YTEMP(I)=VPC2*DISC
I=10+ISTEP
I=I+ITVAR+LP2
IF (I.LE.,(10+2*ISTEP)) YTEMP(I)=1.
I=9+10*ISTEP
I=I+ITVAR
YTEMP(I)=VPC2
GO TO 05000
R2700 CONTINUE
C HERE IF S
YTEMP(I)=VS*DISC
IF (ITVAR,EQ,ISTEP) YTEMP(I)=VSSALV*DISC
I=10+6*ISTEP
I=I+ITVAR
YTEMP(I)=-1.
I=I+1
IF (I.LE.,(10+7*ISTEP)) YTEMP(I)=1.-DS
I=15+11*ISTEP
I=I+1
IF (KCI,AE,0,AND,ITVAR,EQ,ISTEP) YTEMP(I)=-1.
GO TO 05000
R2800 CONTINUE
C HERE IF SP

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YTEMP(I)=VSP*DISC
IF (ITVAR.EQ.ISTEP) YTEMP(I)=VSPALV*DISC
I=10+7*ISTEP
I=I+ITVAR
YTEMP(I)=-1
I=I+1
IF (I.LE.(10+8*ISTEP)) YTEMP(I)=1.-DCP
I=10+8*ISTEP
I=I+ITVAR
YTEMP(I)=1.
I=10+9*ISTEP
I=I+2
IF (KC1.NE.0.AND.ITVAR.EQ.ISTEP) YTEMP(I)=-1.
GO TO B=000
R2900 CONTINUE
C HERE IF PIPE
YTEMP(I)=VPIPE*DISC
I=10+6*ISTEP
I=I+ITVAR
IF (I.LE.(10+7*ISTEP)) YTEMP(I)=-1.
I=10+7*ISTEP
I=I+ITVAR+LPIPE
IF (I.LE.(10+8*ISTEP)) YTEMP(I)=1.
I=10+9*ISTEP
I=I+ITVAR
YTEMP(I)=1.
GO TO B=000
R3000 CONTINUE
C HERE IF TCW1
YTEMP(I)=VCW1*DISC
I=10
I=I+ITVAR
IF (I.LE.(10+ISTEP)) YTEMP(I)=-1.
I=10+2*ISTEP
I=I+ITVAR+LCW1
IF (I.LE.(10+3*ISTEP)) YTEMP(I)=1.
GO TO B=000
R3100 CONTINUE
C HERE IF TCW2
YTEMP(I)=VCW2*DISC
I=10+ISTEP
I=I+ITVAR
IF (I.LE.(10+2*ISTEP)) YTEMP(I)=-1.
I=10+3*ISTEP
I=I+ITVAR+LCW2
IF (I.LE.(10+4*ISTEP)) YTEMP(I)=1.
GO TO B=000
R3200 CONTINUE
C HERE IF TCH1
YTEMP(I)=VCH1*DISC
I=10
I=I+ITVAR
IF (I.LE.(10+ISTEP)) YTEMP(I)=-1.
I=10+4*ISTEP
I=I+ITVAR+LCH1
IF (I.LE.(10+5*ISTEP)) YTEMP(I)=1.
GO TO B=000
R3300 CONTINUE

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C      HERR IF TCH2
      YTEMP(1)=VCH2*DTSC
      I=10+ISTEP
      I=I+ITVAR
      IF(I.LE.(10+2*ISTEP))YTEMP(I)=-1.
      I=10+5*ISTEP
      I=I+ITVAR+LCH2
      IF(I.LE.(10+6*ISTEP))YTEMP(I)=1.
      GO TO 00000
R3400 CONTINUE
C      HERR IF TWH1
      SUM=0.
      KK=1
      KKK=1WH1
      DO R3405 I=KK,KKK
R3405 SUM=SUM+(VPW1/KW1)*DISC*(1./((1.+R)**(I-1)))
      YTEMP(1)=SUM+VWH1*DTSC
      I=10+2*ISTEP
      I=I+ITVAR
      IF(I.LE.(10+3*ISTEP))YTEMP(I)=-1.
      I=10+4*ISTEP
      I=I+ITVAR+LWH1
      IF(I.LE.(10+5*ISTEP))YTEMP(I)=1.
      KK=11+6*ISTEP
      KKK=10+7*ISTEP
      DO R3410 I=KK,KKK
      II=I-(10+6*ISTEP)
      IF(II.LT.ITVAR)GOTO R3410
      IF(II.GE.ITVAR+1WH1)GOTO R3410
      YTEMP(I)=1./KW1
R3410 CONTINUE
      KK=10+10*ISTEP
      KKK=9+11*ISTEP
      DO R3415 I=KK,KKK
      II=I-(9+10*ISTEP)
      IF(II.LT.ITVAR)GOTO R3415
      IF(II.GE.ITVAR+LWH1)GOTO R3415
      YTEMP(I)=VPW1/KW1
R3415 CONTINUE
      GO TO 00000
R3500 CONTINUE
C      HERR IF TWH2
      SUM=0.
      KK=1
      KKK=1WH2
      DO R3505 I=KK,KKK
R3505 SUM=SUM+(VPW2/KW2)*DISC*(1./((1.+R)**(I-1)))
      YTEMP(1)=SUM+VWH2*DTSC
      I=10+3*ISTEP
      I=I+ITVAR
      IF(I.LE.(10+4*ISTEP))YTEMP(I)=-1.
      I=10+5*ISTEP
      I=I+ITVAR+LWH2
      IF(I.LE.(10+6*ISTEP))YTEMP(I)=1.
      KK=11+6*ISTEP
      KKK=10+7*ISTEP
      DO R3510 I=KK,KKK
      II=I-(10+6*ISTEP)

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      IF (II.LT.ITVAR) GOTO R3510
      IF (II.GF.ITVAR+LWH2) GOTO R3510
      YTEMP(I)=1./KW2
R3510 CONTINUE
      KK=10+10*ISTEP
      KKK=9+11*ISTEP
      DO R3515 I=KK, KKK
      II=I-(Y+10*ISTEP)
      IF (II.LT.ITVAR) GOTO R3515
      IF (II.GF.ITVAR+LWH2) GOTO R3515
      YTEMP(I)=VPW2/KW2
R3515 CONTINUE
      GO TO HEND00
R3600 CONTINUE
C      HERE IF TWC1
      YTEMP(I)=VWC1*DISC
      I=10
      I=I+ITVAR+LWC1
      IF (I.LE.(10+ISTEP)) YTEMP(I)=1.
      I=10+2*ISTEP
      I=I+ITVAR
      IF (I.LE.(10+3*ISTEP)) YTEMP(I)=-1.
      GO TO HEND00
R3700 CONTINUE
C      HERE IF TWC2
      YTEMP(I)=VWC2*DISC
      I=10+ISTEP
      I=I+ITVAR+LWC2
      IF (I.LE.(10+2*ISTEP)) YTEMP(I)=1.
      I=10+3*ISTEP
      I=I+ITVAR
      IF (I.LE.(10+4*ISTEP)) YTEMP(I)=-1.
      GO TO HEND00
R3800 CONTINUE
C      HERE IF THC1
      YTEMP(I)=VHC1*DISC
      I=10
      I=I+ITVAR+LHC1
      IF (I.LE.(10+ISTEP)) YTEMP(I)=1.
      I=10+4*ISTEP
      I=I+ITVAR
      IF (I.LE.(10+5*ISTEP)) YTEMP(I)=-1.
      GO TO HEND00
R3900 CONTINUE
C      HERE IF THC2
      YTEMP(I)=VHC2*DISC
      I=10+ISTEP
      I=I+ITVAR+LHC2
      IF (I.LE.(10+2*ISTEP)) YTEMP(I)=1.
      I=10+5*ISTEP
      I=I+ITVAR
      IF (I.LE.(10+6*ISTEP)) YTEMP(I)=-1.
      GO TO HEND00
R4000 CONTINUE
C      HERE IF THW1
      YTEMP(I)=VHW1*DISC
      I=10+2*ISTEP
      I=I+ITVAR+LHW1

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      IF (I.LE.(10+3*ISTEP)) YTEMP(I)=1.
      I=I+4*ISTEP
      I=I+ITVAR
      IF (I.LE.(10+5*ISTEP)) YTEMP(I)=-1.
      GO TO H=000
R4100 CONTINUE
C      HERE IF THW2
      YTEMP(1)=VHW2*DISC
      I=I+3*ISTEP
      I=I+ITVAR+LHW2
      IF (I.LE.(10+4*ISTEP)) YTEMP(I)=1.
      I=I+5*ISTEP
      I=I+ITVAR
      IF (I.LE.(10+6*ISTEP)) YTEMP(I)=-1.
      GO TO H=000
R4200 CONTINUE
C      HERE IF THW1
      YTEMP(1)=(VW1+VDW1/KW1)*ZZ1+ZZ2*VS/KW1+ZZ3*VCW1+VPC1*ZZ4
      YTEMP(2)=-((1.-DW1)**(NPIURCH-1))
      YTEMP(4)=YTEMP(2)
      YTEMP(6)=ZZ5/KW1
      YTEMP(7)=-1./KW1
      YTEMP(8)=YTEMP(2)/KW1
      I=I+11*ISTEP
      Z77=0.
      DO R4205 II=1,NPIURCH
R4205 Z77=Z77+((1.-DW1)**(II-1))
      YTEMP(1)=VPC1+Z77*VDW1/KW1
      I=I+11*ISTEP
      IF (KC1.NE.0) I=I+3
      IF (KC2.NE.0) I=I+4
      IF (KC3.NE.0) I=I+1
      IF (NSS.GT.0) I=I+1
      IF (KC4.NE.1) GO TO R=000
      I=I+1
      YTEMP(1)=1.
      GO TO H=000
R4300 CONTINUE
C      HERE IF THW2
      YTEMP(1)=(VW2+VDW2/KW2)*ZY1+ZY2*VS/KW2+ZY3*VCW2+VPC2*ZY4
      YTEMP(3)=-((1.-DW2)**(NPIURCH-1))
      YTEMP(5)=YTEMP(3)
      YTEMP(6)=ZY5/KW2
      YTEMP(7)=-1./KW2
      YTEMP(8)=YTEMP(3)/KW2
      I=I+11*ISTEP
      Z7Y=0.
      DO R4305 II=1,NPIURCH
R4305 Z7Y=Z7Y+((1.-DW2)**(II-1))
      YTEMP(1)=VPC2+Z7Y*VDW2/KW2
      I=I+11*ISTEP
      IF (KC1.NE.0) I=I+3
      IF (KC2.NE.0) I=I+4
      IF (KC3.NE.0) I=I+1
      IF (NSS.GT.0) I=I+1
      IF (KC4.NE.1) GO TO R=000
      I=I+1
      YTEMP(1)=1.

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      GO TO 85000
C
85000 CONTINUE
C
      DO 9270 I=1,NMROWS
      YTEMP1=YTEMP(I)
      IF (ABS(YTEMP1).IF.7TOLZE) GO TO 9270
      NFLEM=NFLEM+1
      IA(NFLEM)=I
      A(NFLEM)=YTEMP1
9270 CONTINUE
      NCCL=NCCL+1
      LA(NCOL+1)=NELEM+1
      GO TO 8400
C
9300 DO 9390 J=J1,J2
C
      DO 9380 I=1,NMROWS
      CALL GETPHI(I,JJ,CUTS(J),ATEMP)
      IF (ABS(ATEMP).IF.7TOLZE) GO TO 9380
      NFLEM=NFLEM+1
      IA(NFLEM)=I
      A(NFLEM)=ATEMP
9380 CONTINUE
      NFLEM=NFLEM+1
      IA(NFLEM)=NMROWS+NCCL
      A(NFLEM)=1.
      NCCL=NCCL+1
      LA(NCOL+1)=NELEM+1
9390 CONTINUE
      NCCL=NCCL+1
9400 CONTINUE
      IF(NFLEM.GT.MAXA)CALL FRR(3)
200  FORMAT(16A5)
250  FORMAT(8A10)
C *****DONE READING IN DATA
C *****SET UP STARTING BASIS
      DO 9200 I=1,NROW
      JH(I)=I
      KINRAS(I)=I
9200 IF(K5.EQ.1)CALL SCATL
      IF(K2.NE.0)365,370
360 PRINT 361
361  FORMAT(1H0,55HPACKED MATRIX BY COLUMNS, ROW NUMBER BELOW EACH ELEM
      ENT)
      IXI=NFLEM/11+1
      DO 365 I=1,IXI
      KK=(I-1)*11+1
      IF(KK.GT.NELEM)GO TO 370
      K=KK+10
      IF(K.GT.NELEM)K=NELEM
      PRINT 366,(A(J),J=KK,K)
      PRINT 367,(IA(J),J=KK,K)
366  FORMAT(1H0,11G12.4)
367  FORMAT(1H ,11I12)
365 CONTINUE
370 CONTINUE
      PRINT 200

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290  FORMAT(1H1,19HSTARTING TO ITERATE)
    PRINT 300
300  FORMAT(1H0,4X,19HSTAGE,PROBLEM,7X,11HLOWER BOUND,9X,11HUPPER BOUND
1,6X,19HBRANCHING VARIABLE,/)
C    *****READY TO START LOOP
C    *****READY TO START LOOP
C    *****READY TO START LOOP
C    *****READY TO START LOOP
      DO 990 I=1,LSTMAX
        IDOVR(I)=0
990    ZLSLR(I)=1.F90
        PARENT=0.0
        LSTKR(I)=0
        LSTKL(I)=0
        STGPPR=0.0
        LSTNUM=0
        NLP=0
        IRPPAR=0
        NOLEFT=1
          DO 990 I=1,NIMVAR
            KL(I)=KLO(I)
990      KH(I)=KRO(I)
1000  PRINT 1005,STGPPR
1005  FORMAT(1H0,8X,F6.1)
        NOLEFT=NOLEFT-1
        NLP=NLP+1
        IF(NLP.GT.MAXLP)CALL ERR(4)
C
      JK=KRO(NIMVAR)
      DO 6000 J=1,JK
C
6000  W(J)=0.0
      CALL LIMERG
      IF(K1.EQ.1)CALL LOPP(W)
      IF(LFLG.NE.1)GO TO 1010
      IF(NLP.EQ.1)CALL FRR(5)
      PRINT 1008
1008  FORMAT(1H+,24X,11HLo. INFELAS.)
      GO TO 5000
1010  IF(VAL-RIERTOL.LE.BUB)GO TO 1020
      PRINT 1015
1015  FORMAT(1H+,25X,9HLo GT BUB)
      GO TO 5000
C    *****PUT THIS PROBLEM ON THE LIST, FIND THE NEXT EMPTY SPOT
1020  IF (LSTNUM.GT.LSTMAX)CALL FRR(6)
      PRINT 1025,VAL
1025  FORMAT(1H+,25X,G12.4)
      LSTNUM=LSTNUM+1
      ZLSTNO(LSTNUM)=STGPPR
      ZLSTPA(LSTNUM)=PARENT
      IF(IRPPAR.NE.0)LSTKL(LSTNUM)=KL(IRPPAR)
      IF(IRPPAR.NE.0)LSTKR(LSTNUM)=KH(IRPPAR)
      ZLSLR(LSTNUM)=VAL
C    *****NOT DONE WITH LIST YET
C    *****CREATE XCODED, COMPACTIFIED VERSION OF X--ELEMENTS OF XCODED
C    *****AKE X, IF X CORRESPONDS TO A LINEAR VARIABLE. OR ELSE THE
C    *****MEAN OF GUARDED VARIABLES
      DO 1030 I=1,NIMVAR

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        IF (KLO(I).NE.KRO(I))GO TO 1040
        II=KLO(I)
        XCODED(I)=W(II)
        GO TO 1020
1040    XCODED(I)=0.0
        IW=KLO(I)
        IZ=KRO(I)
        DO 1050 IT=IW,IZ
1050    XCODED(IT)=XCUEED(I)+W(II)*CUTS(II)
1030    CONTINUE
C      *****XCUEED CREATED, CHECK IT
        DO 1060 I=1,NUMVAR
        IF (KLO(I).EQ.KRO(I))GO TO 1060
        IL=KLO(I)
        IR=KRO(I)
        XXI=CUTS(II)-CUTTOL
        XXR=CUTS(IR)+CUTTOL
        IF (XCUEED(I).LT.XXL)CALL ERR(7)
        IF (XCUEED(I).GT.XXR)CALL ERR(7)
1060    CONTINUE
C      *****NOW WE WILL TRY TO FIND AN UPPER BOUND AND ALSO A
C      *****BRANCHING VARIABLE
        IFEAS=0
        DIFFMA=0.0
        IREVR(I:INUM)=0
        UR=1.E/0
        DO 2000 IROW=1,NMROWS
        IF (ICLK(IROW).EQ.1)GO TO 2000
        ROWVAL=0.0
        DO 2010 I=1,NUMVAR
C      *****SET INDEX AND FRAC
        IW=KLO(I)
        IZ=KRO(I)
        IF (IW.EQ.IZ)7005,7010
7005    INDEX=-1
        FRAC=0.0
        GO TO 7000
7010    IH=IZ-1
        DO 7015 IJ=IW,IH
        IK=IJ+1
        IF (CUTS(IJ).LE.XCODED(I).AND.CUTS(IK).GT.XCODED(I))GO TO 7025
7015    CONTINUE
        XXX=CUTS(IW)-XCODED(I)
        XXX=ABS(XXX)
        IF (XXX.IE.CUTTOL)GO TO 7016
        XXX=XCODED(I)-CUTS(IZ)
        XXX=ABS(XXX)
        IF (XXX.IE.CUTTOL)GO TO 7017
        CALL ERR(7)
7025    FRAC=(XCODED(I)-CUTS(IJ))/(CUTS(IK)-CUTS(IJ))
        INDEX=IJ
        GO TO 7000
7016    INDEX=IW
        FRAC=0.0
        GO TO 7000
7017    INDEX=IZ
        FRAC=0.0
7000    CONTINUE

```

```

DIFF=0.0
DO 2020 IJ=TW,TZ
  IT=I+NDOW
  INDCOL=IA(IT)
  INDNXT=IA(IT+1)-1
  DO 2030 I=INDCOL,INDNXT
    IF (IA(IT).NE.ITROW) GO TO 2030
    IF (INDEX.NE.-1) DIFF=DIFF-W(IJ)*A(III)
    IF (INDEX.EQ.IJ) DIFF=DIFF+(1.-FRAC)*A(III)
    IF (INDEX.EQ.-1) ROWVAL=ROWVAL+XCODEN(I)*A(III)
    IF (INDEX.EQ.IJ) ROWVAL=ROWVAL+(1.-FRAC)*A(III)
    IF ((INDEX+1).EQ.I) DIFF=DIFF+FRAC*A(IT)
    IF ((INDEX+1).EQ.I) ROWVAL=ROWVAL+FRAC*A(III)
  CONTINUE
2030 CONTINUE
2020 CONTINUE
  IF (ISTYPE(ROW).EQ.-1) DIFF=ABS(DIFF)
  IF (DIFF.LT.DIFFMA+DIFFTO) GO TO 2010
  DIFFMA=DIFF
  FLAG(LSTNUM)=INDEX
  FLAG(LSTNUM)=FLAG(LSTNUM)+FRAC
  IRVR(LSTNUM)=I
2010 CONTINUE
  IF (ISTYPE(ROW)) 2040,2050,2060
2050 IR=ROWVAL
  GO TO 2000
2060 IF (R(ROW)) 2061,2062,2063
2061 IF (ROWVAL.LE.(B(ROW)*(1.-FEASTL))) GO TO 2000
  IFEAS=1
  GO TO 2000
2062 IF (ROWVAL.LE.FEASTL) GO TO 2000
  IFEAS=1
  GO TO 2000
2063 IF (ROWVAL.LE.(B(ROW)*(1.+FEASTL))) GO TO 2000
  IFEAS=1
  GO TO 2000
2040 IF (ABS(R(ROW)).EQ.0.0) GO TO 2070
  XXX=1.-ABS(ROWVAL/B(ROW))
  IF (ABS(XXX).LT.FEASTL) GO TO 2000
  IFEAS=1
  GO TO 2000
2070 IF (ABS(ROWVAL).LE.FEASTL) GO TO 2000
  IFEAS=1
2000 CONTINUE
C *****DONE--WE HAVE PICKED A BRANCHING VARIABLE AND STORED IT ON
C *****THE LIST WHILE TESTING FOR FEASIBILITY
  IF (IFEAS.NE.1) GO TO 3000
  PRINT 2005,IRVR(LSTNUM)
2005 FORMAT(1H+,49X,4HNONFE,16X,16)
  GO TO 3000
  PRINT 3005,UR,IRVR(LSTNUM)
  PRINT 3005,UR,IRVR(LSTNUM)
  IF (IXPRINT.EQ.1) CALL XPRINT(XCODEN)
  IF (UR.LT.RUB) GO TO 3010
  GO TO 3000
3010 RIIR=UR
  DO 3020 I=1,NUMVAR
C *****NOW BEGIN BRANCHING PROCEDURE
3020 XDEFN(I)=XCODEN(I)

```

```

5000 IF (NOLFT.EQ.0) GO TO 5050
C *****SOLVE NEXT PROBLEM IN THIS STAGE
KL(IARRPA)=KHL(NOLFT)
Kp(IARRPA)=KBR(NOLFT)
STGPRH=STGPRB+.1
GO TO 1000
C *****WE ARRIVE HERE IF WE ARE DONE WITH A STAGE
5050 NIIM=0
RLR=1.E70
DO 5060 I=1,1STNUM
IF (ZLSLR(I).GE.RLR) GO TO 5060
NIIM=I
RLR=ZLSLR(I)
5060 CONTINUE
IF (RLR.GE.1.E70) CALL EPR(8)
IF (RLR.GE.BUR-DONT01) GO TO 8000
C *****NUM IS THE ENTRY ON THE LIST ON WHICH WE ARE TO BRANCH
5062 FORMAT(1F0,20HDONE WITH THIS STAGE)
IF (IRPVR(NUM).NE.0) GO TO 5064
CALL FHD(9)
5064 PRINT 5063
PRINT 5065,RLB,RIR,7LSTNO(NUM),IRPVR(NIIM)
5065 FORMAT(1F,6HRLB=,G12.4,H, BUR=,G12.4,22H, BRANCHING ON PROBL
1EM,F5.1,17H, VARIABLE NUMBER,16)
IF (K4.EQ.1) PRINT 50651
50651 FORMAT(1F0,32H*****PRESENT STATUS OF LIST)
IF (K4.EQ.1) PRINT 50652
50652 FORMAT(1F0,6HPRORNO,5X,6HPARENT,5X,6HLISTKL,5X,6HLISTKR,5X,
11HLOWFO ROUNO,5X,12HBRANCH, VAR.,RX,4HFLAG,/)
IF (K4.EQ.1) 50653,50657
50653 DO 50000 I=1,LSTNIIM
PRINT 50001,ZLSTNO(I),7LSTPA(I),LSTKL(I),LSTKR(I)
50001 FORMAT(1F,F6.1,5X,F6.1,5X,15.0X,1E)
IF (7LSLR(I).GE.1.E70) 50002,50004
50002 PRINT 50003,IRPVR(I),FLAG(I)
50003 FORMAT(1F+,48X,3H0FF,4X,9X,14.9X,F10.2)
GO TO 50009
50004 PRINT 50005,ZLSLR(I),IRPVR(I),FLAG(I)
50005 FORMAT(1F+,44X,G11.2,9X,14.9X,F10.2)
50000 CONTINUE
PRINT 50656
50656 FORMAT(1F0)
50657 CONTINUE
PARFNT=7LSTNC(NIIM)
IARRPA=IRPVR(NUM)
C *****NOW WE KNOW THE PARENT AND BRANCHING VARIABLE FOR THE NEXT
C *****STAGE--SET UP 2 OR 3 NEW PROBLEMS
C *****FILL KL AND KR VECTORS
DO 5070 I=1,NIIMVAR
KR(I)=KRO(I)
5070 KL(I)=KLO(I)
ZNRACK=7LSTNC(NIIM)
DO 5080 I=1,NIIM
IJ=NIIM-I+1
IF (7NRACK.EQ.0,0) GO TO 5110
IF (ZLSTNO(IJ).NE.7NRACK) GO TO 5080
DO 5090 IK=1,NUM
IF (ZLSTNO(IK).EQ.ZLSIPA(IJ)) GO TO 5095

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```

5090      CONTINUE
5095      IIT=IBRVK(IK)
      IF (.NOT.((LSTKL(IIT).GE.KI(IIT)).AND.(LSTKR(IIT).LE.KR(IIT))))
1      GO TO 5130
      KL(IIT)=LSTKL(IIT)
      KR(IIT)=LSTKR(IIT)
5100      ZNRACK=ZLSTPA(IIT)
5080      CONTINUE
5110 CONTINUE
C      *****NOW HAVE TO DIVIDE UP THE K-SET FOR THE BRANCHING VARIABLE
C      *****BUT FIRST, REMOVE THE PARENT PROBLEM FROM THE LIST
      ZLCLR(NIIM)=1.E7A
C      *****SET UP TWO OR THREE PROBLEMS
      IF ((FLAG(NUM).LT.KL(IRRPAR)).OR.(FLAG(NUM).GT.KR(IRRPAR)))
1CALL ERK(11)
C      *****CHECK TO SEE IF FLAG PRECISELY EQUALS SOME CUT
      IW=KL(IRRPAR)
      IZ=KR(IRRPAR)
      DO 5120 J=IW,I7
      ZJ=J
      XXX=ZJ-FLAG(NIIM)
      XXY=ABS(XXX)
      IF (XXX.LE.CHITOL) GO TO 5130
5120      CONTINUE
      IX=FLAG(NIIM)
      IF (IX.EQ.KL(IRRPAR)) GO TO 5140
      KRL(1)=KL(IRRPAR)
      KRR(1)=IX
      KRL(2)=IX
      KRR(2)=IX+1
      IF ((IX+1).EQ.KR(IRRPAR)) 5150,5160
5150      NOLEFT=2
      GO TO 5180
5160      KRL(3)=IX+1
      KRR(3)=KR(IRRPAR)
      NOLEFT=3
      GO TO 5180
5140      KRL(1)=IX
      KRR(1)=IX+1
      KRL(2)=IX+1
      KRR(2)=KR(IRRPAR)
      NOLEFT=2
      GO TO 5180
5170      IF ((J.EQ.KL(IRRPAR)).OR.(J.EQ.KR(IRRPAR))) CALL ERK(10)
      KRL(1)=KL(IRRPAR)
      KRR(1)=J
      KRL(2)=J
      KRR(2)=KR(IRRPAR)
      NOLEFT=2
6080      TXX=STGPRR
      STGPRR=TXX
      STGPRR=STGPRR+1.
      GO TO 5180
C      *****DONE-- PRINT OUT THE RESULTS
8000 CONTINUE
8010 FORMAT(1F10,8A10)
      PRINT N820,RLB
8020 FORMAT(1F10,31HOBJECTIVE FUNCTION AT OPTIMUM ,G12.4)

```

```

TCOSTS=TCOSTS+BIIR
PRINT B225,TCOSTS
R02= FORMAT(I10,/* TOTAL DISCOUNTED COSTS= *,F10.3/)
PRINT B230
R03= FORMAT(I10,28HVARIABLE VALUES AT OPTIMUM=)
CALL XPRINT(XBEST)
END

```

```

SUBROUTINE XPRINT(7)
COMMON      KLN(R40),KRO(R40),KL(R40),KH(R40),XCODED(R40),XREST
1(R40),W(R40),CUTS(R40),ZLSTNO(5),71STPA(5),LSTKL(*),LSTKR(5),
2ZLSLR(5),IHRVR(5),FIAG(5),KBL(3),KPR(3),VARNAM(1),PROBNA(1),
3MAXVAR,MAXCUT,LSTMAX,MAXROW,MAXA,NMROWS,NUMVAR,ICLK(430),VAL,LFLG,
4ISTEP,LW1,LW2,KW1,KW2,KH1,KH2
DIMENSION W1(36),W2(36),H1(36),H2(36),TWH1(36),TWH2(36),PROD(36)

DIMENSION Z(1)
REAL KW1,KW2,KH1,KH2

PRINT 1A
10 FORMAT(1F0)
PRINT 2A
20 FORMAT(1F0,* BUILD-UP PERIOD *50(1H*))
I1=6+2*ISTEP
I2=7+2*ISTEP
PRINT 115,Z(11),7(I2)
110 FORMAT(1F0,*IBW1= *F12.3,3X*IBW2= *F12.3)
PRINT 110,Z(1),7(2),7(3),Z(4)
110 FORMAT(1F0,*RC1= *F12.3,3X*RC2= *F12.3,3X*RW1= *F12.3,3X*RW2= *
1F12.3)
A=7(5)-7(6)
R=7(7)-7(8)
C=7(9)-7(10)
D=7(11)-7(12)
PRINT 120,A,R,C,D
120 FORMAT(1F0,*SLOPEC1= *F12.3,3X*SLOPEC2= *F12.3,3X*SLOPEW1= *F12.3,
13X,*SLOPEW2= *F12.3)
PRINT 120
120 FORMAT(1F0,* STEADY-STATE PERIOD *50(1H*))
TOTCAP=7(13)+Z(14)+7(15)+Z(16)
PRINT 130,Z(13),7(14),7(15),Z(16),TOTCAP
130 FORMAT(1F0,*EC1= *F12.3,3X*EC2= *F12.3,3X*EW1= *F12.3,3X*EW2= *F12
1.3,3X*INITAL CAPITAL= *,F12.3)
PRINT 140,Z(17),7(18)
140 FORMAT(1F0,*ES= *F12.3,3X*EPREF= *F12.3)
XRATIO=TOTCAP/Z(17)
PRINT 141,XRATIO
141 FORMAT(1F0,* BASE/STOCKPILE RATIO= *F7.3)
PRINT 142
142 FORMAT(1F0,* WAP TIME PERIOD *50(1H*))
PRINT 1A
DO 150 I=1,ISTEP
I1=I+1H
I2=I+1H+1STEP
I3=I+1H+2*ISTEP
I4=I+1H+3*ISTEP
I5=I+1H+4*ISTEP
W1(I)=Z(I3)
W2(I)=Z(I4)
H1(I)=Z(I5)
150 PRINT 145,I,Z(I1),I,Z(I2),I,Z(I3),I,Z(I4),I,Z(I5)
145 FORMAT(1F0,*C1(*I2*)=*F12.3,6X,*C2(*I2*)=*F12.3,6X*W1(*I2*)=*F12.3
1.6X*W2(*I2*)=*F12.3,6X*H1(*I2*)=*F12.3)
DO 160 I=1,ISTEP
I1=I+1H+5*ISTEP

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```

I2=I+18+6*ISTEP
I3=I+18+7*ISTEP
I4=I+18+8*ISTEP
I5=I+18+9*ISTEP
H2(I)=Z(I1)
160 PRINT 165,I,Z(I1),I,Z(I2),I,Z(I3),I,Z(I4),I,Z(I5)
165 FORMAT(1H,*,H2(*I2*)=*F12.3,6X*PC1(*I2*)=*F12.3,5X*PC2(*I2*)=*F12.
13,5X*5(*I2*)=*F12.3,7X*SP(*I2*)=*F12.3)
II=ISTEP-1
DO 170 I=1,II
I1=I+18+10*ISTEP
I2=I+17+11*ISTEP
I3=I+16+12*ISTEP
I4=I+15+13*ISTEP
I5=I+14+14*ISTEP
170 PRINT 175,I,Z(I1),I,Z(I2),I,Z(I3),I,Z(I4),I,Z(I5)
175 FORMAT(1H,*,PIPF(*I2*)=*F12.3,4X*TCW1(*I2*)=*F12.3,4X*TCW2(*I2*)=*
1F12.3,4X*TCH1(*I2*)=*F12.3,4X*TCH2(*I2*)=*F12.3)
DO 180 I=1,II
I1=I+13+15*ISTEP
I2=I+12+16*ISTEP
I3=I+11+17*ISTEP
I4=I+10+18*ISTEP
I5=I+9+19*ISTEP
TWH1(I)=7(I1)
TWH2(I)=7(I2)
180 PRINT 185,I,Z(I1),I,Z(I2),I,Z(I3),I,Z(I4),I,Z(I5)
185 FORMAT(1H,*,TWH1(*I2*)=*F12.3,4X*TW2(*I2*)=*F12.3,4X*TWC1(*I2*)=*
1F12.3,4X*TWC2(*I2*)=*F12.3,4X*THC1(*I2*)=*F12.3)
DO 190 I=1,II
I1=I+8+20*ISTEP
I2=I+7+21*ISTEP
I3=I+6+22*ISTEP
190 PRINT 195,I,Z(I1),I,Z(I2),I,Z(I3)
195 FORMAT(1H,*,THC2(*I2*)=*F12.3,4X*THW1(*I2*)=*F12.3,4X*THW2(*I2*)=*
1F12.3)

```

```

C
C      PRINT OUT PRODUCTION CURVE
C

```

```

DO 300 I=1,ISTEP
I71=LWH1
I72=LWH2
IF (I71.GT.I) I71=I
IF (I72.GT.I) I72=I
SMTWH1=0.
DO 201 J=1,I71
SMTWH1=SMTWH1+TWH1(I-J+1)
201 CONTINUE
SMTWH2=0.
DO 202 J=1,I72
SMTWH2=SMTWH2+TWH2(I-J+1)
202 CONTINUE
C
XX1=(SMTWH1+W1(I))/KW1
XX2=(SMTWH2+W2(I))/KW2
XX3=H1(I)/KH1
XX4=H2(I)/KH2
PRCD(I)=XX1+XX2+XX3+XX4

```



```

300 CONTINUE
      PRINT 310
310  FORMAT(1H ,//*   WARTIME PRODUCTION CURVE */)
      XSUM=0.
      DO 320 I=1,ISTEP
      XSUM=XSUM+PROD(I)
      PRINT 315,I,PROD(I)
315  FORMAT(1H ,*PRODUCTION(*I2*)=*F12.3)
320  CONTINUE
      PRINT 330,XSUM
330  FORMAT(1H-,*   TOTAL WARTIME PRODUCTION=*,F10.3)
      PRINT 10
      RETURN
      END

```

```

SUBROUTINE LPPR(Y)
COMMON      KLD(R40),KHO(R40),KL(R40),KH(R40),XCODED(R40),XREST
1(R40),W(R40),CUTS(R40),ZLSTNO(5),ZLSTPA(5),LSTKL(5),LSTKR(5),
27LCLR(5),IHRVR(5),FLAG(5),KBL(3),KPR(3),VARNAM(1),PROBNA(1),
3MAXVAR,MAXCUT,LSTMAX,MAXROW,MAXA,NMROWS,NUMVAR,ICLK(430),VAL,LFLG,
4[STEP,LWP1,LWP2,KW],KW2,KH1,KH2
DIMENSION Y(1)
PRINT 15
10  FORMAT(1F0,29HPACKED LP SOLUTION, 1  X(I))
      IW=KHO(NUMVAR)
      DO 30 I=1,IW
      IF (ABS(Y(I)).GE.1.F-10) PRINT 20,I,Y(I)
20  FORMAT(1H,15X,I6,2X,G10.4)
30  CONTINUE
PRINT 45
40  FORMAT(1F0)
RETURN
END

```

```

SUBROUTINE EPR(T)
PRINT100
100 FORMAT(*PROGRAM MOGG ABORTED BECAUSE,...*)
GOTO(101,102,103,104,105,106,107,108,109,110,111),I
101 PRINT 201
CALL EXIT
102 PRINT 202
CALL EXIT
103 PRINT 203
CALL EXIT
104 PRINT 204
CALL EXIT
105 PRINT 205
CALL EXIT
106 PRINT 206
CALL EXIT
107 PRINT 207
CALL EXIT
108 PRINT 208
CALL EXIT
109 PRINT 209
CALL EXIT
110 PRINT 210
CALL EXIT
111 PRINT 211
CALL EXIT
RETURN
201 FORMAT(*VARIABLE CARDS OUT OF ORDER--LOOK NEAR MOGG LABEL 105*)
202 FORMAT(*MAXCUTS EXCEEDED--LOOK NEAR MOGG LABEL 117 OR 124*)
203 FORMAT(*MATRIX A EXCEEDED--LOOK NEAR MOGG LABEL 9400*)
204 FORMAT(*LPMAX EXCEEDED--LOOK NEAR MOGG LABEL 1005*)
205 FORMAT(*INITIAL LP INFEASIBLE--LOOK NEAR MOGG LABEL 1008*)
206 FORMAT(*LIST LENGTH EXCEEDED--LOOK NEAR MOGG LABEL 1020*)
207 FORMAT(*EXCODED VIOLATES CUTS--LOOK NEAR MOGG LABEL 1060 OR 7025*)
208 FORMAT(*NO BRANCHING NODE FOUND--LOOK NEAR MOGG LABEL 5060*)
209 FORMAT(*NO FEASIBLE POINT FOUND--LOOK NEAR MOGG LABEL 5064*)
210 FORMAT(*NO BRANCHING POSSIBLE ON VARIABLE CHOSEN--LOOK NEAR MOGG
1 LABEL 5120*)
211 FORMAT(*FLAG COMPILED IMPROPERLY--LOOK NEAR MOGG LABEL 5110*)
END

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SUBROUTINE SCAII
COMMON      KLO(R40),KHO(R40),KL(R40),KH(R40),XCNUED(R40),XREST
1(R40),W(R40),CUTS(R40),ZLSTNO(5),ZLSTPA(5),LSTKL(5),LSTKR(5),
271SLR(5),THPRV(5),FIAG(5),KBL(3),KPR(3),VARNAM(1),PROBNA(1),
3MAXVAR,MAXCUT,LSTMAX,MAXROW,MAXA,NMROWS,NUMVAR,ICLK(430),VAL,LFLG,
41STEP,LWH1,LWH2,KW1,KW2,KH1,KH2
COMMON/WORK1/B(430),X(430),Y(430),VTEMP(430),A(3700),E(5700),
1IA(3700),IE(5700),LA(1302),LE(2002),ICNAM(1302,2),KINBAS(1302),
2JL(430),ISTYPE(430),NAME(20),NTEMP(20),CMIN,COND,ERMAX,IFFEZ,
3INVEKO,TORJ,IROWP,ITCH,IYCHA,ITCNT,ITHFRQ,IYIN,IYOUT,JCPLP,KINP,
4XSTAT,NROW,NCOL,NFLEM,NETA,NLELEM,NIFTA,NGELEM,NGETA,NUFLEM,
5NIETA,SIJINF,K3
COMMON/LOCK/ ZTOLFE,ZTOLPV,ZTCOST,NRMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1GFI,QFC,QRL,QPL,QMJ,QA,QB,QC,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BLDG(36),DD(36),ED(36),HSP(36),HPIPE(36)
DO 100 IXX=2,NMROWS
SMALL=1.E70
BIG=-1.E70
LAST=LA(NCOL+1)-1
IFIRST=IA(NROW+1)
DO 200 IXY=IFIRST, LAST
IF(IA(IXY).NE.IXX)GOTO200
IF(ABS(A(IXY)).LT.SMALL)SMALL=ABS(A(IXY))
IF(ABS(A(IXY)).GT.BIG)BIG=ABS(A(IXY))
200 CONTINUE
AV=SQRT(SMALL*BIG)
Z1ZAV=ALOG(AV)/ALOG(2.)
L2ZAV=INT(Z1ZAV)
IF(Z1ZAV.LT.0..AND.L2ZAV-Z1ZAV.GE..5)L2ZAV=L2ZAV-1
IF(Z1ZAV.GT.0..AND.Z1ZAV-L2ZAV.GE..5)L2ZAV=L2ZAV+1
DIV=2.**L2ZAV
DO 300 IXY=IFIRST, LAST
IF(IA(IXY).NE.IXX)GOTO300
A(IXY)=A(IXY)/DIV
300 CONTINUE
R(IXX)=R(IXX)/DIV
100 CONTINUE
RETURN
END

```

SUBROUTINE LINPRG

```

COMMON      KL0(840),KRO(840),KL(840),KR(840),XCODED(840),XBEST
1(840),W(840),CUTS(840),ZLSTNO(5),ZLSTPA(5),LSTKL(5),LSTKR(5),
2ZLCLB(5),IBRV(5),FLAG(5),KBL(3),KPR(3),VARNAM(1),PROBNA(1),
3MAXVAR,MAXCUT,LSTMAX,MAXROW,MAXA,NMROWS,NUMVAR,ICLK(430),VAL,LFLG,
4ISTEP,LWH1,LWH2,KW1,KW2,KH1,KH2
COMMON/WORK1/B(430),X(430),Y(430),YTEMP(430),A(3700),E(5700),
1IA(3700),IE(5700),LA(1302),LF(2002),ICNAM(1302,2),KINBAS(1302),
2JH(430),ISTYPE(430),NAME(20),NTFMD(20),CMIN,COND,ERMAX,IFFEZ,
3INVERK,IOBJ,IPROW,ITCH,ITCHA,ITCNT,ITFRQ,IVIN,IVOUT,JCOLP,KINP,
4XSTAT,NROW,NCOL,NFLEM,NETA,NLELEM,NIFTA,NGELEM,NGETA,NUFLEM,
5NIETA,SUMINF,K3
COMMON/LOCK/ZT017F,7TOLPV,7TCOST,NRMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1GFI,QFC,QBL,QPL,QMT,QA,QB,QC,QE,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUDG(36),DD(36),FU(36),HNSP(36),URPIPE(36)

C
C
C
      ITCNT=0
      ITCHA=0
C      SET UP STARTING BASIS
      DO 9100 J=1,NCOL
9100  KTBAS(J)=0
      DO 900 I=1,NROW
      ICOL=JH(I)
      ML=NROW
      DO 700 K=1,NUMVAR
      MR=KL(K)+NROW
      IF((ICOL.GT.ML).AND.(ITCOL.LT.MR))GO TO 700
      ML=KR(K)+NROW
900  CONTINUE
      IF(ITCOL.GT.ML)GO TO 700
      GO TO 900
700  JH(I)=I
900  CONTINUE
C
C
C 1000 CALL INVERT
      ITSJNV = 0
      CALL ITFROP(0)
C
C      SIMPLIFX CYCLE
C
1500 CALL FUDMC
      CALL SHIFTR(3,4)
      ITCH=0
1700 CALL RTDAN
      CALL PRICE
      IF (CMIN.LE.-ZTCOST) GO TO 3000
      IF (XSTAT.EG.01) GO TO 2000
      XSTAT = QBL
      GO TO 6000
2000 XSTAT=QM
      GO TO 6000
3000 CALL UNPACK(JCOLP)
      CALL FIDAN(1)

```

```

      ERMAX=0.
      DO 8000 I=1,NROW
      ERMAX=ERMAX+Y(I)*YTEMP(I)
8000  CONTINUE
      DIFXX=CMIN-ERMAX
      DIFXX=ABS(DIFXX)
      IF (DIFXX.LE.ZTCOST) GO TO 8500
      IF (K3.NF.1) GO TO 8100
      PRINT 9500,CMIN,ERMAX
9500  FORMAT(1F,10X,6HCMIN=,F14.8,5X,7HERMAX=,F16.8)
8100  IF (ERMAX.LE.0.) GO TO 8500
      IF (ITCH.GT.0) GO TO 1000
      ITCH=JCOLP
      ITCHA=ITCHA+1
      CALL SHIFTR(4,3)
      GO TO 1700
8500  CONTINUE
      CALL CHUZR
      IF (XSTAT.EQ.GU) GO TO 6000
      IVOUT=JH(IROWP)
      IVIN = JCOLP
      CALL UPPEFA
      KINRAS(JCOLP) = IPQWP
      KINRAS(IVOUT) = 0
      JH(IPQWP) = IVIN
      ITCNT = ITCNT + 1
      ITSINV = ITSINV + 1
      CALL ITFROP(1)
      IF (NFIEN.GT.5500) GO TO 1000
      CALL WRPEFA
      IF (ITSTAV .GE. INVERQ) GO TO 1000
      IF (ITCNT .GE. ITPERO) GO TO 6000
      GO TO 1500
C
6000  CALL ITFROP(1)
C
C      SFT DAKMS
C
      DO 7000 I=1,NROW
      JHX=JH(I)
      IF (JHX.LE.NROW) GO TO 6500
      W(JHX-NROW)=X(I)
6500  CONTINUE
7000  CONTINUE
C
C      VAL=-X(ICRJ)
      LFLG=1
      IF (XSTAT.EQ.QB1) LFLG=0
      PRINT 9600,ITCHA
9600  FORMAT(1F,10X,14HSTABILITY COUNT = ,I5)
7100  CONTINUE
      RETURN
      END

```

SUBROUTINE FORMC

```

C
COMMON/WORK1/B(430),X(430),Y(430),VTFMP(430),A(3700),E(5700),
1IA(3700),IE(5700),LA(1302),LE(2002),TCNAM(1302,2),KINBAS(1302),
2 JH(430),ISTYPE(430),NAME(20),NTFMP(20),CMIN,COND,ERMAX,IFFE7,
3 INVERH,IORJ,IPOW,ITCH,ITCHA,ITCNT,ITKFRQ,IVIN,IVOUT,JCPLP,KINP,
4 XSTAT,APOW,NCOL,NFLEM,NETA,NLELEM,NIFTA,NGELEM,NGETA,NUFLEM,
5 NUFETA,SUMINF,K3
COMMON/BLOCK/ ZTOL7F,ZTOLMV,ZTCOST,NEMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1 QFI,QFC,QRL,QPL,QMI,QDA,UR,QC,QF,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION RUCU(36),RD(36),FU(36),HSP(36),HPIPE(36)

C
C
XSTAT=0F
IFFE7 = 1
DO 100 I = 1,NROW
Y(I) = 0.
100 CONTINUE
SUM = 0.

C
DO 1000 I = 1,NROW
ICOL = JH(I)
IF (ICOL .GT. NROW) GO TO 500
IF (ISTYPE(ICOL)) 200,1000,500

C
200 IF (ABS(X(I)) .IF. ZTOLZE) GO TO 1000
IF(X(I) .LT. 0.) Y(I) = +1.
IF(X(I) .GT. 0.) Y(I) = -1.
SUM = SUM + ABS(Y(I))
GO TO 510

C
500 IF(X(I) .GT. -ZTOL7F) GO TO 1000
Y(I) = +1.
SUM = SUM - X(I)
510 IFFE7 = 1
XSTAT = GI
1000 CONTINUE

C
SUMINF = SUM
IF (IFFE7 .LE. 0) GO TO 9000
Y(ORJ) = 1.

C
9000 RETURN
END

```

SUBROUTINE BTRAN

```

COMMON/WORK1/B(430),X(430),Y(430),YTEMP(430),A(3700),E(5700),
1 IA(3700),IE(5700),LA(1302),LE(2002),ICNAM(1302,2),KINBAS(1302),
2 JF(430),ISTYPE(430),NAME(20),NTEMP(24),CMIN,COND,EPMAX,IFFEZ,
3 INVERO,IORJ,IROW,ITCH,IYCHA,ITCNT,ITKFRQ,IVIN,IVOUT,JCOLP,KINP,
4 XSTAT,NROW,NCOL,NFLEM,NETA,NLELEM,NLETA,NGELEM,NGETA,NUELEM,
5 NLETA,SUMINF,K3
COMMON/BLOCK/ ZTOL7F,ZTOLPV,ZTCOST,NRMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1 QFI,QFC,QBL,QBL,QMT,QQA,QRC,QCE,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUOG(36),ND(36),FD(36),URSP(36),URPIPE(36)

```

```

IF (NETA .LE. 0) GO TO 9000
DO 1000 I = 1,NETA
IK = NETA - I + 1
LL = LE(IK)
KK = IE(IK+1) - 1
IPIV = IE(LL)
DP = E(IK)
DY = Y(IPIV)
DSUM = 0.
IF (KK .LE. LL) GO TO 600
LL = LL + 1
DO 500 J = LL,KK
IP = IE(J)
DE = E(J)
DPROD = DE * Y(IP)
DSUM = DSUM + DPROD

```

500 CONTINUE

```

600 Y(IPIV) = (DY - DSUM) / DP
1000 CONTINUE

```

```

9000 RETURN
END

```


SUBROUTINE PRICE

```

COMMON      KLO(840),KRO(840),KL(840),KH(840),XCODED(840),XBEST
1(840),W(840),CUTS(840),ZLSTNO(5),ZLSTPA(5),LSTKL(5),LSTKR(5),
27LCLR(5),IBQVR(5),FLAG(5),KBL(3),KPR(3),VARNAM(1),PROBNA(1),
3MAXVAR,MAXXCUT,LSTMAX,MAXROW,MAXA,NMROWS,NUMVAR,ICWK(430),VAL,LFLG,
4ISTEP,LWF1,LWF2,KW1,KW2,KH1,KH2
COMMON/WORK1/B(430),X(430),Y(430),YTEMP(430),A(3700),E(5700),
1IA(3700),IE(5700),LA(1302),LE(2002),ICNAM(1302,2),KINBAS(1302),
2JH(430),ISTYPE(430),NAME(20),NTEMP(20),CMIN,COND,FRMAX,IFFEZ,
3INVERO,IORJ,IPOWP,ITCH,IYCHA,ITCNT,ITKFRQ,IVIN,IVOUT,JCOLP,KINP,
4XSTAT,NROW,NCOL,NFLEM,NETA,NLELEM,NIFTA,NGELEM,NGETA,NUELEM,
5NIETA,SUMINF,K3
COMMON/BLOCK/ ZTOLPF,ZTOLPV,ZTCOST,NRMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1GFI,QFC,QBL,QPL,QMI,QA,QB,QC,QE,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUDG(36),DD(36),FD(36),UPSP(36),UBPIPE(36)

```

```

JCCLP = 0
CMIN = 1.E10
DO 1000 J = 1,NCOL
IF (J.LE. NROW .AND. ISTYPE(J).NE. 1) GO TO 1000
IF (KINBAS(J).NE. 0) GO TO 1000
IF (ITCH.EQ.J) GO TO 1000

```

```

DSUM = 0.
LL = LA(J)
KK = LA(J+1) - 1
DO 500 I = LL,KK
IP = IA(I)
DE = A(I)
DPROD = DE * Y(IP)
DSUM = DSUM + DPROD

```

```

500 CONTINUE
IF (DSUM.GE. CMIN) GO TO 1000
CMIN = DSUM

```

```

JCCLP = J
1000 CONTINUE
RETURN
END

```

SUBROUTINE SHIFTR(TOLD,INEW)

```

C      COMMON/WORK1/H(430),X(430),Y(430),VTEMP(430),A(3700),E(5700),
1     IIA(3700),IE(5700),IA(1302),LE(2002),TCNAM(1302,2),KINBAS(1302),
2     JH(430),ISTYPE(430),NAME(20),NTEMP(20),CMIN,COND,ERMAX,IFFEZ,
3     INVERO,IORJ,IROWP,ITCH,ITCHA,ITCNT,ITKFRQ,IVIN,IVOUT,JCOLP,KINP,
4     XSTAT,AROW,NCOL,NLEFM,NETA,NLELFM,NIFTA,NGELEM,NGETA,NUFLEM,
5     NIETA,SUMINF,K3
C      COMMON/BLOCK/ ZTOLZF,ZTOLPV,ZTLOST,NRMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1     GFI,QFC,QBL,QPL,QMT,QA,QR,QC,QE,QF,QG,QH,QI,QL,QM,QN,QU,QR,QU,QZ
C      DIMENSION BUDD(36),DD(36),FU(36),URSP(36),UBPIPE(36)
C
C      DIMENSION BARRAY(1400)
C      EQUIVALENCE (BARRAY(1),B(1))
C
C      IFO = (TOLD - 1) * NRMAX
C      IFN = (TNEW - 1) * NRMAX
C
C      DO 1000 I = 1,NROW
C      BARRAY(IFO + I) = BARRAY(IFN + I)
1000 CONTINUE
C      RETURN
C      END

```

SHRPOUTTAE UNPACK(TV)

```

COMMON/WCRK1/B(432),X(430),Y(430),YTFMP(430),A(3700),E(5700),
1 IA(3700),IE(5700),LA(1302),LE(2002),TCNAM(1302,2),KINBAS(1302),
2 JF(430),ISTYPE(430),NAME(20),NTFMP(20),CMIN,COND,ERMAX,IFFE7,
3 INVFKC,IORJ,IPQWP,ITCH,ITCHA,ITCNT,ITKFRQ,IVIN,IVOUT,JCOLP,KINP,
4 XSTAT,XROW,NCOL,NFLEM,NETA,NLELEM,NIFIA,NGELEM,NGETA,NUFLEM,
5 NIETA,SUMINF,K2
COMMON/PLCK/ ZTQ17F,ZTULPV,ZTCOST,NRMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1 QFI,QFC,QRL,QPL,QMT,QA,QB,QC,QE,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUCC(36),DD(36),FD(36),UDSP(36),URPIPE(36)

```

```

DO 100 I = 1,NROW
Y(I) = 0.
100 CONTINUE

```

```

LL = LA(TV)
KK = LA(TV+1) - 1
DO 200 I = LL,KK
IP = IA(I)
Y(IP) = A(I)
200 CONTINUE

```

```

RETURN
END

```

SUBROUTINE FTRAN(IPAR)

```

C
COMMON/WCPK1/B(432),X(430),Y(430),VTEMP(430),A(3700),E(5700),
1IA(3700),IE(5700),LA(1302),LE(2002),ICNAM(1302,2),KINBAS(1302),
2 JH(430),ISTYPE(430),NAME(20),NTFMP(20),CMIN,COND,ERMAX,IFFEZ,
3 INVERC,IORU,IPROW,ITCH,ITCHA,ITCNT,ITHFREQ,IVIN,IVOUT,JCOLP,KINP,
4 XSTAT,AROW,NCOL,NFLEM,NETA,NLELEM,NIFTA,NGELEM,NGETA,NUELEM,
5 NUNETA,SUMINF,K3
COMMON/BLOCK/ ZTOLZF,ZTOLPV,ZTLOST,NEMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1 GFI,GFQ,QRI,QPL,QMT,QA,QA,QC,QE,CF,CG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUD(36),DD(36),FU(36),HSP(36),URPIPE(36)
C
GO TO (100,110),IPAR
100 NFF = 1
NLF = NETA
GO TO 200
110 NFF = NUNETA + 1
NLF = NETA
200 IF (NFF .GT. NLF) GO TO 9000
DO 1000 JK = NFF,NLF
LL = LE(JK)
KK = LE(JK+1) - 1
IPIV = IF(LL)
DY = Y(IPIV)
DY = DY/F(LL)
Y(IPIV) = DY
IF (KK .LE. LL) GO TO 1000
LL = LL + 1
DO 500 I = LL,KK
IR = IE(I)
Y(IR) = Y(IR) - F(J) * DY
500 CONTINUE
1000 CONTINUE
9000 CONTINUE
RETURN
END

```

SUBROUTINE CHUZR

```

COMMON/WORK1/B(432),X(430),Y(430),VTEMP(430),A(3700),E(5700),
1IA(3700),IE(5700),LA(1302),LE(2002),ICNAM(1302,2),KINBAS(1302),
2 JH(430),ISTYPE(430),NAME(20),NTFMD(20),CMIN,COND,ERMAX,IFFE7,
3 INVERNO,IORJ,IROWP,ITCH,ITCHA,ITCNT,ITFRQ,IVIN,YVOUT,JCOLP,KINP,
4 XSTAT,AROW,NCOL,NFLEM,NETA,NLELEM,NIFTA,NGELEM,NGETA,NUELEM,
5 NNETA,CUMINF,K2
COMMON/BLOCK/ ZTOLZF,ZTOLXX,ZTCOST,NRMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1 GFT,WFC,QRL,QRL,QNT,QA,WR,QU,QE,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUDG(36),DD(36),FD(36),URSp(36),URPIPE(36)

```

SELECT PIVOT ROW/VARIABLE TO LEAVE THE BASIS

```

ZTOLCH=1.E-5
ZTOLXX=1.E-10
XMIN1=1.F10
XMIN2=1.F10
XMIN3=1.F10
IROWP1=0
IROWP2=0
IROWP3=0

```

```

DO 2000 I=1,AROW
IF (ISTYPE(I).EQ.0) GO TO 2000
IF (ABS(Y(I)).LT.ZTOLCH) GO TO 2000
ICOL=JH(I)
IF ((ICOL.LE.NROW).AND.(ISTYPE(I).LT.0)) GO TO 1000
XRATIO=X(I)/Y(I)
IF (XRATIO.LT.-ZTOLZF)GOTO2000
IF (Y(I).LT.0.)GOTO2000
IF (XRATIO.GT.XMIN1) GO TO 2000
XMIN1=XRATIO
IROWP1=I
GO TO 2000

```

```

1000 IF (ABS(X(I)).LT.ZTOLZF) GO TO 1500
XRATIO=X(I)/Y(I)
IF (XRATIO.LT.0.) GO TO 2000
IF (XRATIO.GT.XMIN2) GO TO 2000
XMIN2=XRATIO
IROWP2=I
GO TO 2000

```

```

1500 XXX=ABS(Y(I))
XRATIO=ZTOLXX/XXX
IF (XRATIO.GT.XMIN3) GO TO 2000
XMIN3=XRATIO
IROWP3=I

```

2000 CONTINUE

TEST FOR OUTGOING VECTOR

```

IROWP=IROWP1
XRATIO=XMIN1
IF (XRATIO.LE.XMIN2) GO TO 3000

```

```

      IRCWP=IRCWP2
      XRATIO=XMIND
C
3000 IF (XRATIO.LE.XMIND) GO TO 4000
      IRCWP=IRCWP3
      XRATIO=XMIND3
C
4000 IF (IROWP.LE.0) XSTAT=QU
      I=IROWP
      IF (K3.NE.1) RETURN
      PRINT 9700,IROWP,Y(I),Y(I),JH(1)
9000 FORMAT(2F IRCWP= ,I4,2X,6H Y(I)= ,F16.8,2X,6H Y(I)= ,F16.8,2X
1,7H JH(1)= ,I4)
      RETURN
      END

```

SUBROUTINE UPBETA

```

COMMON/WORK1/B(432),X(430),Y(430),VTEMP(430),A(3700),E(5700),
1IA(3700),IE(5700),LA(1302),LE(2002),TCNAM(1302,2),KINBAS(1302),
2 JH(430),ISTYPE(430),NAME(20),NTFMD(25),CMIN,COND,ERMAX,IFFEZ,
3 INVERNO,IORJ,IROWP,ITCH,ITCHA,ITCNT,ITKFRQ,IVIN,IVOUT,JCOLP,KINP,
4 XSTAT,AROW,NCOL,NFLEM,NETA,NLELEM,NIFIA,NGELEM,NGETA,NUFLEM,
5 AUETA,SUMINF,K3
COMMON/BLOCK/ ZT01ZF,ZTOLPV,ZTCOST,NRMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1 GFI,QFC,QBL,QPL,QMJ,QA,QR,QC,QE,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUDG(36),DD(36),FU(36),HSP(36),URPIPE(36)

```

```

DE = X(IROWP)
DP = DE/Y(IROWP)
X(IROWP) = DP
DO 1000 I = 1,NROW
IF (I.EQ. IROWP) GO TO 1000
DE = X(I)
X(I) = DE - Y(I)*DP
1000 CONTINUE
RETURN
END

```

SUBROUTINE WRETA

```

C
COMMON/WORK1/B(435),X(430),Y(430),VTEMP(430),A(3700),E(5700),
1IA(3700),IE(5700),LA(1302),LE(2002),ICNAM(1302,2),KINBAS(1302),
2 JH(430),ISTYPE(430),NAME(20),NTEMP(25),CMIN,COND,ERMAX,IFFEZ,
3 INVERQ,IORJ,IROWP,ITCH,IYCHA,ITCNT,ITFRQ,IVIN,YVOUT,JCOLP,KINP,
4 XSTAT,AROW,NCOL,NFLEM,NETA,NLELEM,NIFTA,NGELEM,NGETA,NUELEM,
5 NIETA,SUMINF,K2
COMMON/BLOCK/ ZTOLZF,ZTOLPV,ZTCOST,NRMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1 GF1,QFC,QBL,QPL,QM1,QA,QR,QC,QE,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUDG(36),DD(36),FD(36),HSP(36),URPIPE(36)

C
NFLEM = NFLEM + 1
IF(NFLEM) = IROWP
E(NFLEM) = Y(IROWP)

C
DO 1000 I = 1,NROW
IF (I.EQ. IROWP) GO TO 1000
IF (ABS(Y(I)) .LE. ZTOLZE) GO TO 1000
NFLEM = NFLEM + 1
IF(NFLEM) = I
E(NFLEM) = Y(I)
1000 CONTINUE

C
NETA = NETA + 1
LF(NETA,1) = NFLEM + 1
RETURN
END

```


SUBROUTINE ITEROP(IPAR)

```

COMMON/WORK1/B(432),X(430),Y(430),VTFMP(430),A(3700),E(5700),
1 IA(3700),IE(5700),LA(1302),LE(2002),ICNAM(1302,2),KINBAS(1302),
2 JH(430),ISTYPE(430),NAME(20),NTFMP(20),CMIN,COND,ERMAX,IFFE7,
3 INVEKO,IORJ,IOWP,ITCH,ITCHA,ITCNT,ITFRQ,IVIN,IVOUT,JCOLP,KINP,
4 XSTAT,AROW,NCOL,NFLEM,NETA,NLELEM,NIEIA,NGELEM,NGETA,NUFLEM,
5 NUETA,SUMINF,K2
COMMON/BLOCK/ ZTOL7F,ZTOLPV,ZTCOST,NHMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1 QFI,QFC,QRL,QPL,QMI,QA,QR,QC,QF,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUDG(36),DD(36),FU(36),URSP(36),URPIPE(36)

```

```

IF (IPAR.EQ.0) GO TO 1000
OBJ = -X(10BJ)
IF (IFFE7.EQ. 1) OBJ = SUMINF

```

```

IF (K3.NF.1) RETURN
WRITE(6,P000) ITCNT,XSTAT,OBJ,IVIN,IVOUT,CMIN,
INETA,NLEFM,TIMEP
8000 FORMAT(1F,15,4XA4,2X,F16.8,4X,I6,4X,T6,4X,F16.8,4X,I6,I8,
1F8.2 )
GO TO 7000
1000 IF (K3.NF.1) RETURN
WRITE(6,P100)
8100 FORMAT(//RH0ITCNT,2X,HSTATUS,4X,QWOR,1 VALUE,8X,5HVECIN,5X,HVECOIT
1,11X,2HNUJ,12X,4HNETA,3X,5HNLEFM,4X,4HTIME )
9000 RETURN
END

```

SUBROUTINE INVERT

```

COMMON/WCPK1/B(435),X(430),Y(430),YTEMP(430),A(3700),E(5700),
1IA(3700),IE(5700),LA(1302),LE(2002),ICNAM(1302,2),KINBAS(1302),
2 JH(430),ISTYPE(430),NAME(20),NTEMP(20),CMIN,COND,ERMAX,IFFEZ,
3 INVEKO,IORJ,IROW,ITCH,ITCHA,ITCNT,ITFRQ,IVIN,IVOUT,JCOLP,KINP,
4 XSTAT,AROW,NCOL,NFLEM,NETA,NLELEM,NIFTA,NGELEM,NGETA,NUELEM,
5 NIETA,SUMINF,K3
COMMON/ALOCK/ ZTOLZF,ZTOLPV,ZTOLST,NRMAX,NTMAX,NEMAX,QR0,QMA,QBA,
1 CFI,QFC,QBL,QPL,QMI,QA,QH,QC,QE,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUDG(36),DD(36),FU(36),HSP(36),URPIPE(36)

```

```

INTEGER MREG,HREG,VREG
DIMENSION MREG(432),HREG(430),VREG(430)
EQUIVALENCE (MREG,YTEMP),(HREG,X)

```

SET PARAMETERS

```

NETA = 0
NLETA = 0
NGETA = 0
NIETA = 0
NFLEM = 0
NLELEM = 0
NGELEM = 0
NIFLEM = 0
NAROW = 0
LF(1) = 1
LP1 = 1
KP1 = 0
LP4 = NDCW + 1
KP4 = NDCW

```

PUT SLACKS AND ARTIFICIALS IN PART 4 AND REST IN PART 1

```

DO 100 I = 1,NROW
IF (JH(I) .GT. NROW) GO TO 50
LP4 = LP4 - 1
MREG(LP4) = JH(I)
VREG(LP4) = JH(I)
GO TO 90
50 KP1 = KP1 + 1
VREG(KP1) = JH(I)
90 HREG(I) = -1
JH(I) = 0
100 CONTINUE

```

```

KP3 = LP4 - 1
LP3 = LP4

```

```

DO 200 I = LP4,KP4
IR = MREG(I)
HREG(IR) = 0
JH(IR) = IR
KINBAS(IF) = IR
200 CONTINUE

```

PULL OUT VECTORS BELOW RUMP AND GET ROW COUNTS

```

C
C
NRAONZ = KR4 - LP4 + 1
IF (KR) .EQ. 0) GO TO 1190
J = LR1
210 IV = VREG(J)
LL = LA(IV)
KK = LA(IV+1) - 1
IRCNT = 0
DO 220 I = LL, KK
NRAONZ = NRAONZ + 1
IR = IA(I)
IF (HREG(IR) .GE. 0) GO TO 220
IRCNT = IRCNT + 1
HREG(IR) = HREG(IR) - 1
IRP = IR
220 CONTINUE
IF (IRCNT = 1) 230, 250, 300
230 CONTINUE
IF (K3.EQ.1) PRINT A000
4000 FORMAT(1AHOMATRIX SINGULAR )
KTARAS(IV) = 0
VREG(J) = VREG(KR1)
KR1 = KR1 - 1
IF (J .GT. KR1) GO TO 310
GO TO 210

```

```

C
250 VREG(J) = VREG(KR1)
KR1 = KR1 - 1
LR3 = LR3 - 1
VREG(LK3) = IV
HREG(LK3) = IRP
HREG(LK3) = 0
JH(IRP) = IV
KTARAS(IV) = IRP
IF (J .GT. KR1) GO TO 310
GO TO 210
300 IF (J .GE. KR1) GO TO 310
J = J + 1
GO TO 210

```

PULL OUT REMAINING VECTORS ABOVE AND BELOW THE
BUMP AND ESTABLISH MERIT COUNTS OF COLUMNS

```

C
C
310 NVREFM = 0
IF (KR1 .EQ. 0) GO TO 1190
J = LR1
320 IV = VREG(J)
LL = LA(IV)
KK = LA(IV+1) - 1
IRCNT = 0
DO 330 I = LL, KK
IR = IA(I)
IF (HREG(IR) .NE. -2) GO TO 400
330 CONTINUE
PIVOT ABOVE RUMP (PART OF L)
NAROVE = NAROVE + 1

```

```

      IRCWP = IR
      CALL UNPACK(IV)
      CALL WHETA
      NLETA = NETA
      JH(IP) = IV
      KIARAS(IV) = IR
      VREG(J) = VREG(KR1)
      KR1 = KR1 - 1
      NVREM = NVREM + 1
      HREG(IV) = IV
      GO TO 940
C
400 IF (HREG(IR) .GE. 0) GO TO 800
      IRCNT = IRCNT + 1
      IRP = IR
      800 CONTINUE
C
      IF (IRCNT = 1) R10,900,1000
810 CONTINUE
      IF(K3.EQ.1)PRINT R000
      KIARAS(IV) = 0
      VREG(J) = VREG(KR1)
      NVREM = NVREM + 1
      KR1 = KR1 - 1
      IF (J .GT. KR1) GO TO 1010
      GO TO 320
C
C          PUT VECTOR BELOW BUMP
C
900 VREG(J) = VREG(KR1)
      NVREM = NVREM + 1
      KR1 = KR1 - 1
      LR3 = LR3 - 1
      VREG(LR3) = IV
      HREG(LR3) = IRP
      HREG(IV) = 0
      JH(IRP) = IV
      KIARAS(IV) = IRP
C
C          CHANGE ROW COUNTS
C
940 DO 950 IJ = LL,KK
      IIR = IA(IJ)
      IF (HREG(IIR) .GE. 0) GO TO 950
      HREG(IIR) = HREG(IIR) + 1
950 CONTINUE
      IF (J .GT. KR1) GO TO 1010
      GO TO 320
1000 IF (J .GE. KR1) GO TO 1010
      J = J+1
      GO TO 320
1010 IF (NVREM .GT. 0) GO TO 310
C
C          GET MERIT COUNTS
C
1020 IF (KR1 .EQ. 0) GO TO 1190
      DO 1100 IJ = LR1,KR1
      IV = VREG(J)

```

```

LL = LA(IV)
KK = LA(IV+1) - 1
IMCNT = 0
DO 1050 I = LL, KK
  IP = IA(I)
  IF (HREG(IR) .GE. 0) GO TO 1050
  IMCNT = IMCNT - (HREG(IR) + 1)
1050 CONTINUE
MREG(J) = IMCNT
1100 CONTINUE
C
C          SORT COLUMNS INTO MERIT ORDER
C          USING SHELL SORT
C
  ISD = 1
1106 IF (KPI .LT. 2*ISD) GO TO 1108
  ISD = 2*ISD
  GO TO 1106
1108 ISD = ISD - 1
C          END OF INITIALIZATION
1109 IF (ISD .LE. 0) GO TO 1107
  ISK = 1
  ISJ = ISK
  ISL = ISK + ISD
  ISY = MREG(ISL)
  ISZ = VREG(ISL)
1109 IF (ISY .LT. MREG(ISJ)) GO TO 1104
1106 ISL = ISJ + ISD
  MREG(ISL) = ISY
  VREG(ISL) = ISZ
  ISK = ISK + 1
  IF ((ISK + ISD) .IF. KPI) GO TO 1102
  ISD = (ISD - 1) / 2
  GO TO 1101
1104 ISL = ISJ + ISD
  MREG(ISL) = MREG(ISJ)
  VREG(ISL) = VREG(ISJ)
  ISJ = ISJ - ISD
  IF (ISJ .GT. 0) GO TO 1103
  GO TO 1105
1107 CONTINUE
C          END OF SORT ROUTINE
C
C          PUT HIT BELOW BUMP FTAS (PART OF U)
C
1108 NSICK = 0
  NRELOW = 0
  NFI AST = NEMAX
  NTI AST = NTMAX
  LE(NTI AST + 1) = NFI AST + 1
C
  IP = IR3
  IF (LR3 .GE. LR4) LP = LR4
  IF (LR .GT. KR4) GO TO 2050
  JK = KR4 + 1
  DO 2000 IJ = LR, KR4
  JK = JK - 1
  IV = VREG(JK)

```

```

      I = MREG(JK)
      NRELOW = NBELOW + 1
      IF (IV .GT. NROW) GO TO 1200
      NSLCK = ASLCK + 1
1200  LL = LA(IV)
      KK = LA(IV+1) - 1
      IF (KK .GT. LL) GO TO 1300
1250  IF (ABS(A(LL) - 1.) .LE. 4TOL7E) GO TO 2000

```

```

C
1300  NIETA = NUETA + 1
      DO 1400 J = LL, KK
      IR = IA(J)
      IF (IR .EQ. I) GO TO 1390
      IF (NEI ACT) = IR
      F(NFLAST) = A(J)
      NFLAST = NELAST - 1
      NIIFLEM = NUELEM + 1
      GO TO 1400
1390  EP = A(J)
1400  CONTINUE
      IF (NELAST) = I
      F(NFLAST) = EP
      LF(NTI ACT) = NEI ACT
      NFLAST = NELAST - 1
      NTLAST = NTLAST - 1
      NIIFLEM = NUELEM + 1
2000  CONTINUE
2050  IF (KR1 .EQ. 0) GO TO 3500

```

```

C
C          DO L-U DECOMPOSITION OF BUMP
C

```

```

      DO 3000 J = LR1, KR1
      IV = MREG(J)
      CALL UNPACK(IV)
      CALL FIDAN(2)
      IROWP = 0
      IRCMIN = -999999
      DO 2100 I = 1, NROW
      IF (ABS(Y(I)) .LE. 7TOLPV) GO TO 2100
      IF (MREG(I) .GE. 0) GO TO 2100
      IF (MREG(I) .LE. IRCMIN) GO TO 2100
      IRCMIN = MREG(I)
      IROWP = I
2100  CONTINUE
      IF (IROWP .GT. 0) GO TO 2150
      IF (K2 .EQ. 1) PRINT 8000
      KJNRAS(IV) = 0
      GO TO 3000

```

```

C
2150  INCP = MREG(IROWP) + 3
C
C          WRITE I AND U ETAS
C

```

```

      IF (J .EQ. KR1) GO TO 2160
      NFLEM = NELEM + 1
      IF (NELEM) = IROWP
      F(NFLEM) = Y(IROWP)
2160  DO 2300 J = 1, NROW

```

```

IF (I .EQ. IROWP) GO TO 2300
IF (ABS(Y(I)) .LE. 7TOLZE) GO TO 2300
IF (HREG(I) .GE. 0) GO TO 2400

```

L ETA ELEMENTS

```

NLEFM = NLEFM + 1
IF(NLEFM) = 1
E(NLEFM) = Y(I)
GO TO 2300

```

U ETA ELEMENTS

```

2200 IF(NELAST) = 1
E(NELAST) = Y(I)
NELAST = NELAST - 1
NUELEM = NUELEM + 1
2300 CONTINUE

```

```

JH(IROWP) = IV
KTHAS(IV) = IROWP
NIETA = NIETA + 1
IF(NELAST) = IROWP
IF (J .NE. KR1) GO TO 2330
E(NELAST) = Y(IROWP)
GO TO 2340

```

```

2330 E(NELAST) = 1.
NETA = NETA + 1
LE(NETA+1) = NLEFM + 1

```

```

2340 NLEFM = NUELEM + 1
LE(NLAST) = NELAST
NELAST = NELAST - 1
NLAST = NLAST - 1

```

UPDATE ROW COUNTS

```

DO 2350 I = 1,NROW
IF (ABS(Y(I)) .LE. 7TOLZE) GO TO 2350
IF (HREG(I) .GE. 0) GO TO 2350
HREG(I) = HREG(I) - INCR
IF (HREG(I) .GE. 0) HREG(I) = -1
2350 CONTINUE
HREG(IROWP) = 0
3000 CONTINUE

```

MERGE I AND U ETAS

```

3500 NLEFM = NETA
NETA = NLETA + NIETA
NLEFM = NELEM
NLEFM = NLELEM + NLEFM
IF (NLEFM .EQ. 0) GO TO 3550
CALL SHETE

```

INSERT SLACKS FOR DELETED COLUMNS

```

3550 DO 3600 I = 1,NROW
IF (JH(I) .NE. 0) GO TO 3600

```

```

      JH(I) = I
      IRCWP = I
      CALL UNPACK(I)
      CALL FIDAN(I)
      CALL WHETA
3000 CONTINUE
C
C          UPDATE X
C
      CALL SHIFTR(1,3)
      CALL FTRAN(1)
      CALL SHIFTR(3,2)
C
C          PRINT STATISTICS
C
      NODD = NFLEM - NETA
      NSTR = NROW - NSICK
      IF(K3.NF.1)RETURN
      WRITE(6,=00)NBNONZ,NSTR,NAROVE,NRELOW,NLELEM,NLETA,NUELEM,NUETA,
      1HOD,NETA
500 FORMAT(1PHOINVERT STATISTICS/1H ,I4,14H NONZ IN BASIS/1H ,I4,
      12PH STRUCTURAL COLUMNS IN BASIS/1H ,I4,19H VECTORS ABOVE BUMP/1H ,
      2I4,19H VECTORS BELOW BUMP/3H 11,15,5H NONZ,15,5H ETAS/3H 11,15,
      35H NONZ,15,5H ETAS/PH TOTALS:15,14H OFF DIAG NONZ,15,5H ETAS )
C
      RETURN
      END

```


SUBROUTINE SHFTF

```

COMMON/WORK1/B(432),X(430),Y(430),VTEMP(430),A(3700),E(5700),
1  IA(3700),IE(5700),LA(1302),LE(2002),ICNAM(1302,2),KINBAS(1302),
2  JH(430),ISTYPE(430),NAME(20),NTEMP(20),CMIN,COND,ERMAX,IFFEZ,
3  INVERO,IORJ,IPOWP,ITCH,ITCHA,ITCNT,ITKFRQ,IVIN,IVOUT,JCOLP,KINP,
4  XSTAT,AROW,NCOL,NFLEM,NETA,NLELEM,NIFTA,NGELEM,NGETA,NUFLEM,
5  NNETA,SUMINF,K3
COMMON/BLOCK/ ZTOLZF,ZTOLPV,ZTCOST,NFMAX,NTMAX,NEMAX,QRO,QMA,QBA,
1  GFI,WFC,QBL,QPL,QMT,QA,QB,QC,QE,QF,QG,QH,QI,QL,QM,QN,QO,QR,QU,QZ
DIMENSION BUDD(36),DD(36),FU(36),URSP(36),URPIPE(36)

```

SHIFT IF AND F OF U ELEMENTS

```

NF = NEMAX - NUFLEM + 1
INCR = 2
DO 1000 I = NF,NEMAX
  INCR = IACR + 1
  IF(NLELEM + INCR) = IE(I)
  F(NLELEM + INCR) = F(I)

```

1000 CONTINUE

```

IDIF = NFMAX - NLELEM - NUFLEM
NF = NTMAX - NNETA + 1
INCR = 2
DO 2000 I = NF,NTMAX
  INCR = IACR + 1
  LE(NLETA + INCR) = IE(I) - IDIF
2000 CONTINUE
LE(NETA+1) = NLEFM + 1
RETURN
END

```

SUBROUTINE GETPHT(I,J,Y,F)
RETURN
END

```

FUNCTION FUNCT1(A,I)
IF (I.GE.2) GO TO 10
FUNCT1=1.
RETURN
10  FUNCT1=1.
    I=I-1
    DO 20 J=1,I
20  FUNCT1=FUNCT1+(1.-A)** J
    I=I+1
RETURN
END

```

```

FUNCTION FUNCT2(A,I)
  IF (I.GE.2) GO TO 10
  FUNCT2=0.
  RETURN
10 FUNCT2=0.
  I=I-1
  DO 20 J=1,I
  20 FUNCT2=FUNCT2+FLOAT(J)*((1.-A)**(I-J) )
  I=I+1
  RETURN
END

```

```

FUNCTION FUNCT3(A,R,I)
IF (I.GE.1) GO TO 10
FUNCT3=0.
RETURN
10 FUNCT3=0.
DO 20 J=1,I
20 FUNCT3=FUNCT3+((1.-A)**(I-J))*FUNCT1(R,J)
RETURN
END

```

```

FUNCTION FUNCT4 (A,R,I)
FUNCT4=0.
IF (I.LT.1) RETURN
DO 20 J=1,I
20 FUNCT4=FUNCT4+((1.-A)**(I-J))*FUNCT2 (R,J)
RETURN
END

```

```

FUNCTION FUNCT5(DW,DS,NPURCH)
IF (NPURCH-1) 10,20,30
10 FUNCT5=0.
RETURN
20 FUNCT5=1.
RETURN
30 LL=0
LL=NPURCH-1
FUNCT5=0.
DO 40 I=LL,LL
40 FUNCT5=FUNCT5+((1.-DW)**(NPURCH-1-I))*((1.-DS)**I)
RETURN
END

```